

AFWAL-TR-81-4172



DEVELOPMENT OF ENGINEERING DATA ON
ADVANCED COMPOSITE MATERIALS

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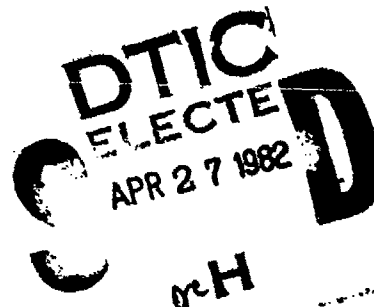
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Engineering data have been generated on six advanced composite materials; T300/AFR800 (graphite/epoxy by Hexcel); SiC/5506 (silicon carbide/epoxy by AVC6); HyE 2034D (pitch based graphite/epoxy by Fiberite); T300/V378A (graphite/polyimide by U.S. Polymer); HyE 1076J (graphite/epoxy by Fiberite); and 6535-1 (graphite/epoxy by AVC6). Prepreg tape was obtained from each vendor and laminates and test specimens prepared at UDR. Five different static mechanical properties (tension, compression, flexure, inplane shear, and		

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interlaminar shear) were measured on various fiber orientations at four different temperatures (-67°F, 72°F, and two elevated temperatures). Tensile fatigue, creep, and stress-rupture tests were also conducted and four thermophysical properties (thermal expansion, thermal conductivity, specific heat, and glass transition temperature) were determined. Environmental agings (at 160°F and 100 percent relative humidity) were conducted on each material and the effects on this exposure on several mechanical properties were determined. On four of the materials, tests were conducted on specimens with a hole located in the center of the gage section. On the last material, three different ply stacking sequences incorporating 0°, 90°, and +45° plies were tested. These three different sequences gave rise to tensile, compressive, and zero stress in the thickness direction at the specimen free edges.

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PREFACE

This summary report covers work performed during the period from 1 September 1978 to 30 September 1981 under Air Force Contract F33615-78-C-5172. The contract was initiated under Project Number 7381, "Materials Application". The work was administered under the direction of the Systems Support Division of the Air Force Wright Aeronautical Laboratories/ Materials Laboratory, Wright-Patterson Air Force Base, Ohio. Mr. David Watson (AFWAL/MLSA) acted as Project Engineer.

This work was conducted under the general supervision of Mr. D. Gerdeman, Project Supervisor. The Principal Investigator for this program was D. Robert Askins. Research Technicians who made major contributions to the program include: R. J. Kuhbander, D. Byrge, R. Glett, R. Rondeau, D. Pike, D. Miller, and W. Miller.

The author is also indebted to Dr. Fred Bogner for the analysis and computation of normal edge stresses in the multi-directional laminates.

This report was submitted by the author in October 1981. The contractor's report number is UDR-TR-81-85.

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SECTION 1

INTRODUCTION

Fiber reinforced composite materials have been used in Aerospace structures for many years. The use of these materials is continually growing, and as new fiber reinforcements and matrix materials become available, the problem of selecting materials becomes an ever-growing task for aircraft builders and designers. In order to screen and select materials for a particular aircraft structure, a certain minimal amount of engineering data must be available to the aircraft designer. The data base from which this information is extracted must be continually updated and supplemented so that the spectrum of available candidate composite systems for consideration be broadened in step with the latest technological advancements. Data such as this are intended to reduce the time lag between the development of a new composite material system or component and its eventual use in an aircraft system. The general objective of this program was to develop engineering data on advanced composite materials. These materials were to be newly developed composite materials systems which were commercially available, but which at the same time were new enough that little data was available for the purpose of evaluating their potential. The purpose was to generate physical, mechanical, and thermophysical properties on a number of these advanced composite materials. The data generated in this program are not sufficient to eliminate the need for more detailed and more comprehensive design data programs. Rather, an initial data base is developed to facilitate the selection of candidate materials, and which provides a basis for developing subsequent design allowable efforts on selected materials. It provides the information required to make preliminary assessments of composite materials for potential aerospace service.

SECTION 2

SELECTION OF MATERIALS

The initial portion of the program involved an identification of available candidate composite materials. Both written and verbal contact was established with a wide cross-section of industry and government representatives who are active in the area of composite materials research, development, and application. Letter questionnaires were sent to individuals representing all the services, all the major aircraft companies, and nearly all of the major material suppliers. The questionnaire was directed toward obtaining each individual's feelings as to what materials should be considered for inclusion in this program, what their assessment of the current data availability on the various materials was, and their feelings as to potential applications for which the various advanced and newly available composite material systems might be considered. In addition, these representatives were asked what they felt the most useful and most needed type of engineering data were, as well as their feeling about the effect of manufacturing processes required for a specific composite material or its potential usage by the Aerospace community. These letter-questionnaires were sent to a total of 111 individuals. A total of 16 written responses were received, representing 14 percent of the total mailing. In addition to the written inputs numerous telephone contacts were made with individuals who did not respond in writing to our questionnaires and to obtain additional information to that requested in the letter. All the verbal as well as written inputs to this phase of the program were tabulated and discussed with Air Force Wright Aeronautical Laboratory/Materials Laboratory (AFWAL/ML) representatives prior to the establishment of a list of tentative candidate materials for possible inclusion in the program.

The criteria employed to determine and select these candidate materials included (a) the present or imminent commercial

availability of the material, (b) the degree of interest in the material expressed in the written responses and telephone contacts, (c) the material's potential to overcome specific problems of current concern to the United States Air Force (USAF), and (d) the potential value to the USAF if the material proves applicable to Air Force weapons systems. The candidate material identification and selection process was a continuing activity throughout the program. As new materials were learned of they were added to the candidate list and telephone inquiries were initiated to learn as much as possible about the material. A total of six composite systems were ultimately selected from among the candidates for inclusion in the data generation effort. These six selections were made approximately every six months starting at the beginning of the program. Table 1 lists the candidates which were considered at one time or another. In most cases a fiber or resin matrix candidate is listed alone.

The six composite material systems ultimately selected were:

- (1) T300/AFR800 by Hexcel,
- (2) SiC/5506 by AVCO,
- (3) HyE 2034D by Fiberite,
- (4) T300/V378A by U.S. Polymeric,
- (5) HyE 1076J by Fiberite, and
- (6) 6535-1 by AVCO.

The T300/AFR800 system was selected because it is an epoxy system which does not require refrigerated storage. It was developed by the Aerotherm Division of Accurex Corporation under contract to the Air Force Materials Laboratory to compete with 350°F (177°C) epoxy systems.

The silicon carbide/5506 system was selected because of the silicon carbide fiber. This fiber, on a carbon substrate, was developed by the AVCO Corporation and provides properties essentially equivalent to boron fiber but has a potentially

TABLE 1
CANDIDATE MATERIALS

<u>Material</u>	<u>Comments</u>
1. PKXA	A silane terminated polysulfone. This feature permits some end group cross-linking which improves solvent/moisture resistance and temperature capability.
2. HyE 1076E	A graphite/epoxy system alleged to be more moisture resistant than Narmco's 5208. Also supposed to be a higher elongation matrix than other 350°F (177°C) class epoxies.
3. HMF-351/76	Same as #2 except a woven fabric.
4. CPI-2272	A polyimide resin alleged to have equivalent or better moisture resistance and temperature capability than F178.
5. NCNS	Developed to replace the M4-720 base resin used in 350°F (177°C) class epoxies. It is fire retardant, generates little smoke, and is water resistant.
6. PMR-II	Second generation material claimed to have higher temperature capability than PMR-15.
7. X904B	A non-proprietary 350°F (177°C) epoxy system developed under USAF contract. Reputed to have low moisture absorption.
8. E788	An elastomer modified epoxy system.
9. LARC 160	A 550°F (288°C) polyimide supposed to have better handling and processing characteristics than PMR-15.
10. AS/3006	A graphite/polyphenylsulfone (Radel PPS) system which processes easily and has good water resistance. Main shortcoming is solvent resistance leading to stress-cracking.
11. DAPI	Diaminophenylindane. A thermoplastic with 500°F (260°C) service capability and which processes easily. Its solvent resistance is principal problem.

TABLE 1 (Continued)
CANDIDATE MATERIALS

<u>Material</u>	<u>Comments</u>
12. Pitch-based graphite fiber	Three grades are being developed, having nominal moduli of 55 msi, 75 msi, and 100 msi. This fiber is potentially very inexpensive.
13. Glass matrix composites	High temperature capability. Excellent dimensional stability. Water and solvent resistant. Not yet commercially available.
14. FP alumina fibers	Potential for low cost makes it a candidate to replace boron.
15. SiC/epoxy	Silicon carbide on a carbon substrate has properties equivalent to boron but has a much lower cost potential.
16. Phthalocyanine	A new matrix system being developed. It is alleged to have high toughness and good elevated temperature capabilities.
17. V378A	A polyimide system with improved wet high-temperature properties. Microcracking is supposed to be substantially reduced.
18. Thermid 600	Acetylene terminated polyimide system with 550-600°F (288-316°C) service capabilities.
19. XPL 1056	This vinyl polyester resin system cures very rapidly at relatively low temperatures and pressures. Preliminary tests indicated very good moisture resistance. The material also appears to form a better bond to aramid fibers than epoxy resins, leading to higher shear and compression properties.
20. High filament end graphite tow	Larger graphite tows now being developed reduce prepreg preparation costs.

TABLE 1 (Concluded)
CANDIDATE MATERIALS

<u>Material</u>	<u>Comments</u>
21. AFR800	An epoxy resin system developed under Air Force contract which has a long room temperature shelf life.
22. NR150B2	Probably the highest service temperature organic matrix system available. Very difficult to process.
23. RX-6450	N-cyanosulfonamide. An addition type resin that cures like conventional epoxies but offers better temperature capabilities and greater environmental resistance.
24. PSP 6002	This polystyrylpyridine resin is a heterocyclic aromatic polymer which appears to offer very good high temperature performance. It was developed in France.
25. Ryton	This polyphenylene sulfide material retains good mechanical property levels up to 300°F (149°C), has excellent chemical resistance, and is relatively easy to process.

much lower cost. The 5506 resin system was developed by AVCO as a 350°F (177°C) epoxy and was recommended by them for use with the SiC fiber.

The HyE 2034D material consists of Union Carbide's VSC-32 pitch-based graphite fiber in Fiberite's 934 epoxy resin system. The VSC-32 is a low cost 75×10^6 psi (517 GPa) modulus fiber which can favorably compete with boron in many applications.

The V378A resin is a 450°F (232°C) polyimide system which was developed by U.S. Polymeric and was of interest to many respondents to our mail and telephone inquiries. Initially, it was intended to characterize the resin on Celion 6000 graphite fiber with a polyimide (NR150B2) size but initial testing by U.S. Polymeric indicated that epoxy sized T300 produced better property levels with V378A. Rather than wait for further development work with other fiber finishes on Celion, it was decided to go ahead with T300 as the reinforcement.

The fifth material selected was HyE 1076J and consisted of Thornel 300 (15,000 filament tow) in Fiberite's new 976 epoxy, a 350°F (177°C) rated resin with better moisture resistance than the 934 system. Originally the fiber desired in this prepreg was Hercules' AS4 graphite in a 12,000 filament tow. This fiber, however, was not readily available at the time and in order to avoid a delay of uncertain duration, the T300 was substituted.

The last material tested was AVCO's 6535-1 graphite/epoxy prepreg system. This consisted of a 160,000 filament tow graphite fiber in a 350°F (177°C) class epoxy resin. Both components were AVCO products.

SECTION 3

TEST PROGRAM AND PROCEDURES

The laboratory efforts required during this program consisted of four generally sequential steps for each of the six materials characterized. These consisted of prepreg physical property characterization, laminate fabrication and specimen machining, laminate physical property characterization, and laminate mechanical and thermophysical property measurements. Each of the test methods and types of specimen used in the determination of these various properties, as well as the panel fabrication and specimen preparation procedures, are described in this section. Procedures or circumstances which were unique to a particular material are discussed in detail in the appropriate part of Section 4.

3.1 PREPREG PHYSICAL PROPERTY CHARACTERIZATION

The standard prepreg physical properties which were measured consisted of volatile content, resin content, and gel time. In addition, flow was measured on some of the materials and high pressure liquid chromatographic (HPLC) analyses were conducted on all but one of the prepregs. The specific test methods used to determine these properties are identified in Table 2 for each prepreg system. Detailed step-by-step procedures for each of the prepreg test methods listed in Table 2 are presented in Appendix B. The summarized prepreg properties themselves are presented in Section 4 for each specific material. These prepreg physical property characterizations were not intended primarily as a means of accepting or rejecting a particular batch of material. Rather, they were conducted to provide the reader with an indication of the normal property levels and variability encountered in purchased prepreg and also to provide a basis for the subsequent assessment of laminate properties obtainable from such prepreg.

TABLE 2
PREPREG PHYSICAL PROPERTY TEST AND SPECIFICATIONS

Prepreg Material	Test Specification Identification ¹			
	Volatile Content	Resin Content	Gel Time	Flow
T300/APR800	HD-SG-2-6006C (5.1.2); Hercules	HD-SG-2-6006C (5.2); Hercules	HD-SG-2-6006C(5.5) Hercules	HD-SG-2-6006C (5.3.2B); Hercules
SiC/5506	4.2.3.3 Adv. Comp. Des. Guide	4.2.3.2.1 Adv. Comp. Des. Guide	---	---
HyE 2034D	QCI-C-V-14 Fiberite	R15 Fiberite	G2 Fiberite	QCI-C-F-42 Fiberite
T300/V378A	QCI-C-V-14 Fiberite	R15 Fiberite	G2 Fiberite	---
HyE 1076J	QCI-C-V-14 Fiberite	R15 Fiberite	G2 Fiberite	---
6535-1	QCI-C-V-14 Fiberite	R15 Fiberite	G2 Fiberite	---

¹Each of the procedures identified in this table are presented in their entirety in Appendix B.

Reverse phase HPLC was used to separate the epoxy and polyimide resins into their constituent components. A 4.6 mm diameter by 25 cm long column packed with Zorbax ODS (by DuPont) was used in conjunction with a mobile phase of dioxane and water. A programmed concentration gradient for the mobile phase was selected for optimum peak separation and analysis time. In this program, the mobile phase started as 100 percent water to precipitate the resin at the head of the column. Increasing percentages of dioxane were added to separate and move the resin components through the column. Since reverse phase chromatography uses a non-polar support and a polar mobile phase, the more polar compounds elute first followed by less polar components as the mobile phase becomes less polar.

Samples for the prepreg physical property tests were obtained from each roll of prepreg tape and three specimens were used for each test. A complete tabulation of these prepreg test results is presented in Appendix B. All of the prepreg used in this program except for the T300/AFR800 was stored at -30°F (-34°C) when not in use and all of the laminates needed for the program were prepared prior to the expiration of the manufacturer's stated storage life of each specific material. In addition, a written record was maintained for each roll of prepreg which noted the cumulative total time the material was exposed to room temperature conditions during the period in which laminates were being fabricated from the tape. The T300/AFR800 material was stored at room temperature since this material was formulated to have extended room temperature storage life.

3.2 LAMINATE PROCESSING AND SPECIMEN FABRICATION

When laminates were to be made, the roll of prepreg was (except for the T300/AFR800 material) removed from the freezer and allowed to warm to room temperature without opening the sealed bag in which the prepreg was contained. This was done in order to eliminate the chance of moisture condensation directly on the prepreg material. After the prepreg had warmed thoroughly to room temperature, it was removed from its package and unrolled on a clean countertop. Pieces were cut from the tape in the required shape and size with a razor and after removing the release paper, carefully layed up in the desired stacking sequence for a particular laminate panel. This stack was then carefully rebagged and returned to the freezer for storage until lamination and curing. Normally ten or more laminates were layed up at the same time to minimize "out time" with the prepreg. When a laminate was to be cured, it was removed from the freezer and warmed to ambient before reopening its storage bag. The prepreg was then removed from the storage bag and incorporated into a

layup stack similar to that illustrated in Figure 1. This layup stack was assembled on the table platen in an autoclave. The detailed curing schedules for each specific prepreg material are presented in Section 4. After lamination and cure, machining diagrams were sketched onto the panel surfaces and individual specimens were cut out of the panels with a diamond cut-off wheel and finish machined to the required dimensions on a Tensile-Cut belt sander. In the case of the silicon carbide reinforced panels, the hardness of the fiber made final specimen machining so difficult that the laminates were finish cut to final dimensions on a special diamond cut-off wheel equipped with an accurately positioned movable table. Specimens from each panel were set aside for measurement of panel physical characteristics.

Most of the mechanical test specimens required doubling tabs in the grip sections. A 1/16-inch thick glass fabric reinforced phenolic laminate material was used for this purpose. Scotchply is specified in the Design Guide for tab material but it proved unsatisfactory for the elevated temperatures. Several adhesives were used to bond the tabs to the specimen. Originally Loctite 306 was used for all tab bonding. When multidirectional ply orientations, which required high loads, were introduced into the program; however, it was found necessary to switch to FM400 as a tab adhesive. M-Bond 200 was used as a tab adhesive on specimens which were humidity aged prior to testing because these specimens did not require high loads and this adhesive cured rapidly (three to five minutes) at room temperature, thereby minimizing specimen dryout. The FM400 was cured at 325°F (163°C) for one hour. The Loctite 306, when it was used, was cured for 15 minutes at 275°F (135°C). All tabs were clamped in place with spring clamps during adhesive cure.

3.3 LAMINATE PHYSICAL PROPERTY CHARACTERIZATION

Four different physical properties were measured on each laminate to insure acceptable laminate quality. These were

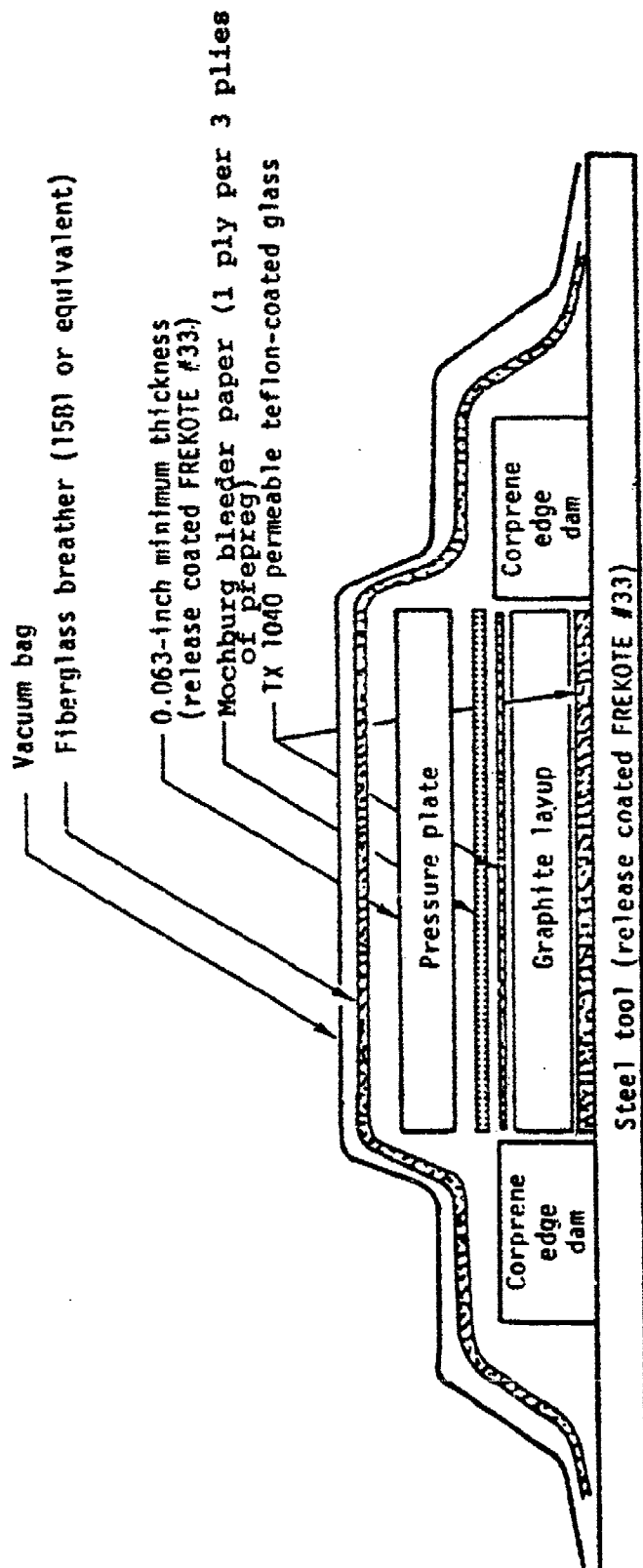


Figure 1. Typical Laminating Layup Stack.

specific gravity, resin content, fiber content, and void content. Each of the procedures used for these measurements is identified and discussed in the following paragraphs. The laminate physical properties obtained for each of the materials investigated are summarized in tables in Section 4 and are presented in their entirety in Appendix C.

3.3.1 Specific Gravity

Three specimens from widely scattered locations on each laminate were selected for specific gravity determinations. Specimen size depended upon both panel size and the number and size of mechanical test specimens required from the panel, but in general ranged from a minimum of 1/2" x 1/2" to a maximum of 1" x 3/4". The method used was ASTM D792, a weight-in-air/weight-in-water technique.

3.3.2 Resin Content

The same specimens which were used for specific gravity measurements were used for resin content determinations. The procedure used involved the digestion of the matrix resin in an acid solution at elevated temperatures. For the five epoxy matrix systems, the acid solution was 70% nitric acid at 145°F (63°C). For the polyimide matrix system (V378A), the digestion solution consisted of a mixture of 96% sulfuric acid and 30% hydrogen peroxide (80:20 volume ratio, respectively, in the mix) at 175°F (78°C).

3.3.3 Fiber Content

The fiber contents of the laminates were computed, as percent by volume, from the same data used for the resin content determinations. The computational procedure is illustrated in AFML-TR-67-243 and employed values for fiber and resin specific gravity reported by the respective manufacturers.

3.3.4 Void Content

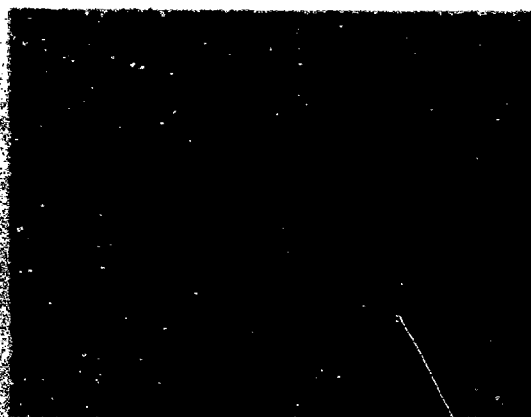
The void contents, just as the fiber contents, were computed, as percent by volume, from the same data obtained

in the resin content determinations. The computational procedure is described in ASTM D2734, method B. The result of this procedure frequently gives negative values for laminates having low void contents. This occurs because minor inaccuracies in the values used for resin, fiber, and composite specific gravities become significant at low void contents. A negative result was obtained for numerous laminates made in this program, even though photomicrographs did sometimes reveal the presence of low levels of porosity. Figure 2 illustrates typical laminate cross sections for each of the composite materials characterized.

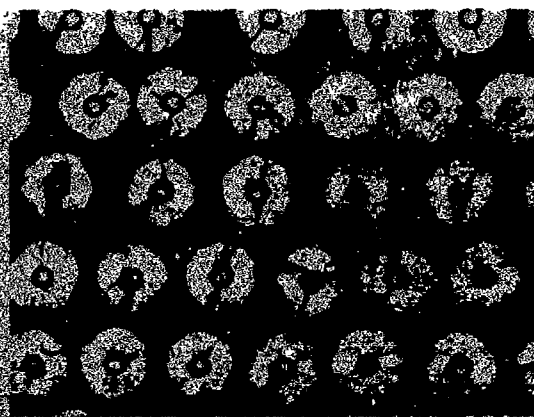
3.4 SPECIMEN CONDITIONING

Three different types of conditioning were involved in this program. The first was simply a dry dessicated storage of finished specimens at ambient temperature until they were to be tested. This provides a data base for the dry material to which both humidity aging data and data for other materials systems can be compared.

The second type of conditioning was the elevated and reduced test temperatures. In all of the mechanical testing except for specimens which were humidity aged, the specimens were soaked for one-half hour at the test temperature prior to loading. Thermal conductivity specimens were soaked at temperature for periods of from one to several hours in order to provide sufficient time for the test stack to reach thermal equilibrium before readings were taken. The thermal expansion and specific heat specimens were soaked for various periods of time at the endpoints of the test temperature brackets in order to permit stable baseline recordings to be achieved. These periods typically ran from five to 30 minutes in the specific heat tests to one-half to one hour in the thermal expansion tests. The glass transition temperature tests did not involve an isothermal soak since the specimen was heated at a constant rate throughout the test.



(a) T300/AFR800, 100X



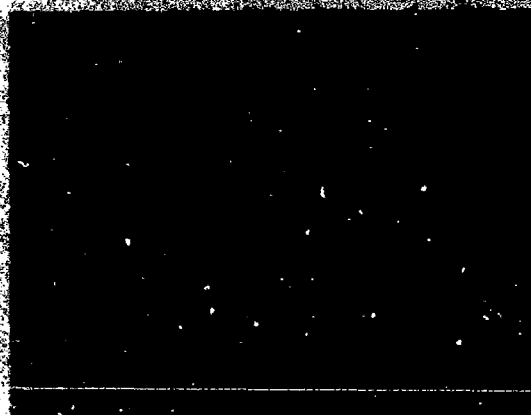
(b) Kevlar 49/AFR800, 100X



(c) Kevlar 49/AFR800, 100X



(d) T300/V350, 100X



(e) Kevlar 49/V350, 100X



(f) T300/V350-1, 100X

Figure 2. Typical Cross-Sections of Fabricated Composites.

The third type of conditioning was an elevated temperature, high humidity exposure. The specimens involved in these tests were exposed to conditions of 160°F and 100% R.H. until they either reached saturation, as evidenced by constant weight, or about 50% of their saturated weight gain. Specimens were removed from the humidity cabinets for weighing periodically to determine weight gain. The frequency of removal varied from material to material depending upon whether the aging was being carried to saturation or half-saturation and upon the rate and extent of moisture absorption by the particular matrix system being aged. The half-saturation agings, for example, typically required between 18 hours and nine days, depending upon the size of the specimen and the material. Normally two to six weighings were made during this period at various intervals. The fully saturated agings, on the other hand, required from one to 12 weeks to complete, again depending on specimen size and material. Specimens were removed from the aging cabinet and weighed between four and ten times at intervals of three to 14 days. After final removal from the humidity aging, the specimens were tested at both 72°F and at one of the elevated temperatures for which data on dry specimens were obtained. After removal from the humidity aging cabinet, the specimens were kept in a 72°F, 100% R.H. environment until tested (less than one-half day). During this period the specimens were exposed to ambient conditions for a maximum of about 45 minutes, during which time strain gages and gripping tabs were mounted on the specimens (interlaminar shear, short beam specimens of course, did not need this). The specimens tested at elevated temperature were placed in a preheated test oven and tested after a five to ten minute soak at the test temperature. The insertion of the specimens for elevated temperature testing into the grips in the test oven required less than one minute, during which time, the oven temperature fell about 50°F below its setpoint. The five to ten minute soak time was counted from the time the oven temperature returned to its

set point. The test oven required about five minutes to return to its set point. Hence, the humidity aged specimens which were tested at elevated temperature were actually in the test oven for a maximum of 10-15 minutes before testing. It is recognized that any elevated temperature soak of a "wet" composite produces a drying effect so that the test results are not actually representative of a truly "saturated" material. A compromise must be made, however, between the length of time required for a specimen to heat up to the test temperature and the rate at which a specimen dries out. Ideally, a steam test chamber would eliminate the requirement to make such a compromise. Few organizations have such a test chamber, however. The dryout which does occur during this period in the test oven results in a moisture concentration gradient through the thickness of the specimen, with the surfaces being "drier" than the interior. Several investigations^[1-6] have conducted measurements on various composite materials and developed analytical expressions, based on diffusion studies, which can be used to compute moisture content profiles in "wet" laminates exposed to elevated temperature dryout conditions. No attempt was made in this work to measure the degree of moisture loss which occurred during testing of the "wet" specimens.

With the T300/V378A material, the effect of time-at-temperature (350°F, 177°C) before testing was examined on 90° compression specimens which had been humidity aged to saturation. Two specimens were tested after 10 minutes and three were tested after 5 minutes at 350°F (177°C). The 10-minute soak produced an average strength of 17.0 ksi (117 MPa), while the 5 minute soak produced an average strength of 20.1 ksi (138 MPa). This would seem to indicate that the specimens after 10 minutes may have been nearer to the test temperature than after 5 minutes. As far as the effect of drying out is concerned, the 5 minute values should have a higher retained moisture level than the 10 minute values.

3.5 LAMINATE MECHANICAL AND THERMOPHYSICAL PROPERTY CHARACTERIZATION

A total of eight types of mechanical property tests were performed on the composite materials evaluated during this program; tension, compression, flexure, inplane shear, interlaminar shear, tensile creep, tensile stress-rupture, and tensile-tensile fatigue. In addition, four thermophysical properties were measured; specific heat, thermal conductivity, coefficient of thermal expansion, and glass transition temperature. Tables 3-6 summarize the test matrices for the various types of tests conducted in this program, indicating the number of specimens tested for each test and test condition.

It can be observed from Tables 3 and 4 that the test matrices for the static and dynamic mechanical tests were not the same for each of the six materials tested. Two basic changes were made during the program, each of which imposed a different requirement for various numbers of certain tests and ply stacking sequence on the composite systems subsequently tested. These changes affected only the static tensile and the creep and fatigue tests.

It was determined early in the program that there was very little interest in or use for, creep and fatigue data on unidirectional 0° or 90° laminate orientations. Rather, it was determined there was considerably more interest in data on a multidirectional layup consisting of something on the order of 50% 0° plies, 45% $\pm 45^\circ$ plies, and 10% 90° plies. Even though the stacking sequence, and amount and direction of each ply orientation may be unique to a particular application, there was considerably more interest expressed in creep and fatigue data on any multidirectional layup corresponding roughly to the composition expressed above than in 0° or 90° unidirectional data. Consequently, it was decided to discontinue creep and fatigue tests on the unidirectional

TABLE 3
STATIC MECHANICAL PROPERTY TEST MATRIX

Test Type	Test Material					
	T300/AFR800	SiC/5506	HyE2034D	T300/V378A	HyE1076J	6535-1
0° Tension ¹	20	20	20	20	20	20
90° Tension ¹	20	20	20	20	20	20
±45° Tension ¹	20	20	20	20	20	20
(0/±45/90) Tension ^{2,5}	0	15	15	15	15	5
(0/±45/90) Tension with hole ^{3,5,8}	0	5	5	5	5	0
(0/±45/90) Tension ^{3,6}	0	0	0	0	0	5
(0/±45) Tension ^{3,7}	0	0	0	0	0	5
0° Compression ¹	20	20	20	20	20	20
90° Compression ¹	20	20	20	20	20	20
0° Flexure ¹	20	20	20	20	20	20
90° Flexure ¹	20	20	20	20	20	20
Inplane Shear ¹	20	20	20	20	20	20
Interlaminar Shear ⁴	25	25	25	25	25	25

¹Five tests each at four different test temperatures.

²Five tests each at three different test temperatures except for 6535-1, in which case all five were at room temperature.

³All five tests at room temperature.

⁴Ten tests at room temperature, five tests each at other three test temperatures.

⁵Twenty-ply with stacking sequence (0,45,-45,0,0,-45,45,0,90,0)_S.

⁶Twenty-ply with stacking sequence (0,90,45,-45,0,0,-45,45,0,0)_S.

⁷Sixteen-ply with stacking sequence (0,45,-45,0,0,-45,45,0)_S.

⁸Specimens had a 0.1935 inch (4.91 mm) hole in center of gage section.

TABLE 4
DYNAMIC AND TIME DEPENDENT MECHANICAL PROPERTY
TEST MATRIX

Test Type	Test Material					
	T300/AFR800	Sic/5506	HyE2034D	T300/V378A	HyE1076J	6535-1
0° Tensile Creep/ Stress Rupture	18 ^{1,6}	---	---	---	---	---
90° Tensile Creep/ Stress-Rupture	27 ^{1,7}	---	---	---	---	---
+45° Tensile Creep/ Stress-Rupture	27	27	27	27	27	27
(0/+45/90) Tens. Creep/ Stress-Rupture ⁸	---	27	27	27	27	6 ^{1,3,5}
(0/+45/90) Tens. Creep/ Stress-Rupture ⁹	---	---	---	---	---	6
(0/+45) Tensile Creep/ Stress-Rupture ¹⁰	---	---	---	---	---	6
0° Tensile-Tensile Fatigue	30 ^{2,4,6}	---	---	---	---	---
90° Tensile-Tensile Fatigue	30	---	---	---	---	---
+45° Tensile-Tensile Fatigue	30	30	30	30	30	30
(0/+45/90) Tensile- Tensile Fatigue ⁸	---	30	30	30	30	15 ^{2,4,5}
(0/+45/90) Tensile- Tensile Fatigue with hole ⁸	---	15	15	15	15	---
(0/+45/90) Tensile- Tensile Fatigue ⁹	---	---	---	---	---	15
(0/+45) Tensile- Tensile Fatigue ¹⁰	---	---	---	---	---	15

¹Three tests per stress level.

²Five tests per stress level.

³Two stress levels per test temperature.

⁴Three stress levels per test temperature.

⁵One test temperature.

⁶Two test temperatures.

⁷Three test temperatures.

⁸Twenty ply with stacking sequence [0,45,-45,0,0,-45,45,0,90,0]_s

⁹Twenty ply with stacking sequence [0,90,45,-45,0,0,-45,45,0,0]_s

¹⁰Sixteen ply with stacking sequence [0,45,-45,0,0,-45,45,0]_s

TABLE 5
THERMOPHYSICAL PROPERTY TEST MATRIX

Test Type	Test Temperature ¹			
	-67°F	72°F	T ₃	T ₄
Specific Heat	3	3	3	3
0° Thermal Conductivity	3	3	3	3
+45° Thermal Conductivity	3	3	3	3
0° Thermal Expansion	3	3	3	3
90° Thermal Expansion	3	3	3	3
+45° Thermal Expansion	3	3	3	3
Glass Transition Temp. ² (dry)	3			
(wet)	3			

¹The two elevated temperatures varied, depending upon the matrix resin.

²Dry refers to the as-fabricated composite condition, while wet refers to the condition of the specimen after it has reached an equilibrium weight gain during humidity aging at 160°F and 100% R.H.

TABLE 6
TEST MATRIX FOR STATIC MECHANICAL PROPERTY
TESTS AFTER ELEVATED TEMPERATURE,
HIGH HUMIDITY AGINGS

Test Type	Saturation Level			
	50%		100%	
	Test Temperature		Test Temperature	
	72°F	T ₃ ¹	72°F	T ₃ ¹
90° Tension	5	5	5	5
90° Compression	5	5	5	5
Interlaminar Shear	10	5	10	5

¹This temperature varied depending upon the specific material.

0° and 90° orientations after completion of the work on the first material (T300/AFR800) and to substitute a multidirectional (0,45,-45,0,0,-45,+45,0,90,0)_s orientation instead. In addition, some specimens with this orientation were also to be prepared with a hole in the center of the gage section to obtain an indication of notch sensitivity. The resulting test matrix was maintained for the next four materials which were characterized (SiC/5506, HyE2034D, T300/V378A, and HyE1076J). At that point another change was made.

During the testing of the multidirectional specimens discussed above, it was noted that the specimens exhibited delamination along the edges at the mid-plane during tensile loading. The point at which this delamination occurred was not recorded until the testing of the last material but occurred at a stress level well below that needed to fracture the specimen. In fact, during fatigue testing, these delaminations were usually dramatically evident long before final failure, or, in the case of some specimens, termination of the tests for residual strength determinations.

The reason for this delamination was the development of tensile stresses, at the free edge of the specimen, normal to the plane of the specimen. These stresses, in turn, arise because of the relative position of the various ply orientations, and the differences in the Poisson's ratio of these different plies. A seemingly innocuous shifting of the position of the 90° plies, or the elimination of them altogether, can drastically change the normal free-edge stress levels in specimens such as those under discussion. Several authors have addressed this issue in the literature and an analysis of the orientations tested in this program and discussion of the effects of alternative ply stacking sequences is presented in Appendix A.

As a result of this consideration, two additional multidirectional orientations besides the original (0,45,-45,0,0,-45,45,0,90,0)_s orientation were added to the static and dynamic test matrix for the last material. In order to offset these additions, the number of tests to be run for each orientation was reduced, as indicated in Tables 3 and 4.

In addition to the number of specimens indicated in Tables 3-6, however, numerous instances were encountered where extra or replacement specimens had to be tested. These situations included instances where failures occurred in the tabbed grip areas rather than in the gage section, where instrumentation failures prevented full data acquisition or aborted a test, or simply occasions when anomalous results were obtained which dictated rechecking. Another source of extra specimen testing involved the creep and fatigue tests. In these tests it was found on several occasions that the stress levels initially selected produced premature failures. Consequently, the stress levels at which these tests were conducted were lowered and extra specimens tested so as to provide the full complement of results required. It will be noted in the summarized results in Section 4 that the number of specimens for which the average property values are reported varies from property to property. As discussed above, in some cases extra tests were conducted which raised the number of specimens above the original plan. In other cases, the behavior of the test specimen during test prevented the acquisition of one or more properties from that particular specimen. If, for example, the specimens underwent excessive elongation before failure, the strain gages were lost and ultimate elongation data were not obtained, even though strength, modulus, proportional limit, and Poisson ratio values were.

In the succeeding sections, descriptions of each of the test methods used to obtain the mechanical and thermophysical properties are presented. The summarized test results for each specific material system are presented in Section 4 and a complete tabulation of all of these test results is presented in Appendices D thru Q.

3.5.1 Tension

Tensile tests were conducted in general accordance with ASTM method D3039. The doubling tabs were a glass fabric/phenolic laminate material as discussed previously (Paragraph 3.2). The tensile tests were conducted at an extension rate

of 0.05 inch/minute (1.3 mm/minute) on an Instron Universal Testing Machine. All of the tensile strains were monitored with strain gages. This test procedure corresponds to ASTM method D3039 except for the tab materials. In the ASTM specification, the tab material called for is a non-woven 0°/90° Scotchply material 1/8 inch thick, while in this program a woven glass/phenolic material 1/16 inch thick was used satisfactorily.

Unidirectional 0° specimens were one-half inch (12.7 mm) wide while specimens with all other orientations (90°, +45°, or multidirectional) were one inch (25.4 mm) wide.

The tensile proportional limits were determined with the understanding that the proportional limit should represent the point at which a significant departure from linearity in the slope of the stress-strain curve, presumably indicative of damage to the specimen, occurs. This can produce a substantially different value than if one were to simply take the point of first deviation from linearity. The first deviation of the stress-strain curve from linearity on the 0° fiber orientations actually occurred at roughly one-third of the ultimate stress but at this point the slope of the curve increased rather than decreased. It is generally conceded that this phenomena is due to the behavior of the reinforcing graphite fiber since the same behavior is noted when testing bare graphite fibers. Consequently, this is not felt to indicate damage to the specimen. No decrease in the slope of the stress-strain curve was in fact noted for most of the 0°, 90°, or multidirectional fiber orientations prior to failure except for the high temperature tests on the 90° fiber orientations, and for this reason the proportional limit is reported as equivalent to the ultimate strengths. On some of the high temperature tests with the 90° fiber orientations, on all of the +45° fiber orientations and on all of the SiC/5506 specimens, a significant decrease in the slope of the stress-strain curves was observed below the ultimate strength. Whether this indicates the onset of real and significant damage, at least at the point of first departure, or simply the onset of nonlinear behavior, is a moot point.

The Poisson's ratio values were experimentally measured on all but the 90° fiber orientation. For this, it was computed from the relationship:

$$\nu_{21} = \nu_{12} \left(\frac{E_{22}}{E_{11}} \right), \text{ where}$$

ν_{21} = Poisson's ratio of a 90° fiber orientation,

ν_{12} = Poisson's ratio of a 0° fiber orientation,

E_{22} = Elastic modulus of a 90° fiber orientation, and

E_{11} = Elastic modulus of a 0° fiber orientation.

3.5.2 Compression

Compression tests were conducted in accordance with ASTM method D3410 except that the tab material was the same glass/phenolic material that was used in the tension tests. The compression tests were conducted at a speed of 0.05 inch/minute (1.3 mm/minute) on an Instron Universal Testing Machine. Prior to adoption by ASTM, this test method was widely referred to as the Celanese compression coupon test method.

Compression testing has traditionally been the subject of considerable controversy because of the various types of failure modes one can encounter. Not only can one obtain different failure modes with different types of test specimens and fixtures, but one can also experience different types of failure modes from the same type of test specimen and fixture. Inherent in the question of what is or is not a desirable failure mode is the requirement to avoid a gross specimen buckling-type of failure. This is different from what is called microbuckling, which consists of longitudinally oriented reinforcing fibers undergoing individual, localized buckling due to compressive stresses within the composite exceeding the capability of the resin matrix to support the fiber and maintain its axial alignment. Microbuckling is generally considered a legitimate compressive failure mode, while gross specimen buckling resulting from column instability is not. In order to eliminate the occurrence of column instability failures, specimens are designed with a slenderness ratio

sufficient to insure compressive failure before the load necessary to initiate column buckling is reached. Clark and Lisagor^[7] recently examined three different compressive test methods for graphite/epoxy composites. The effects of specimen size, support arrangement, and method of load transfer were investigated. Their conclusion was that no single test fixture appeared to be universally adequate. Each of the three techniques studied exhibited the potential to provide reliable compressive properties data in certain instances. A method using what is designed as an IITRI (Illinois Institute of Technology Research Institute) fixture was found to provide the most consistent data for unidirectional and quasi-isotropic laminates while a face supported fixture provided the most consistent results for $(+45/-45)_s$ specimens.

The compression test described in D3410 is similar to that described in Clark and Lisagor using the IITRI fixture. The principle difference is that the IITRI fixture utilizes flat wedge type grips while the grips in D3410 are conical wedges. One objection to this test method which has been raised is that the mated conical surfaces make line rather than surface contact during testing and that this produces frictional and alignment problems which affect the recorded results.^[8] Our experience has been that the frictional problems are minimal except when testing at reduced temperatures. In this case, frost accumulates on the fixture and the sliding surfaces do not slide freely, producing some spurious load recordings although use of a low temperature lubricant reduces the problem substantially. Misalignment has proven to be a problem, however. Although the specimens were designed to eliminate buckling instability, it has been found that buckling sometimes occurred anyway at stresses between 75% and 100% of ultimate. This behavior was indicated by strain reversals on the load-strain curve and by nonsymmetrical deformations present in failed specimens. The misalignment is induced by the nonuniform seating of the fixture cone in the conical socket. This non-uniform seating, in turn, results from the distortion imposed upon the split cone by the thickness of the specimen. The

principal advantage of the IITRI flat-wedge fixture over that called for in D3410 is the elimination of the wedge-socket seating and alignment problem.

We have found, however, that increasing the specimen thickness does reduce the amount of buckling which occurs with the conical wedge fixture of D3410. Apparently, the increased column stability obtained with greater thickness more than offsets alignment problems due to the increased distortion of the split cone produced by the specimen thickness. An increase in specimen thickness from 0.080 inch (2.0 mm) to 0.110 inch (2.8 mm) resulted in a reduction of the incidence of specimen buckling from 60% to only 15% of the total number of specimens tested, and the bulk of these remaining cases of buckling occurred at -67°F (-55°C), where frictional problems with the sliding surfaces are greatest. Consequently, it is believed that the use of sufficiently thick specimens, with a lubricated surface at temperatures below freezing, makes this test method quite satisfactory for specimens made with uni-directional tape prepreg. Another advantage to using this test method is that the data will be directly comparable to results obtained by other investigators and on other materials since the technique is widely used in the aerospace industry.

3.5.3 Flexure

Most of the flexural testing in this program was conducted using the four-point loading method described in the January 1971 issue of the Advanced Composite Design Guide.^[9] In this volume, a three-point technique is recommended for 0° fiber orientations and a four-point technique for 90° fiber orientations. It has been observed, however, that with a three-point loading scheme, one frequently encounters undesirable failure modes under the loading nose and subsequent anomalous strength values on high modulus composite materials with a 0° fiber orientation. For this reason, the four-point method was used, with a few exceptions, for both fiber orientations in this program. The reason for the exceptions is that shear failures were obtained on some of the materials, particularly

at elevated temperatures, when the four-point method was used. The ratio of shear stress to flexural stress is greatly reduced in three-point loading versus four-point loading, thereby reducing the likelihood of shear failure before flexural failure.

The four-point loading method described in the Design Guide is essentially identical to the ASTM flexure test (D790) except for the testing speed and the locations of the load application points in four-point loading. The Design Guide recommends a blanket testing speed of 0.05 inch/min. (1.3 mm/min.) while D790 recommends a speed which is dependent upon specimen thickness and span-to-thickness (L/d) ratio. For the thicknesses used in this program and a 32:1 L/d ratio, D790 calls for a testing speed of 0.11 inch/minute (2.8 mm/minute) for three-point loading and 0.13 inch/minute (3.3 mm/minute) for four-point loading, although a maximum variation of up to $\pm 50\%$ above or below these speeds is permitted. The spacing of the upper loading noses the Design Guide method is equal to one-half the span between the lower supports, while in D790 the spacing of the upper loading noses is equal to one-third of the span. The major difference is that the ratio of shear stress to flexural stress is 33% greater in the Design Guide arrangement than in the D790 arrangement.

While a wide range of specimen thickness is permissible according to D790, recent studies at Rockwell^[10] on graphite/polyimide laminates indicated that at both room temperature and 600°F (316°C) flexural strength decreased with specimen thickness in the 0.06-0.10 inch (1.5-2.5 mm) thickness range. Our specimens were 0.070-0.076 inch thick on all of the materials we tested except for the SiC/5506, in which case the specimens were 0.100 inch thick. All of the tests were conducted at a crosshead speed of 0.05 inch (1.3 mm)/minute and at a L/D ratio of 32:1.

3.5.4 Inplane Shear

The inplane shear data were computed from longitudinal and transverse load-strain measurements on a uniaxial

tensile test on a $\pm 45^\circ$ crossplied laminate. This method is in accordance with ASTM D3518.

The inplane shear stress-strain curve is obtained by a point-by-point conversion of the tensile load and strain data. This converts tensile stress-strain (σ - ϵ) information to shear stress-strain (τ - γ) data. The shear modulus (G) can then be obtained from the initial slope of the τ - γ curve. The shear modulus can also be computed directly from the tensile elastic modulus (E) and Poisson's ratio (ν) of the $\pm 45^\circ$ specimen using the basic relationship,

$$G = \frac{E}{2(1+\nu)} .$$

3.5.5 Interlaminar Shear

Interlaminar shear is another property for which no simple or problem-free test exists. The most widely used test is the short beam shear test described in ASTM D2344. Another test is the opposed double notch specimen with side supports and a third test utilizes torsional loading of a rod but requires special fixturing. Each of these tests is subject to certain objections. The notched specimen is known to have high stress concentrations at the notch edges. The torsional specimen is not felt to have a straight line stress distribution at the higher stresses even though this assumption is made in computing the failure strength. The short beam specimen produces high strength values because of its short span and the compressive stresses introduced by the loading nose and supporting points. The stress concentrations and complex stress states present in the short beam specimen are aggravated by the use of a thinner specimen than that illustrated in D2344, a practice common to nearly everyone who conducts this test. Whitney^[11] has found that short beam shear specimens tested at a 4:1 span-to-thickness ratio produce higher strengths in 0.125 inch (3.2 mm) thick specimens than in the 0.250 inch (6.4 mm)

thickness recommended by D2344. He further feels that common failure modes for specimens of this type, particularly in thinner sections, is not normally in interlaminar shear at the midplane, but rather near the top of the specimen and due to a complex interacting stress state. An alternative test method for interlaminar shear, which has produced clear mid-plane shear failures at stress levels near those achieved with a 0.250 inch (6.4 mm) D2344 specimen, has been investigated by Whitney. It consists of a four-point bending test with a 16:1 span-to-thickness ratio for graphite composites. The upper loading noses are spaced half as far apart as the two lower supports. It is felt that the mid-plane stress state is simpler and more nearly pure shear on this type specimen than on the short beam specimen and that so long as the ultimate failure mode is indeed a mid-plane shear failure, one generates realistic shear strength values. The only problem which has been encountered with this test is that ductile matrices (i.e., polysulfone) produce tensile failures on the lower surface before shear failure occurs at the mid-plane.

In spite of the admitted shortcomings with the short beam shear test using specimens thinner than 0.250 inch (6.4 mm), it was decided in this program to use a thin short beam shear specimen for interlaminar shear because it would better enable the generated data to be compared to other composite material data.

3.5.6 Tensile Fatigue

Fatigue tests were conducted on the fiber orientations indicated in Table 4. Where 30 specimens are indicated, 15 tests were conducted at room temperature and 15 at elevated temperature. Where only 15 specimens are indicated, all were conducted at room temperature. Each group of 15 was subdivided into three groups of five, each of which was tested at a different maximum stress level. Five replications were run for most conditions. In some cases, however, the 15 specimens were distributed differently due to an effort to avoid lifetimes that were either too short ($<5,000$ cycles) or too long ($>2 \times 10^6$).

cycles). In these cases, data were obtained at more than three stress levels and less than five specimens were tested at some of the stress levels. The same type of specimen was used for fatigue as was used for tensile tests. All of the tests were constant load amplitude at a frequency of 10 Hz with the minimum stress equal to one-tenth the maximum stress. The specimens were cycled to a maximum of 10^7 cycles, at which time, if no failure had occurred, they were removed and tested for residual tensile properties. All residual property tests were conducted at 72°F, regardless of the temperature at which the specimens were fatigue loaded.

The fatigue lifetimes (number of cycles) reported in Tables 17, 31, 44, 58, 71, and 86 represent log-mean values of the individual specimen values for each stress level. Similarly, the straight lines plotted through the individual data points in Figures 20, 21, 22, 38, 39, 40, 55, 56, 57, 71, 72, 73, 87, 88, 89, 104, and 105 represent a least squares fit of the maximum cyclic stress versus log (cycles to failure), with maximum cyclic stress considered the independent variable (x) and log (cycles to failure) considered the dependent variable (y) in the least squares linear equation $y = a + bx$.

The fatigue tests were carried out on MTS, closed-loop, electrohydraulic, servo-actuated testing machines. Specimen gripping was by means of wedge-type Instron grips. The grips are locked into place on the loading ram and load cell to insure constant alignment. Axial and concentric alignment of the ram and load cell was verified with a dial gage to within 0.001 inch and grip alignment was insured by the use of a specially machined straight aluminum bar in place of a specimen. Spacers were utilized to center the one-half-inch wide 0° specimens in the one-inch wide jaws and periodically, a specially strained gaged specimen was placed in the grips and the strains on opposite sides and edges monitored during loading to insure that eccentric loading was held below 1 percent.

Both room and elevated temperature tests were conducted in Instron circulating air environmental test cabinets. Temperature control in elevated temperature tests was maintained with Instron oven proportional temperature controllers with chromel/alumel thermocouples positioned directly adjacent to the specimen gage section.

An additional thermocouple was taped against the specimen surface in the center of the gage section to monitor specimen temperature. This was done because fatigue loading of specimens with off-axis ply orientations results in the generation of internal heat due to large repetitive deformations. Specimen surface temperatures as much as 25-30°F (14-17°C) greater than surrounding air temperature have been observed on +45° layups on the materials tested in this program. On the multidirectional layups (0/+45/90), specimen surface temperatures as much as 60°F (33°C) above surrounding air temperature have been measured.

3.5.7 Tensile Creep

Creep tests were conducted on the fiber orientations indicated in Table 4. Where 18 specimens are indicated, nine tests were conducted at each of two elevated test temperatures. Where 27 specimens are indicated, nine tests were conducted at each of three test temperatures (room temperature and two elevated temperatures). In each of these cases the nine-specimen groups were further subdivided into three groups of three specimens each and each of these tested at a different stress level. Where only six specimens were indicated, all tests were conducted at room temperature. Each of these groups of six were subdivided into two groups of three and these were then tested at two different stress levels.

The same specimen design used in tensile testing was used for the creep tests. Creep strain measurements were recorded using one-inch long strain gages and were carried out to a maximum of 500 hours, at which time, if a specimen had not

fractured, it was unloaded and creep recovery measurements recorded for a period of three hours. Each of these surviving specimens was then tested for residual tensile properties at 72°F. It will be noted that the creep recovery data are not included in the tabulated summaries of Section 4. The recovery data are presented, however, in Appendix J.

The creep tests were carried out on Arcweld creep frames. Each frame has the capacity, through a 20:1 counter-balanced lever arm, of putting loads of up to 12,000 lbs. on the test specimen. Each frame is also equipped with an electric timer and automatic shutoff switch, which monitors the total creep time as well as time to failure. Each frame also has an electrically driven load weight elevator and self-aligning couplings.

Specimen gripping was by means of serrated face jaw type grips. The 90° and $\pm 45^\circ$ orientations were held in grips where the serrated grip faces were tightened against the loading tab material by means of set screws. The 0° and (0/ $\pm 45^\circ$ /90) orientations were held in wedge-type jaw grips.

Elevated temperature creep tests were conducted in short tube-furnaces (Figure 3).



Figure 3 . Short Tube-Furnace Used in Elevated Temperature Creep Tests.

With these short furnaces (four inches long and one and one-half inches diameter tube), only the gage section of the specimen was in the heated zone. Temperature control on these tube furnaces was maintained with a thermistor actuated, time-proportioning controller employing a zero crossover switching triac, and transient fluctuations were less than $\pm 3^{\circ}\text{F}$ around the setpoint. The temperature controlling thermistor was mounted on the side of the one inch wide test specimens and the specimen centered in the uniform temperature region of the furnaces. Additionally, three thermocouples were attached to the specimen, one next to the thermistor and the other two at a distance of one-half inch on either side of the thermistor to insure that the thermistor was at the optimum location. Figure 4 presents a typical temperature profile of the tube furnaces used for these tests. It can be seen that the central two-inch portion of this type tube furnace maintains a relatively "flat" temperature profile which is within $\pm 5^{\circ}\text{F}$ of the setpoint. Specimens were stabilized at the test temperature for at least two hours before the load was applied.

Strain measurements were obtained from one-inch long strain gages mounted on the specimen surfaces and wired into a Vishay model P-350A digital strain indicator through a Vishay model SB-1 ten-channel switch and balance unit. Compensation for thermal expansion during elevated temperature tests was achieved by utilizing a compensating gage on a short section of unstressed specimen material taped to the gage section of the actual test specimen. The output from this compensating gage was fed into an adjacent leg of a half-bridge circuit.

Many of the creep specimens were tested in a series loading arrangement of up to three specimens in order to increase the rate of data acquisition. Figure 5 illustrates such an arrangement. In cases where one of the specimens in a series broke prior to the 500-hour termination point, the remaining specimens were replaced and new tests conducted.

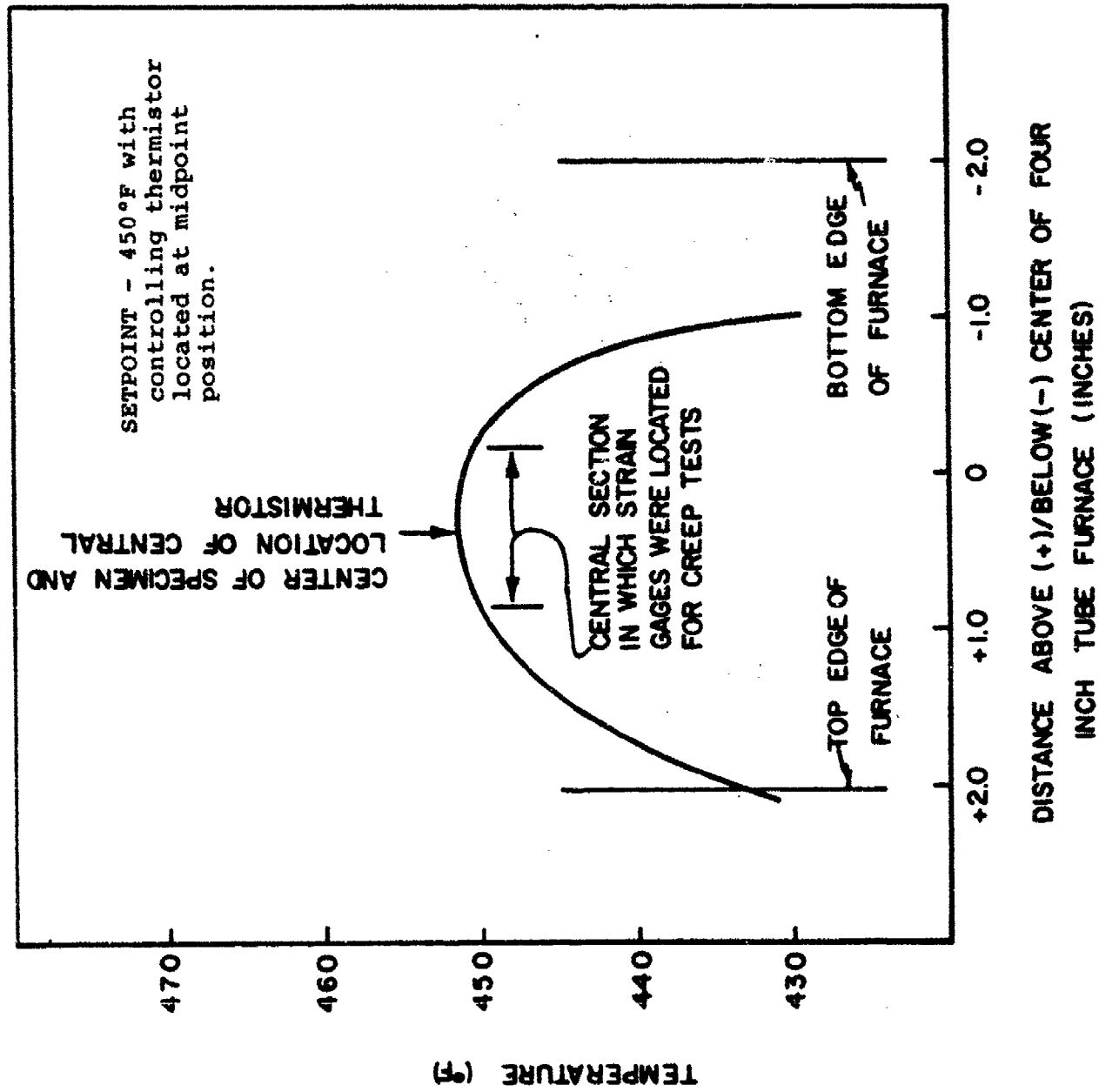


Figure 4. Typical Temperature Profile of Four-Inch Tube Furnaces.



Figure 5. Stacking Arrangement for Testing Three Creep Specimens Simultaneously.

It will be noted in the tables in the text, as well as in Appendix J, that many creep specimens failed on loading even though the applied stress was less than the strength obtained in the static test at the same temperature. The only factor to which this can be attributed is that the creep load was applied at a considerably more rapid (though not instantaneous) rate than the load applied during the static test. The reason for this is that the load pans on the creep frames are raised and lowered by a motor driven elevator, which operates much more rapidly than the 0.05 inch (1.3 mm)/minute rate utilized during static testing.

3.5.8 Tensile Stress Rupture

Stress rupture data were obtained from the same specimens used for the creep tests, the only difference being that time-to-failure rather than strain as a function of time was the measured variable of interest.

3.5.9 Specific Heat

Specific heat was measured with a Perkin-Elmer DSC-2 differential scanning calorimeter. This technique compares the rate of heat input required to maintain a constant rate of temperature rise in an unknown sample to that required to maintain the same rate of temperature rise in a known reference material.

The tests conducted in this program utilized sapphire as a reference material for tests at room temperature and above and benzoic acid for subambient tests. Samples consisted of a single ply of cured prepreg material. A small (10 mg maximum) circular piece was cut from the single ply of material. The test was conducted by equilibrating both sample and reference material at a temperature about 25°C (45°F) below the temperature at which a specific heat value is desired. Both are then heated at a rate of 10°C (18°F)/min. to a temperature about 25°C (45°F) above the measurement temperature and re-equilibrated at this new temperature.

Relative heat capacity values were measured on the ordinate scale of a strip chart recorder for both the sample and reference material. Specific heat of the sample is computed from:

$$C_{p,s} = \left(\frac{W_r}{W_s} \right) \left(\frac{D_s}{D_r} \right) C_{p,r}$$

where:

$C_{p,s}$ = specific heat of the sample
 $C_{p,r}$ = specific heat of the reference

W_s = weight of sample
 W_r = weight of reference

D_s = displacement of sample curve from baseline
 D_r = displacement of reference curve from baseline

The displacement of the respective curves from the baseline are illustrated in Appendix L, which also illustrates the treatment of a sloping baseline and a sample calculation.

3.5.10 Coefficient of Thermal Expansion

Thermal expansion was measured using a Perkin-Elmer Model TMS-2 Thermomechanical Analyzer (TMA). The TMA instrument has been specially modified to isolate it from external vibrations and has been fitted with a special chamber to house the sensitive electronic components in an isothermal environment. With these modifications, the instrument is capable of coefficient of thermal expansion (CTE) measurements as low as $10^{-7}/^{\circ}\text{C}$. Without these modifications, at least one order of magnitude sensitivity is lost.

The instrument basically measures the change in one dimension (i.e., length) of a material, as a function of temperature. For low CTE materials (less than $10^{-5}/^{\circ}\text{C}$) it is important for the test sample to have its ends carefully machined to a flat and parallel condition. A free-floating probe, attached to a linear variable differential transformer (LVDT), rests on the test sample, contained within a stationary sample tube. A furnace can be raised or lowered around the sample tube. A thermocouple is located as close as possible to the sample for temperature measurement independent of the furnace control.

The test is time-consuming since the sample and system must be brought to thermal equilibrium before the measurement is made. This requires from one to seven hours, depending on the temperature level and sensitivity level at which the test must be conducted. For materials with low CTE values, the system must be calibrated by conducting a run without a sample. The change in probe position must be subtracted from that measured with the sample in place in order to obtain an accurate value for the sample alone. This is necessary because of sensitivity of mechanical linkages in the system to temperature changes. As CTE increases this component becomes negligible.

The CTE values reported in Section 4 for the various materials were obtained by equilibrating the sample at a temperature 40°C below the temperature at which a value

was desired, and heating it to an equilibrium condition at a temperature 40°C above the desired temperature. The difference in recorded probe position for the two equilibrium positions is converted to a change in sample length (ΔL) and for the 80°C temperature change (ΔT), a CTE value is computed from the standard equation:

$$\alpha = \frac{\Delta L}{L_0 \Delta T}$$

where: α = CTE

ΔL = change in sample length

L_0 = original sample length

ΔT = change in temperature.

3.5.11 Thermal Conductivity

Thermal conductivity was measured in the direction normal to the laminate surface for both unidirectional and $\pm 45^\circ$ fiber orientations. A comparative technique was employed in which the sample is sandwiched between two identical reference materials of known conductivity. These, in turn, are held firmly between a heater and a heat sink. The heat flux through this stack establishes a temperature gradient which is measured with thermocouples placed on the upper and lower surfaces of both reference plates and the specimen plate in small precisely machined grooves. Radial heat flow to and from the test stack is minimized with a cylindrical guard heater in which a linear temperature gradient, closely matching that of the test stack, is maintained. A Dynatech Model TCFCM-N20 thermal conductivity instrument was used for these measurements. Data points were taken at approximately equal temperature intervals over the range of interest and a "best-fit" curve (or straight-line) plotted through these data points. The reported values in Section 4 were taken from these plotted curves at the specific temperatures. The maximum scatter of the individual data points on either side of the plotted curves was about $\pm 15\%$ of the reported values.

3.5.12 Glass Transition Temperature

Glass transition temperatures (T_g) were measured with a DuPont Model 981 Dynamic Mechanical Analyzer (DMA).

A schematic diagram of the DMA system is shown in Figure 6. The mechanical portion of the system consists of two parallel balanced sample support arms made of stainless steel, and free to oscillate around flexure pivots. The arm-pivot system is constructed in such a way to give it a very low natural free oscillating frequency (less than 3 Hz).

The sample, in the form of a rectangle, is clamped between the arms as shown to form a compound resonance system, the resonant frequency of which is dependent almost entirely (because of the low natural resonant frequency of the arm-pivot system) on the configuration and modulus of the sample. In oscillation, the sample is deformed as illustrated by the geometry in Figure 7. In the equilibrium position, before oscillation, the sample, the centerlines of the two arms, and an imaginary line connecting the centers of the two flexure pivots form a rectangle represented by the broken lines.

If the compound resonance system is deflected away from the equilibrium position to a new position (represented by the solid lines in Figure 7). the two ends of the sample remain parallel to each other and perpendicular to the arms. The center of gravity of the sample and of the arms, however, translate to new positions. During each cycle the sample is subjected to an alternating flexural deformation. The solution for the dynamic equation of motion for the system gives the relationship between Young's modulus and frequency:

$$E = \frac{(4\pi^2 f^2 J - K)}{2W \left[\frac{L}{2} + D \right]^2} \left[\frac{L}{T} \right]^3, \quad \text{where}$$

E = Young's modulus (Pa),

f = DMA frequency (Hz),

J = Moment of inertia of arm ($\text{kg}\cdot\text{m}^2$),

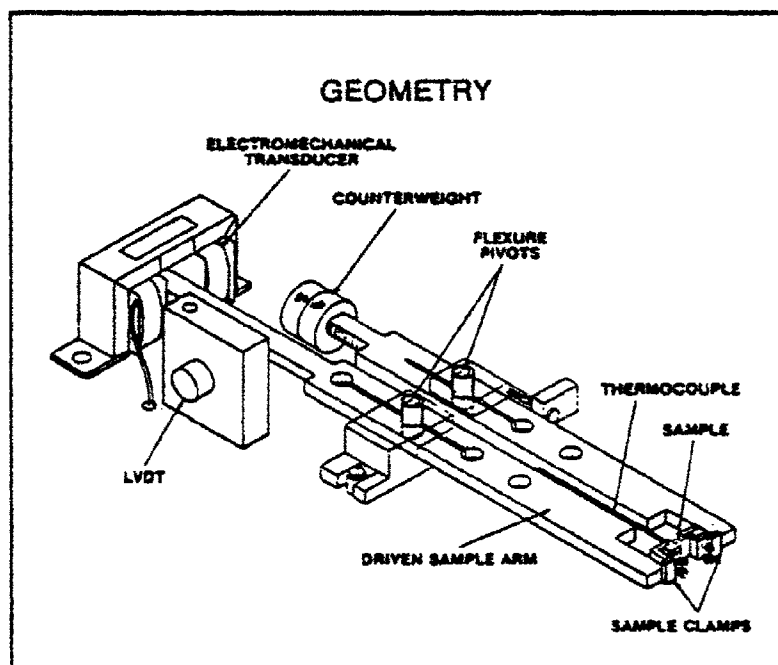


Figure 6 . Test Geometry for DuPont 981 Dynamic Mechanical Analyzer (DMA).

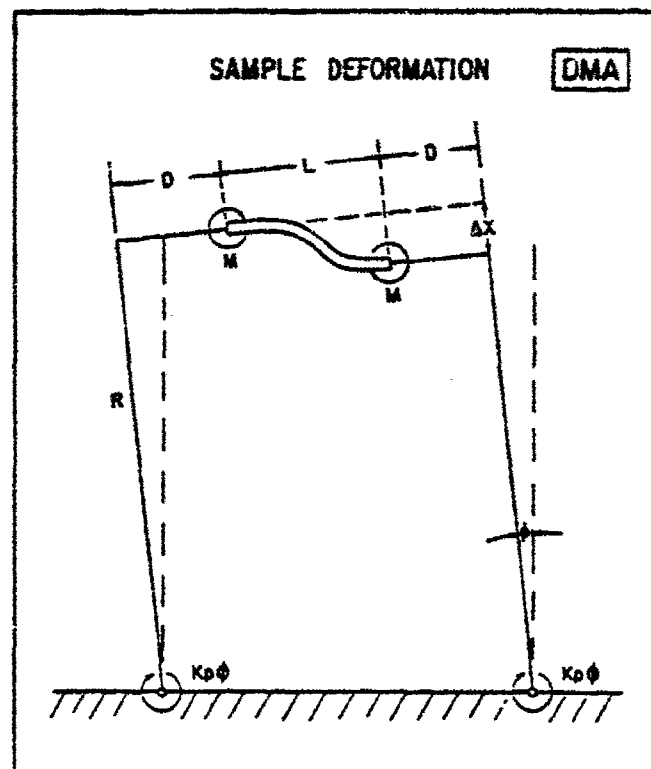


Figure 7. Sample Deformation in DuPont 981 DMA Apparatus.

K = Spring constant of pivot (N·m/rad),
 D = Clamping distance (m),
 W = Sample width (m),
 T = Sample thickness (m), and
 L = Sample length (m).

Sample loss factor, η , is calculated from

$$\eta = \frac{CV}{f^2}, \quad \text{where}$$

V = DMA Damping Signal (mV),
 f = DMA Resonant Frequency (Hz), and
 C = System Constant ($\sim 0.25 \text{ Hz}^2/\text{mV}$).

To make a measurement, a sample of known dimensions is clamped between the two sample arms. The sample-arm-pivot system is oscillated at its resonant frequency by an electromechanical transducer. The frequency and amplitude of this oscillation are detected by an LVDT positioned at the opposite end of the active arm. The LVDT provides a signal to an electromechanical transducer, which in turn keeps the sample oscillating at constant amplitude. Sample resonant frequency (measured to 0.01 Hz) and damping (measured to 0.1 dB) signals are supplied to the temperature programmer/recorder where they are graphically recorded as a function of the measured sample temperature or time. Young's modulus for the sample can be obtained from resonant frequency by using the relationship in the Equation and loss factor can be obtained from the Equation.

In this program, T_g values were defined as that temperature at which the loss modulus is maximum. Loss modulus, in turn, is defined as

$$E' = \frac{E}{\eta}, \quad \text{where}$$

E' = loss modulus,
 E = Young's modulus (from the first equation), and
 η = loss factor (from the second equation).

Specimens were run both "dry" and "wet", the "wet" condition implying that the sample was humidity aged at 160°F and 100% R.H. to an equilibrium weight gain prior to the determination. Unfortunately, there was no way to prevent the "wet" specimen from drying somewhat during the test. Hence, the specimen was no doubt at some moisture content less than saturation when the indicated T_g was observed. Nonetheless, the "wet" values were lower than the "dry" values in five of the six cases, indicating a definite softening due to whatever moisture level still remained in the sample. In the one exception, the T300/V378A system, the composite gained weight during moisture aging very rapidly compared to the epoxy systems, although the total weight gain was only slightly higher. It would not be unreasonable to assume that, when heated, this material would lose absorbed moisture much more rapidly than the epoxy systems also. This, coupled with the fact that the T_g value for the V378A resin is substantially higher than those measured for epoxies (by 200-300°F) would make it reasonable to speculate that the so-called "wet" V378A sample has completely dried out by the time its T_g is reached, thereby resulting in identical T_g values being determined for both the "dry" and "wet" samples.

SECTION 4

SUMMARIZED COMPOSITE DATA

This section presents tabulated summaries of all the data generated for each composite system evaluated during the program. Also presented are the averaged stress-strain, creep, and fatigue S-N curves for each of the systems.

In addition to the summarized data and averaged mechanical property curves, pertinent observations made during the characterization of each material are discussed.

4.1 T300/APR800

The matrix resin in this system was developed under USAF contract by the Aerotherm Division of Accurex Corporation. [12,13] The objective was "to achieve state-of-the-art performance (350°F [177°C]) from graphite fiber reinforced composites coupled with prolonged prepreg flow life under ambient shop conditions." This was basically achieved by utilizing aromatic diamine curing agents with "attenuated reactivity and limited solubility in the resins."

The resin was prepared according to the Aerotherm recipe by Hexcel (Dublin, California) and was also prepregged by Hexcel.

Tables 7 through 18 present the data generated for this graphite-epoxy composite system. Figures 8 through 22 illustrate the stress-strain, fatigue, and creep behavior of this material as well as the effects of humidity aging upon selected composite properties.

TABLE 7
PROCESSING CONDITIONS FOR T300/AFR800 COMPOSITE LAMINATES

Composite Processing Information	
Material System - T300/AFR800	Graphite/Epoxy
Fiber - T300/ Matrix - AFR800 ¹	
Maximum Rated Temperature - 350°F	Prepreg by - Hexcel
Laminate Processing Schedule	
<p>Layup Procedure: The prepreg was stored in a closed wrapper at room temperature. Prepreg was removed from wrapper and plies cut to desired size using a razor knife. Plies were stacked in the desired sequence (release paper removed from each ply). The stack was placed in the autoclave according to the layup system illustrated in Figure 8. The corprene edge dam serves to restrict fiber flow.</p>	
<p>Cure Schedule: Apply full vacuum and hold for one hour at room temperature. Heat to 275°F in 60 + 5 minutes under at least 10 inches Hg vacuum. Hold at 275°F for 50 minutes less than the gel time.² Apply 75 psi and vent vacuum at the end of this hold time. Heat to 325°F in 30 + 5 minutes. Hold at 325°F for four hours. Cool under pressure to 120°F.</p>	
<p>Postcure Schedule: The panels were placed, unrestrained, in an oven at room temperature. The oven was brought to 375°F at rate of about 5°F/min. After a four-hour hold at 375°F, the oven was turned off. When the oven was cooled to near room temperature, the panels were removed.</p>	

¹ Resin development and composition is described in AFML-TR-77-158.

² This cure schedule is given in AFML-TR-77-158, where it is stated that the key processing parameter is the point of pressure application at the 275°F hold temperature. This, in turn, depends upon the gel time. We have found that gel time has depended upon the method used for the measurement. The Hercules method (HD-SG-2-6006C, para. 5.5), in which a prepreg sample is rolled up in aluminum foil, gave a gel time of 140 minutes. The Fiberite method (Fisher-Johns melting point apparatus) gave a gel time of 87 minutes.

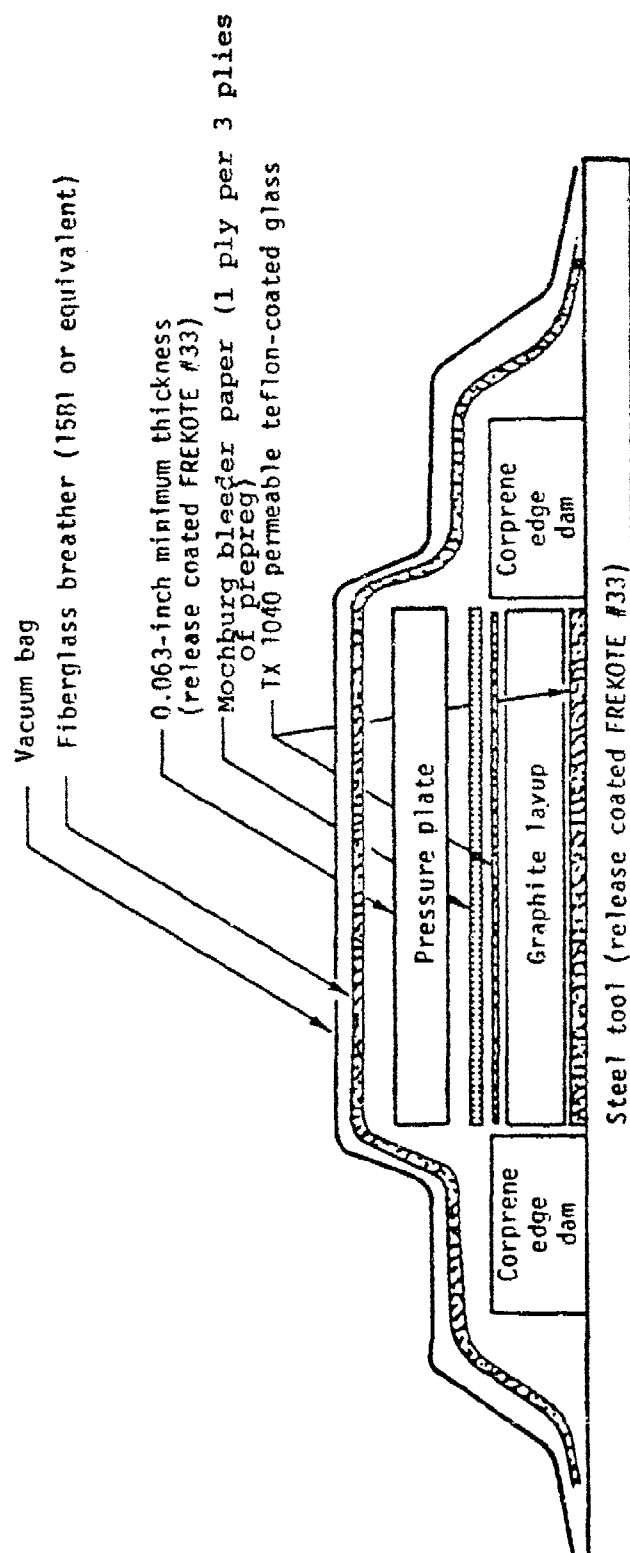


Figure 8. Layup System for AFR-800 Laminates.

TABLE 8
PREPREG AND COMPOSITE PHYSICAL PROPERTIES

Composite Physical Property Information				
Material System - T300/AFR-800			Graphite/Epoxy	
Fiber - T300 Matrix - AFR-800				
Maximum Rated Temperature - 350°F			Prepreg by - Hexcel	
Prepreg Physical Properties				
(Property)	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
Volatile Content- 0.11%		0.07-0.18	HD-SG-2-6006C	(5.1.2)
Resin Content- 40.1%		39.1-41.5	HD-SG-2-6006C	(5.2)
Resin Flow- 15.51% ²		15.49-15.53	HD-SG-2-6006C	(5.3.2B)
No. of Rolls Involved- 1				
No. of Batches Involved- 1			Hercules test methods	
Laminate Physical Properties ¹				
	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
No. of Panels- 36				
Fiber Content- 69.1% by vol.	3.7	61.1-77.0	Acid Digestion AFML-TR-67-243	
Resin Content- 26.6% by wt.	2.8	23.5-33.1		
Void Content- 0.2% by vol.	0.8	0-4.4	D2734	ASTM
Laminate Sp. Gr.- 1.60	0.04	1.54-1.71	D792	ASTM
Fiber Sp. Gr.- 1.70		As reported by manufacturer.		
Matrix Sp. Gr.- 1.24		As reported by manufacturer.		
Thickness per ply-0.0052 inch			---	---

¹The properties reported here represent averages for all panels of this material used throughout the program.

²After 30 days storage at R.T., flow was remeasured and found to have increased to 19.32%.

TABLE 9
TENSILE PROPERTIES OF T300/AFR800 COMPOSITE LAMINATES

Composite Material Properties					
Material System - T300/AFR 800		Prepreg by - Hexcel		Graphite/Epoxy	
Fiber - T300		Matrix - AFR 800			
Maximum Rated Temperature - 350°F(177°C)		Laminate Sp. Gr. - 1.61			
Resin Content - 25.0% by wt.		Nominal Ply Thickness - 0.0051 inch			
Fiber Content - 67.6% by vol.		No. of panels from which specimens were tested in this table - 10			
Void Content - ~0% by vol.					
Thickness of each type specimen: 0° - 6 ply		90° - 15 ply			
TENSION: 0°					
		-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
F_x^{tu} [ksi] (MPa)		[186.7] (1286)	[179.6] (1237)	[193.9] (1336)	[173.5] (1195)
Std. Dev. [ksi] (MPa)		[15.8] (109)	[17.0] (117)	[17.4] (120)	[21.0] (145)
Range [ksi] (MPa)		[172.2-212.1] (1187-1461)	[169.6-205.6] (1169-1417)	[174.3-213.3] (1201-1470)	[159.7-200.9] (1100-1384)
No. of Specimens		5	5	5	5
F_x^{tpl} [ksi] (MPa)		[186.7] (1286)	[179.6] (1237)	[193.9] (1336)	[173.5] (1195)
Std. Dev. [ksi] (MPa)		[15.8] (109)	[17.0] (117)	[17.4] (120)	[21.0] (145)
No. of Specimens		5	5	5	5
F_x^t [ksi] (MPa)		[20.87] (143,800)	[18.69] (128,800)	[20.40] (140,600)	[19.87] (136,900)
Std. Dev. [ksi] (MPa)		[0.49] (3380)	[0.98] (6750)	[0.44] (3030)	[0.43] (2960)
No. of Specimens		5	5	5	5
ϵ_x^{tu} [in/in] (µcm/cm)		8520	8700	9040	8380
Std. Dev.		572	648	620	870
No. of Specimens		5	5	5	5
ν_{xy}^t		0.319	0.312	0.307	0.355
Std. Dev.		0.010	0.034	0.022	0.037
No. of Specimens		5	5	5	5
Test Method Reference		ASTM D3039			
TENSION: 90°					
F_y^{tu} [ksi] (MPa)		[4.69] (32.3)	[4.58] (31.6)	[4.68] (32.2)	[5.42] (37.3)
Std. Dev. [ksi] (MPa)		[1.27] (8.75)	[1.01] (6.96)	[0.50] (3.45)	[0.67] (4.62)
Range		[2.80-6.31] (19.3-43.5)	[3.20-5.75] (22.0-39.6)	[4.33-5.56] (29.8-38.3)	[4.80-6.53] (33.1-45.0)
No. of Specimens		5	5	5	5
F_y^{tpl} [ksi] (MPa)		[2.89] (19.9)	[4.17] (28.7)	[3.79] (26.1)	[2.86] (19.7)
Std. Dev. [ksi] (MPa)		[1.84] (12.7)	[0.65] (4.48)	[1.21] (8.33)	[1.17] (8.06)
No. of Specimens		5	5	5	5
F_y^t [ksi] (MPa)		[1.63] (11,230)	[1.48] (10,200)	[1.36] (9370)	[1.19] (8200)
Std. Dev. [ksi] (MPa)		[0.07] (480)	[0.04] (276)	[0.04] (280)	[0.05] (351)
No. of Specimens		5	5	5	5
ϵ_y^{tu} [in/in] (µcm/cm)		2870	3110	3510	4910
Std. Dev.		760	720	330	897
No. of Specimens		5	5	5	5
ν_{yx}^t		0.025 ¹	0.025 ¹	0.020 ¹	0.021 ¹
Test Method Reference		ASTM D3039			

¹ Computed using elastic modulus and longitudinal Poisson's ratio.

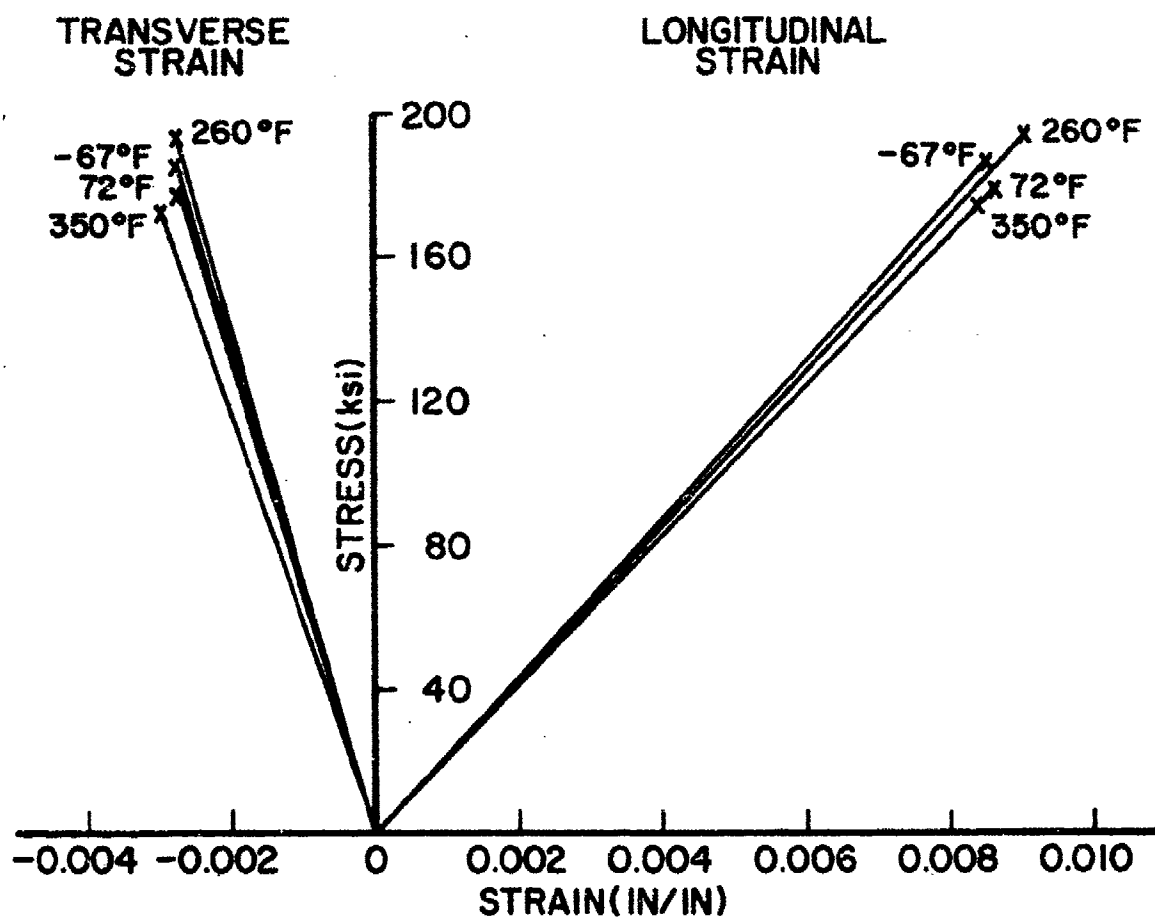


Figure 9. Tensile Stress-Strain Curves for Unidirectional T300/AFR800 Composite Laminates: 0° Fiber Orientation.

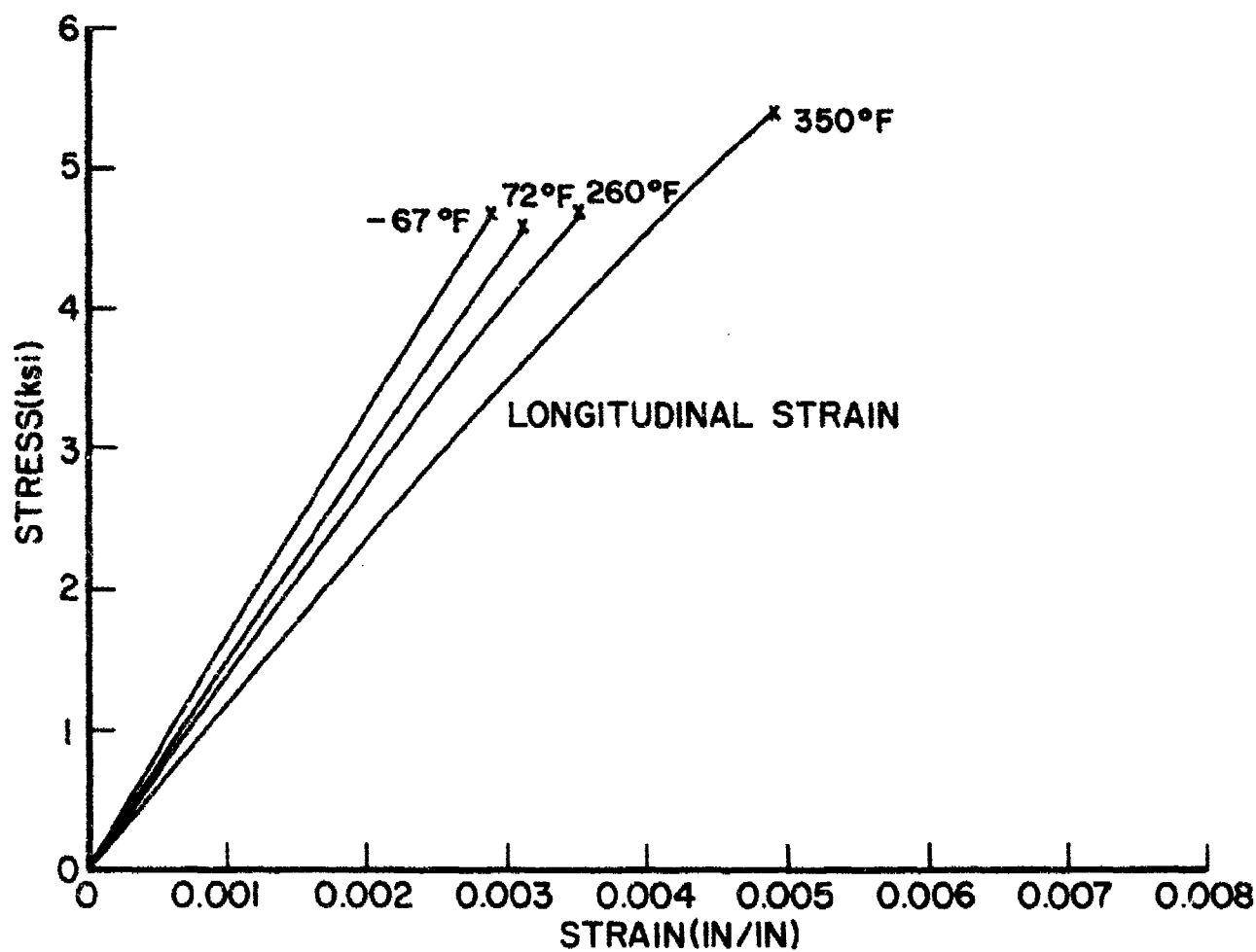


Figure 10. Tensile Stress-Strain Curves for Unidirectional T300/AFR800 Composite Laminates: 90° Fiber Orientation.

TABLE 10
TENSILE PROPERTIES OF T300/AFR800 COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/AFR 800		Prepreg by - Hexcel	Graphite/Epoxy	
Fiber - T300 Matrix - AFR 800		Laminate Sp. Gr. - 1.57		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0057 inch		
Resin Content - 30.5% by wt.		No. of panels from which specimens were tested		
Fiber Content - 59.6% by vol.		in this table - 5		
Void Content - ≈ 0% by vol.		Thickness of specimen - 8 ply		
TENSION: +45°				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F_x^{tu} [ksi](MPa)	[26.4] (182)	[23.2] (160)	[16.8] (116)	[16.3] (112)
Std.Dev.[ksi] (MPa)	[1.00] (6.9)	[1.03] (7.1)	[1.12] (7.7)	[0.86] (5.9)
Range [ksi](MPa)	[25.2-27.8] (174-191)	[21.5-24.1] (148-166)	[15.4-18.0] (106-124)	[15.3-17.1] (105-118)
No. of Specimens	5	5	5	5
F_x^{tpl} [ksi](MPa)	[9.37] (64.6)	[4.69] (32.3)	[4.93] (34.0)	[2.13] (14.7)
Std.Dev.[ksi] (MPa)	[2.36] (16.3)	[1.14] (7.85)	[0.36] (2.48)	[0.34] (2.34)
No. of Specimens	5	5	5	5
E_x^t [Msi](GPa)	[2.28] (15.7)	[2.35] (16.2)	[2.14] (14.7)	[1.62] (11.2)
Std.Dev.[Msi] (GPa)	[0.12] (0.83)	[0.16] (1.10)	[0.11] (0.76)	[0.12] (0.83)
No. of Specimens	5	5	5	5
ϵ_x^{tu} [μ in/in] (μ cm/cm)	>12,080 ¹	17,630	>21,590 ¹	>39,450 ¹
Std. Dev.	---	1,630	> 7,090	---
No. of Specimens	5	5	5	5
ν_{xy}^t	0.69	0.75	0.78	0.88
Std. Dev.	0.04	0.04	0.01	0.06
No. of Specimens	5	5	5	5
Test Method	ASTM D3039			
Reference				

¹ Some strain gages lost before completion of test.

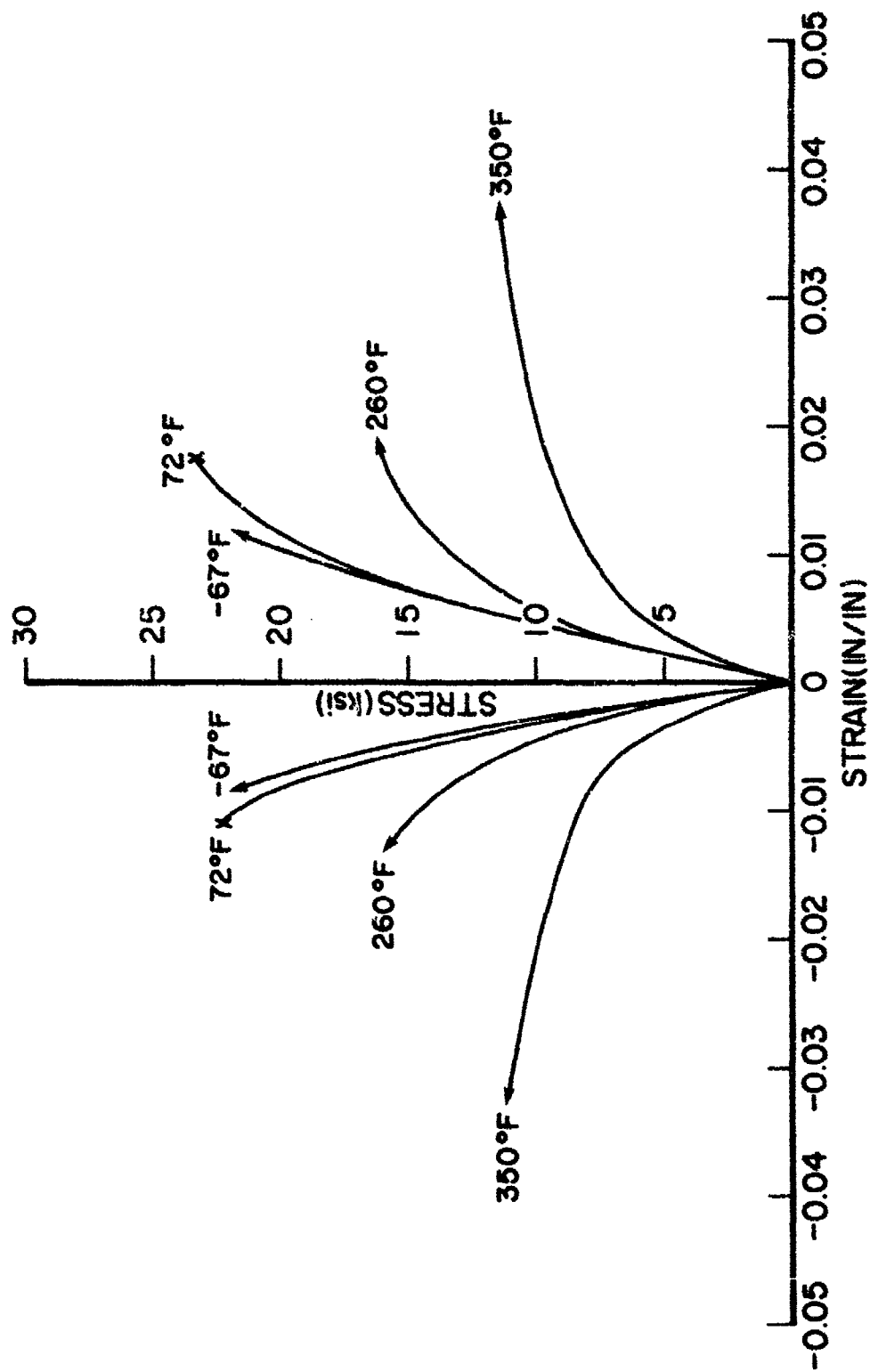


Figure 11. Tensile Stress-Strain Curve for Bidirectional T300/AFR800 Composite Laminates: +45° Fiber Orientation.

TABLE 11
COMPRESSIVE PROPERTIES OF T300/AFR800
COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/AFR800		Prepreg by - Hexcel		Graphite/Epoxy
Fiber - T300 Matrix - AFR800		Laminate Sp. Gr. - 1.61		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0050 inch		
Resin Content - 24.7% by wt.		No. of panels from which specimens were tested		
Fiber Content - 71.1% by vol.		in this table - 2		
Void Content - ± 0% by vol.				
Thickness of each type specimen: 0° - 20 ply ; 90° - 20 ply				
COMPRESSION: 0°				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
P_{cu}^x [ksi] (MPa)	[205.6] (1417)	[174.6] (1203)	[188.2] (1297)	[164.2] (1131)
Std.Dev. [ksi] (MPa)	[17.0] (117)	[23.0] (158)	[29.4] (203)	[27.2] (187)
Range [ksi] (MPa)	[186.4-224.8] (1284-1549)	[145.6-192.9] (1003-1329)	[149.5-220.5] (1030-1519)	[130.4-206.3] (898-1421)
No. of Specimens	5	5	5	5
P_{cpl}^x [ksi] (MPa)	[66.1] (455)	[44.8] (309)	[75.4] (520)	[71.3] (491)
Std.Dev. [ksi] (MPa)	[15.0] (103)	[38.7] (267)	[33.3] (229)	[53.0] (365)
No. of Specimens	5	5	5	5
E_x^c [ksi] (GPa)	[19.15] (132)	[15.98] (110)	[18.38] (127)	[20.71] (143)
Std.Dev. [ksi] (GPa)	[2.19] (15.1)	[2.85] (19.6)	[3.24] (22.3)	[2.64] (18.2)
No. of Specimens	5	5	5	5
ϵ_{cu}^x [μ in/in] (μ cm/cm)	18,300	14,700	14,400	8,300
Std. Dev.	5,600	2,430	2,000	1,400
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3410			
COMPRESSION: 90°				
P_{cu}^y [ksi] (MPa)	[44.2] (305)	[39.7] (274)	[28.4] (196)	[27.7] (191)
Std.Dev. [ksi] (MPa)	[13.8] (95)	[4.8] (33)	[1.5] (10)	[3.9] (27)
Range	[23.9-55.8] (165-384)	[32.4-45.7] (223-315)	[26.7-29.9] (184-206)	[23.0-32.7] (158-225)
No. of Specimens	5	5	5	5
P_{cpl}^y [ksi] (MPa)	[13.7] (95)	[32.8] (226)	[18.9] (130)	[22.3] (154)
Std.Dev. [ksi] (MPa)	[6.8] (47)	[15.7] (108)	[12.4] (85)	[11.0] (76)
No. of Specimens	5	5	5	5
E_y^c [ksi] (GPa)	[1.70] (11.7)	[2.50] (17)	[1.50] (10.3)	[2.02] (13.9)
Std.Dev. [ksi] (GPa)	[0.24] (1.7)	[0.27] (1.9)	[0.09] (0.6)	[0.57] (3.9)
No. of Specimens	5	5	5	5
ϵ_{cy}^c [μ in/in] (μ cm/cm)	31,500	17,900 ^{1,2}	12,700 ^{1,2}	25,800
Std. Dev.	6,600	9,000	4,400	9,800
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3410			

¹Ultimate strain values represent maximum observed strain rather than ultimate values.

²Two of five specimens exhibited evidence of buckling.

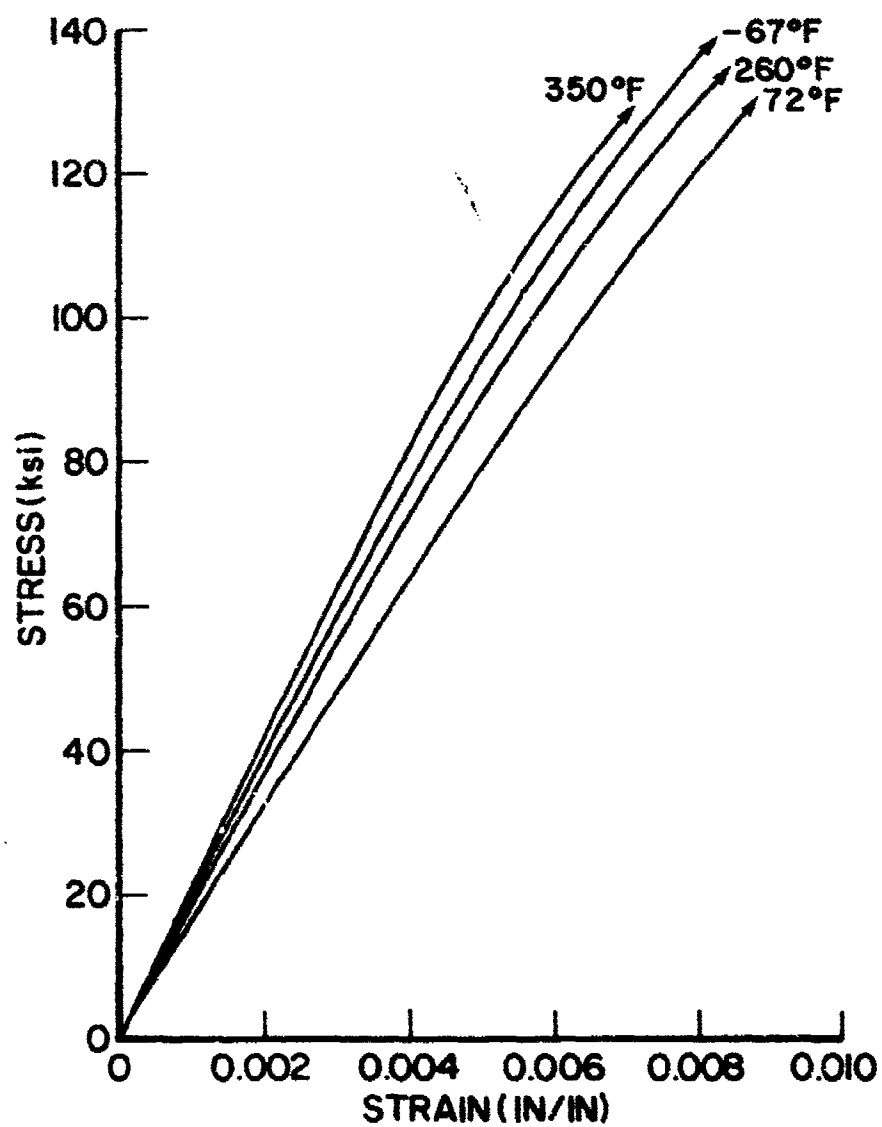


Figure 12. Compressive Stress-Strain Curves for Unidirectional T300/AFR800 Composite Laminates: 0° Fiber Orientation.

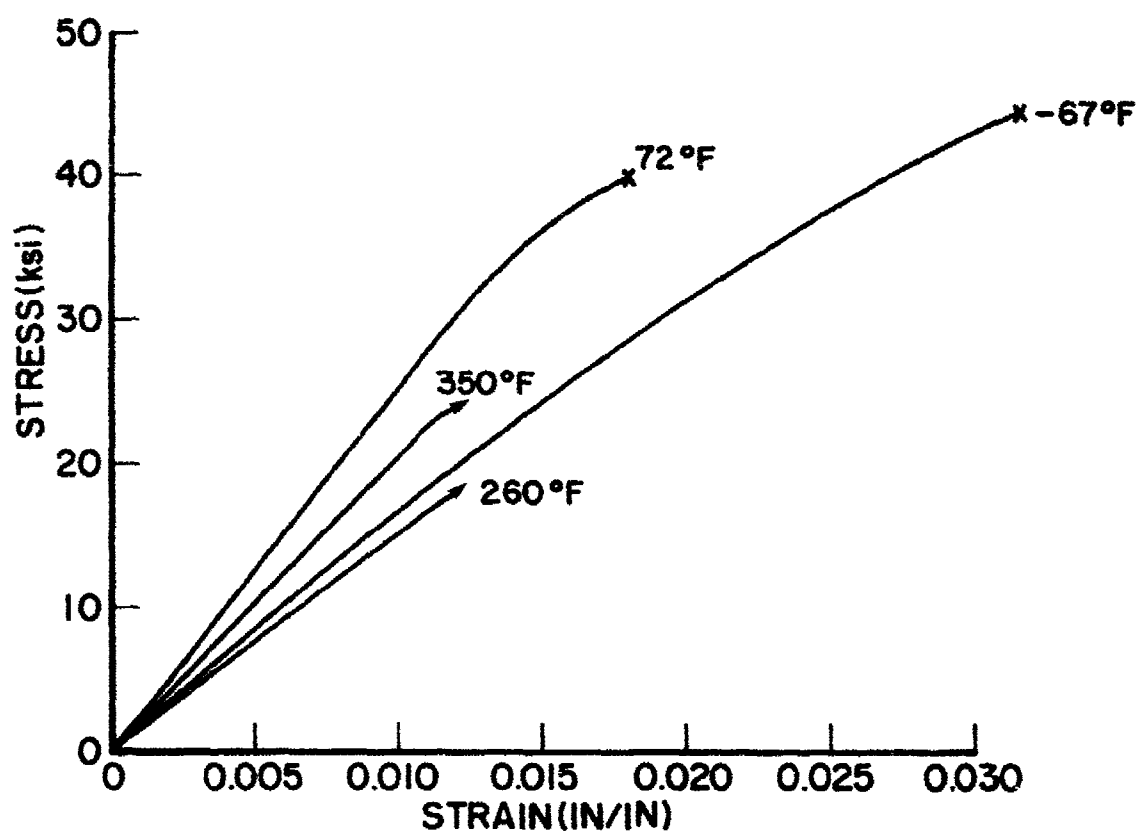


Figure 13. Compressive Stress-Strain Curves for Unidirectional T300/AFR800 Composite Laminates: 90° Fiber Orientation.

TABLE 12
FLEXURAL PROPERTIES OF T300/AFR800
COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/AFR 800		Prepreg by - Hexcel		Graphite/Epoxy
Fiber - T300 Matrix - AFR 800		Laminate Sp. Gr. - 1.69		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0049 inch		
Resin Content - 23.8% by wt.		No. of panels from which specimens were tested in this table - 2		
Fiber Content - 75.54 by vol.				
Void Content - 40% by vol.				
Thickness of each type specimen: 0° - 14 ply ; 90° - 14 ply				
FLEXURE: 0°				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
F_x^{fu} [ksi] (MPa)	[291.6] (2009)	[280.1] (1930)	[218.2] (1503)*	[186.8] (1287)*
Std.Dev. [ksi] (MPa)	[8.2] (56)	[4.4] (30)	[10.9] (75)	[5.3] (37)
Range [ksi] (MPa)	[278.1-299.7] (1916-2065)	[272.9-284.9] (1880-1963)	[206.5-230.0] (1423-1585)	[181.3-192.5] (1249-1326)
No. of Specimens	5	5	5	5
E_x^f [Msi] (GPa)	[20.11] (138.5)	[20.70] (142.6)	[20.82] (143.4)	[19.94] (137.4)
Std.Dev. [Msi] (GPa)	[1.17] (8.06)	[0.74] (5.10)	[0.42] (2.89)	[0.21] (1.45)
No. of Specimens	5	5	5	5
Test Method Reference	4 pt. flexure Design Guide; Jan. 1971 } Corresponds to ASTM D790 except for loading points and loading speed.			
FLEXURE: 90°				
F_y^{fu} [ksi] (MPa)	[14.90] (102.7)	[14.10] (97.1)	[10.68] (73.6)	[11.21] (77.2)
Std.Dev. [ksi] (MPa)	[1.75] (12.1)	[0.36] (2.48)	[0.44] (3.03)	[1.31] (9.03)
Range [ksi] (MPa)	[13.02-17.71] (89.7-122.0)	[13.57-14.43] (93.5-99.4)	[10.21-11.21] (70.3-77.2)	[9.68-12.80] (66.7-88.2)
No. of Specimens	5	5	5	5
E_y^f [Msi] (GPa)	[1.67] (11.51)	[1.27] (8.75)	[1.17] (10.53)	[1.13] (7.79)
Std.Dev. [Msi] (GPa)	[0.06] (0.41)	[0.04] (0.28)	[0.07] (0.48)	[0.08] (0.55)
No. of Specimens	4	5	5	5
Test Method Reference	4 pt. flexure Design Guide; Jan. 1971 } Corresponds to ASTM D790 except for loading points and loading speed.			

*At the two higher test temperatures, the 0° specimens failed by delamination rather than fracture at the lower plies.

TABLE 13
SHEAR PROPERTIES OF T300/AFR800
COMPOSITE LAMINATES

Composite Material Properties				
Material System - AFR800/T300		Prepreg by - Hexcel	Graphite/Epoxy	
Fiber - T300 Matrix - AFR800		Laminate Sp. Gr. - 1.58		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0054 inch		
Resin Content - 29.4% by wt.		No. of panels from which specimens were tested		
Fiber Content - 65.5% by vol.		in this table - 6		
Void Content - =0.4% by vol.				
Thickness of each type specimen - Inplane - 8 ply ; Interlaminar - 15 ply				
INPLANE SHEAR				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
F _{xy} ^{su} [ksi] (MPa)	[13.2] (91.0)	[11.6] (79.9)	[8.4] (58.0)	[8.1] (55.8)
Std.Dev. [ksi] (MPa)	[0.50] (3.45)	[0.52] (3.58)	[0.55] (3.79)	[0.43] (2.95)
Range [ksi] (MPa)	[12.6-13.9] (87.0-95.5)	[10.8-12.0] (74.4-82.7)	[7.7-9.0] (53.0-62.0)	[7.7-8.6] (52.5-59.0)
No. of Specimens	5	5	5	5
G _{xy} ^s [ksi] (MPa)	[0.68] (4.66)	[0.68] (4.69)	[0.61] (4.22)	[0.43] (2.94)
Std.Dev. [ksi] (MPa)	[0.03] (0.18)	[0.05] (0.34)	[0.03] (0.23)	[0.02] (0.14)
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3518			
INTERLAMINAR SHEAR				
f _{isu} [ksi] (MPa)	[18.17] (125.2)	[15.27] (105.2)	[11.77] (81.1)	[9.63] (66.4)
Std.Dev. [ksi] (MPa)	[0.92] (6.34)	[0.79] (5.4)	[0.69] (4.75)	[0.33] (2.27)
Range [ksi] (MPa)	[17.27-19.27] (119.0-132.8)	[14.37-17.16] (99.0-118.2)	[11.02-12.81] (75.9-88.3)	[9.27-10.00] (63.9-68.9)
No. of Specimens	5	10	5	5
Test Method Reference	ASTM D2344			

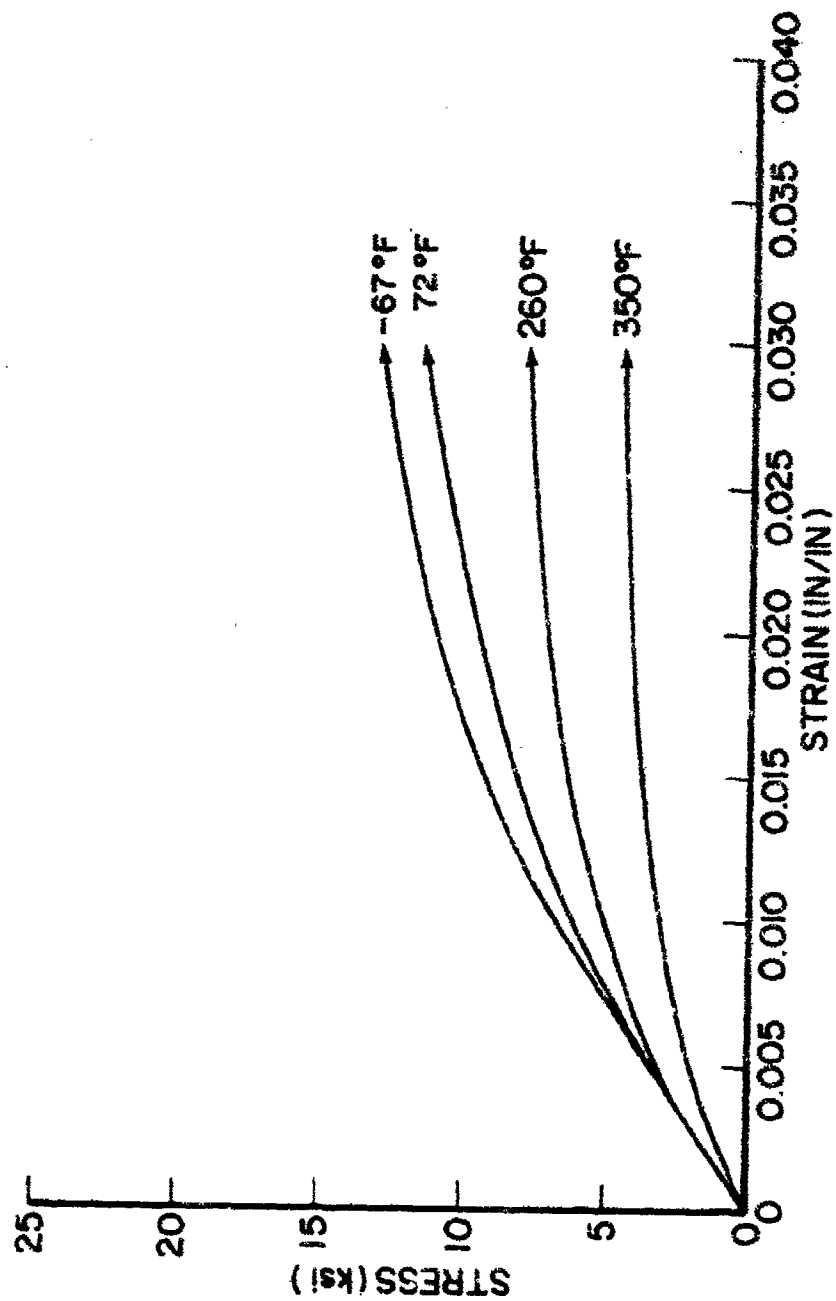


Figure 14. Inplane Shear Stress-Strain Curves for T300/AFR800 Composite Laminates.

TABLE 14
TENSILE, COMPRESSIVE AND SHEAR PROPERTIES OF T300/AFR800
COMPOSITE LAMINATES AFTER HUMIDITY AGING

Compressive Material Properties				
Material System - T300/AFR800		Tested by - General		Composite/Specimen
Fiber - T300		Resin - AFR800		Isotonic Sp. Cr. - 1.25
Random Fiber Dispersion - 350°F (177°C)		Nominal Ply Thickness - 0.0025 inch		
Resin Content - 28.2% by wt.		No. of plies from which specimens were		
Fiber Content - 71.7% by vol.		tested in this table - 7		
Void Content - 2.9% by vol.		Aging Conditions - 350°F (177°C) & 90-100% R.H.		
Thickness of each type specimen: Tension - 35 ply; Comp. - 30 ply; Shear - 25 ply				
TENSION: 90°				
	ASTM D3039	ASTM D3039	ASTM D3039	ASTM D3039
Exposure Time (hrs)	136	296	1036	1904
Weight Gain(% of orig. dry wt.)	0.63	0.38	1.25 ¹	1.27 ¹
Stand. Dev. (%)	0.05	0.10	0.04	0.04
No. of Specimens	5	5	5	5
E_y (ksi) (GPa)	[35.33] (24.5)	[33.33] (23.0)	[33.33] (23.0)	[31.49] (21.7)
Stand. Dev. (ksi) (GPa)	[0.87] (0.6)	[0.87] (0.6)	[0.87] (0.6)	[0.87] (0.6)
Range (ksi) (GPa)	[34.22-36.37]	[32.70-34.00]	[32.70-34.00]	[30.75-32.23]
No. of Specimens	5	5	4	4
σ_{UTS} (ksi) (GPa)	[11.72] (8.1)	[10.48] (7.3)	[11.52] (8.0)	[11.26] (7.8)
Stand. Dev. (ksi) (GPa)	[1.76] (1.2)	[0.00] (0.0)	[0.49] (0.3)	[0.34] (0.2)
No. of Specimens	5	5	4	4
σ_y (ksi) (GPa)	[1.48] (1.0)	[1.55] (1.1)	[1.45] (1.0)	[1.82] (1.3)
Stand. Dev. (ksi) (GPa)	[0.06] (0.0)	[0.11] (0.0)	[0.07] (0.0)	[0.08] (0.0)
No. of Specimens	5	5	4	4
ϵ_y (in/in) (mm/mm)	3030	3115	2566	1362
Stand. Dev.	66	63	52	66
No. of Specimens	5	5	4	4
ν_y				
Stand. Dev.				
No. of Specimens				
Test Method	ASTM D3039			
Reference				
COMPRESSION: 90°				
	ASTM D3039	ASTM D3039	ASTM D3039	ASTM D3039
Exposure Time (hrs)	136	104	1904	1904
Weight Gain(% of orig. dry wt.)	0.65	0.81	1.25 ¹	1.26 ¹
Stand. Dev. (%)	0.03	0.03	0.10	0.03
No. of Specimens	5	5	4	4
E_y (ksi) (GPa)	[30.9] (21.5)	[30.0] (20.8)	[32.2] (22.4)	[34.1] (23.7)
Stand. Dev. (ksi) (GPa)	[0.5] (0.3)	[1.3] (0.9)	[1.2] (0.8)	[1.5] (1.0)
Range (ksi) (GPa)	[29.6-32.6]	[28.4-30.7]	[29.7-33.0]	[32.7-35.5]
No. of Specimens	5	5	3	4
σ_{UTS} (ksi) (GPa)	[24.3] (16.9)	[19.7] (13.8)	[27.1] (19.0)	[22.5] (15.8)
Stand. Dev. (ksi) (GPa)	[16.2] (11.4)	[2.0] (1.4)	[12.8] (9.0)	[2.2] (1.5)
No. of Specimens	5	5	3	4
σ_y (ksi) (GPa)	[1.70] (1.2)	[1.84] (1.3)	[1.80] (1.3)	[1.63] (1.1)
Stand. Dev. (ksi) (GPa)	[0.3] (0.2)	[0.9] (0.6)	[0.5] (0.3)	[0.4] (0.3)
No. of Specimens	5	5	3	4
ϵ_y (in/in) (mm/mm)	43,100	36,300	37,000	33,000
Stand. Dev.	14,000	13,200	16,700	14,000
No. of Specimens	5	5	3	4
Test Method	ASTM D3039			
Reference				
INTER-LAYER SHEAR				
	ASTM D2344	ASTM D2344	ASTM D2344	ASTM D2344
Exposure Time (hrs)	27	27	1306	1306
Weight Gain(% of orig. dry wt.)	0.67	0.78	1.25 ¹	1.26 ¹
Stand. Dev. (%)	0.13	0.19	0.17	0.10
No. of Specimens	20	5	10	5
Strength (ksi) (MPa)	[15.64] (107.7)	[10.84] (75.0)	[12.76] (88.0)	[7.47] (51.5)
Stand. Dev. (ksi) (MPa)	[0.79] (5.4)	[0.42] (3.0)	[0.64] (4.4)	[0.10] (0.68)
Range (ksi) (MPa)	[14.84-16.64]	[10.00-11.19]	[11.05-14.75]	[7.30-7.62]
No. of Specimens	10	5	10	5
Test Method	ASTM D2344			
Reference				

NOTES: 1. 100% saturation at aging conditions.

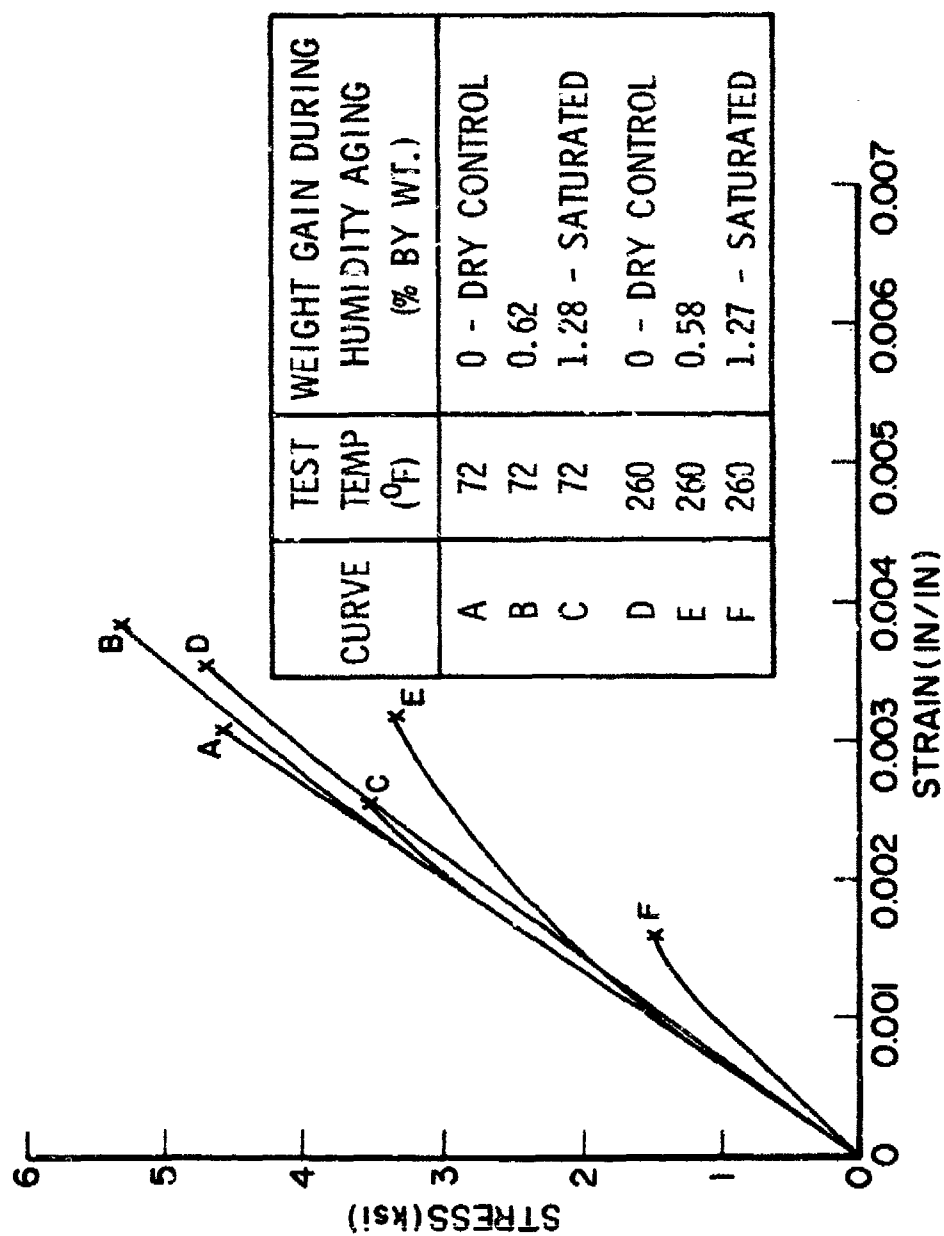


Figure 15. Tensile Stress-Strain Curves for Unidirectional T300/AFR800 Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

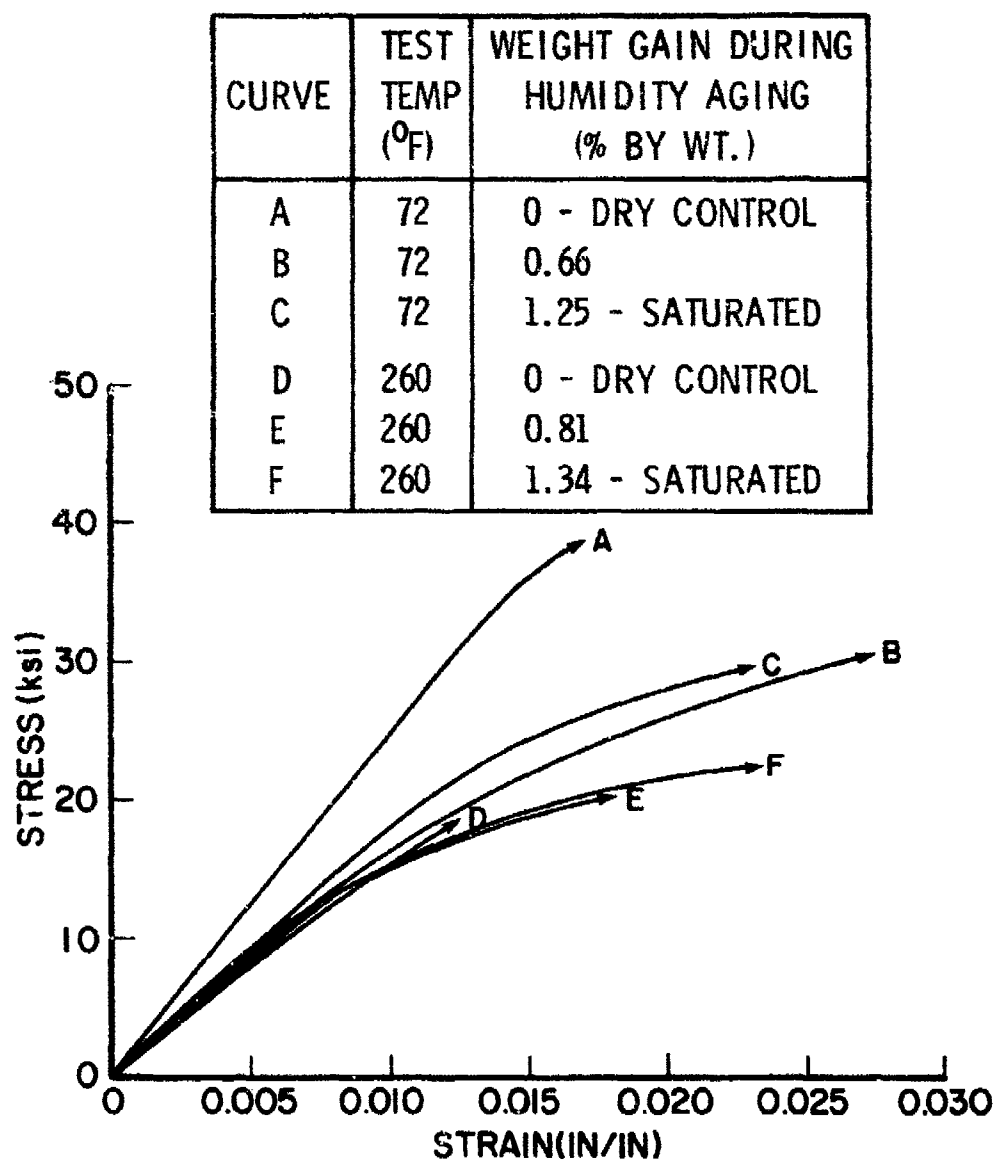


Figure 16 . Compressive Stress-Strain Curves for Unidirectional T300/AFR800 Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

TABLE 15
CREEP PROPERTIES OF T300/AFR800 COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/AFR800		Prepreg by - Hexcel		Graphite/Epoxy
Fiber - T300 Matrix - AFR800		Laminate Sp. Cr. - 1.5%		
Maximum Temperature Rating - 350°F (177°C)		Nominal Ply Thickness - 0.0052 inch		
Resin Content - 27.5% by wt.		No. of panels from which specimens were tested in this table - 24		
Fiber Content - 68.0% by vol.		Thickness of each type specimen:		
Void Content - 4.0% by vol.		0° - 6 ply		
Test Method - Straight-sided tension		90° - 15 ply		
Reference - ASTM D2290 & D3029		+45° - 8 ply		
CREEP				
Temperature	Fiber Orientation	0°	90°	+45°
72°F (22°C)	Stress Level [ksi] (MPa)	[163.8] (1129)	[3.21] (22.1)	[16.27] (112)
	Creep Strain, 500 hr (%)	0.0067	---	0.4039
	No. of Specimens	3	3	3
	Residual Strength [ksi] (MPa)	[211.5] (1457)	---	[23.45] (162)
	No. of Specimens	2	0	3
	Stress Level [ksi] (MPa)	[143.4] (987)	[2.75] (18.9)	[13.94] (96)
	Creep Strain, 500 hr (%)	0.0002	0.0355	0.2693
	No. of Specimens	3	2	3
	Residual Strength [ksi] (MPa)	---	[6.18] (42.6)	---
	No. of Specimens	---	2	---
	Stress Level [ksi] (MPa)	---	[2.29] (15.8)	[11.62] (80)
	Creep Strain, 500 hr (%)	---	0.0342	0.2046
	No. of Specimens	---	3	3
	Residual Strength [ksi] (MPa)	---	[5.60] (38.6)	[22.97] (158)
	No. of Specimens	---	3	3
260°F (127°C)	Stress Level [ksi] (MPa)	[174.5] (1202)	[2.81] (19.4)	[13.44] (93)
	Creep Strain, 500 hr (%)	0.1300 at 910 hr. ¹	---	---
	No. of Specimens	1 ³	3	3
	Residual Strength [ksi] (MPa)	[208.8] (1439)	[6.11] (42.1)	---
	No. of Specimens	1	1	0
	Stress Level [ksi] (MPa)	[155.1] (1068)	[2.58] (17.8)	[11.76] (81)
	Creep Strain, 500 hr (%)	0.0715	0.0610	1.1214
	No. of Specimens	2	3	3
	Residual Strength [ksi] (MPa)	[199.7] (1376)	[5.08] (35.0)	[23.08] (159)
	No. of Specimens	2	3	3
	Stress Level [ksi] (MPa)	[135.7] (935)	[2.34] (16.1)	[10.08] (70)
	Creep Strain, 500 hr (%)	0.0054	0.0608	0.9367
	No. of Specimens	3	3	3
	Residual Strength [ksi] (MPa)	[221.1] (1523)	[4.98] (34.3)	[25.57] (163)
	No. of Specimens	3	3	3
350°F (177°C)	Stress Level [ksi] (MPa)	[186.2] (1076)	[2.71] (18.7)	[9.76] (67)
	Creep Strain, 500 hr (%)	0.0646	---	---
	No. of Specimens	2 ³	3	2
	Residual Strength [ksi] (MPa)	[217.1] (1496)	---	---
	No. of Specimens	3	0	0
	Stress Level [ksi] (MPa)	[138.8] (956)	[2.17] (15.0)	[6.14] (56)
	Creep Strain, 500 hr (%)	0.0162	0.2775 ¹	1.7298 at 7 hr. ¹
	No. of Specimens	4	1 ³	2
	Residual Strength [ksi] (MPa)	[216.9] (1494)	[5.01] (34.5)	[19.35] (133)
	No. of Specimens	4	1	3
	Stress Level [ksi] (MPa)	[121.5] (837)	[1.63] (11.2)	[6.51] (45)
	Creep Strain, 500 hr (%)	0.0494	0.3629	2.372 at 120 hr. ¹
	No. of Specimens	2 ¹	3	2
	Residual Strength [ksi] (MPa)	[186.0] (1282)	[3.93] (27.1)	[16.10] (125)
	No. of Specimens	3	3	2

Notes: All values represent arithmetic average.

All residual strengths determined by tensile test at 72°F.

1. Gage malfunctioned before end of test on one specimen.
2. One specimen failed on loading or during test.
3. Two specimens failed on loading or during test.
4. Three specimens failed on loading or during test.
5. Test oven malfunctioned during test on one specimen.
6. Strain exceeded gage limits on all specimens.

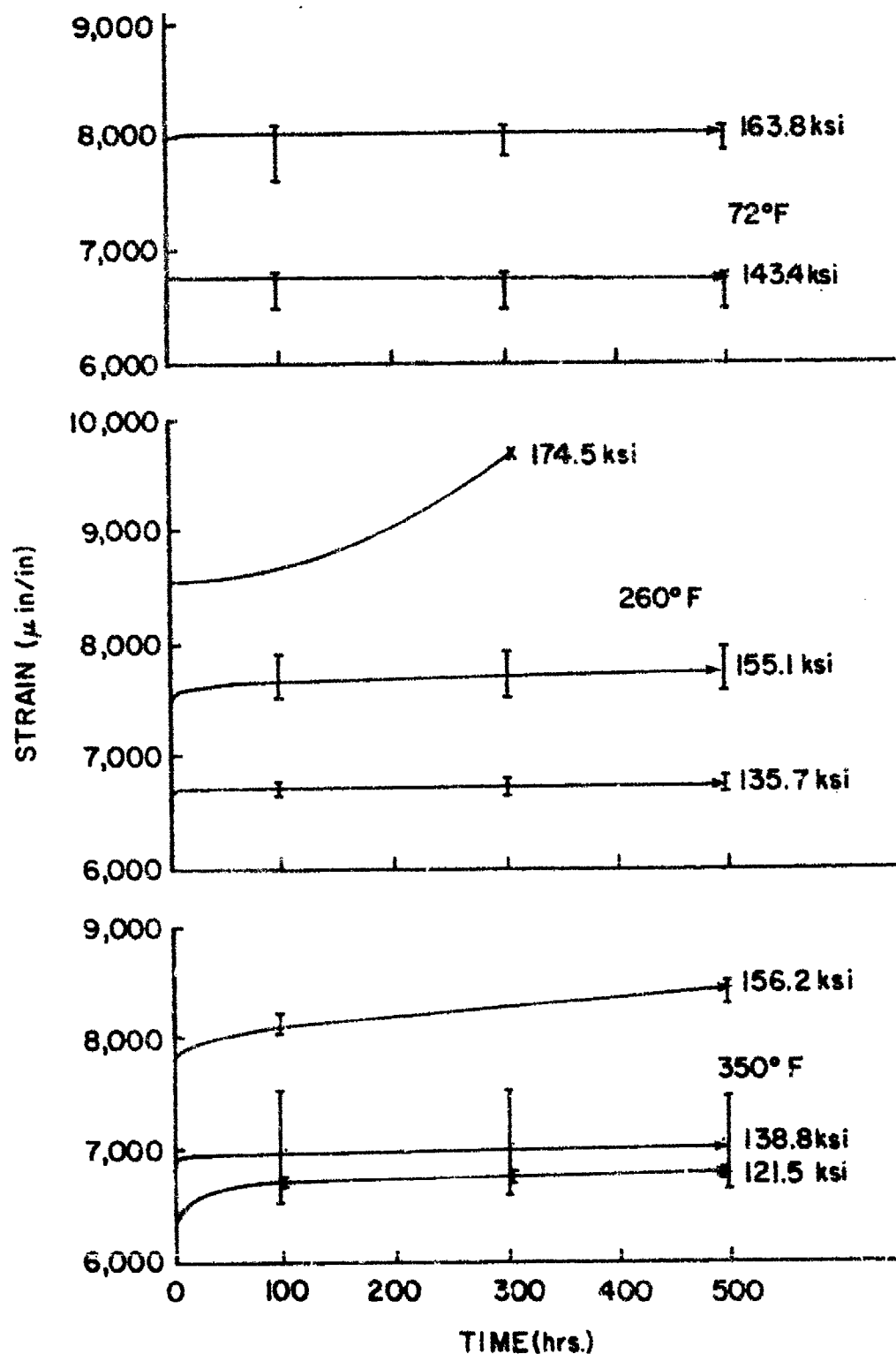


Figure 17. Tensile Creep Behavior of Unidirectional T300/AFR800 Composite Laminates: 0° Fiber Orientation.

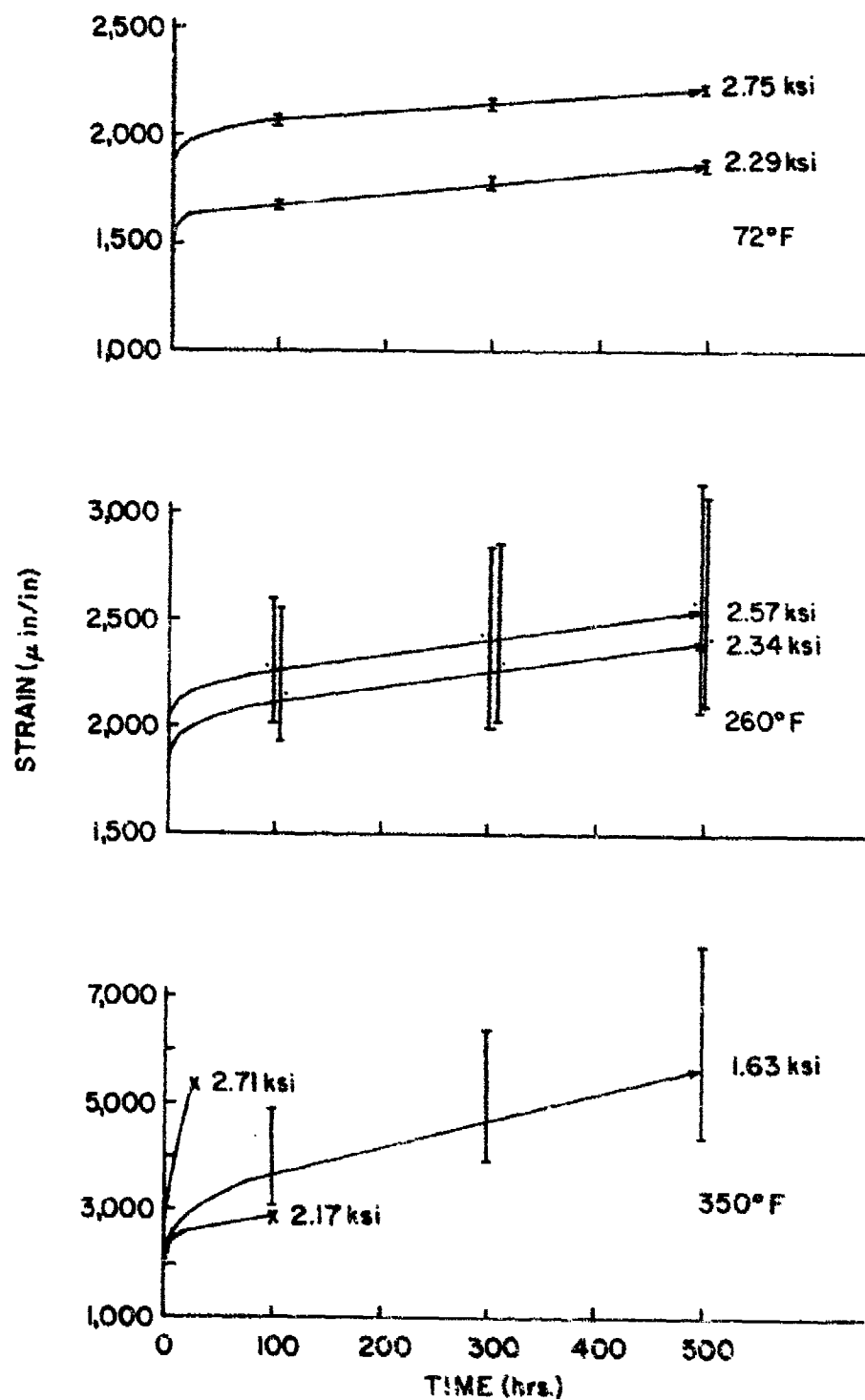


Figure 18. Tensile Creep Behavior of Unidirectional T300/APR800 Composite Laminates: 90° Fiber Orientation.

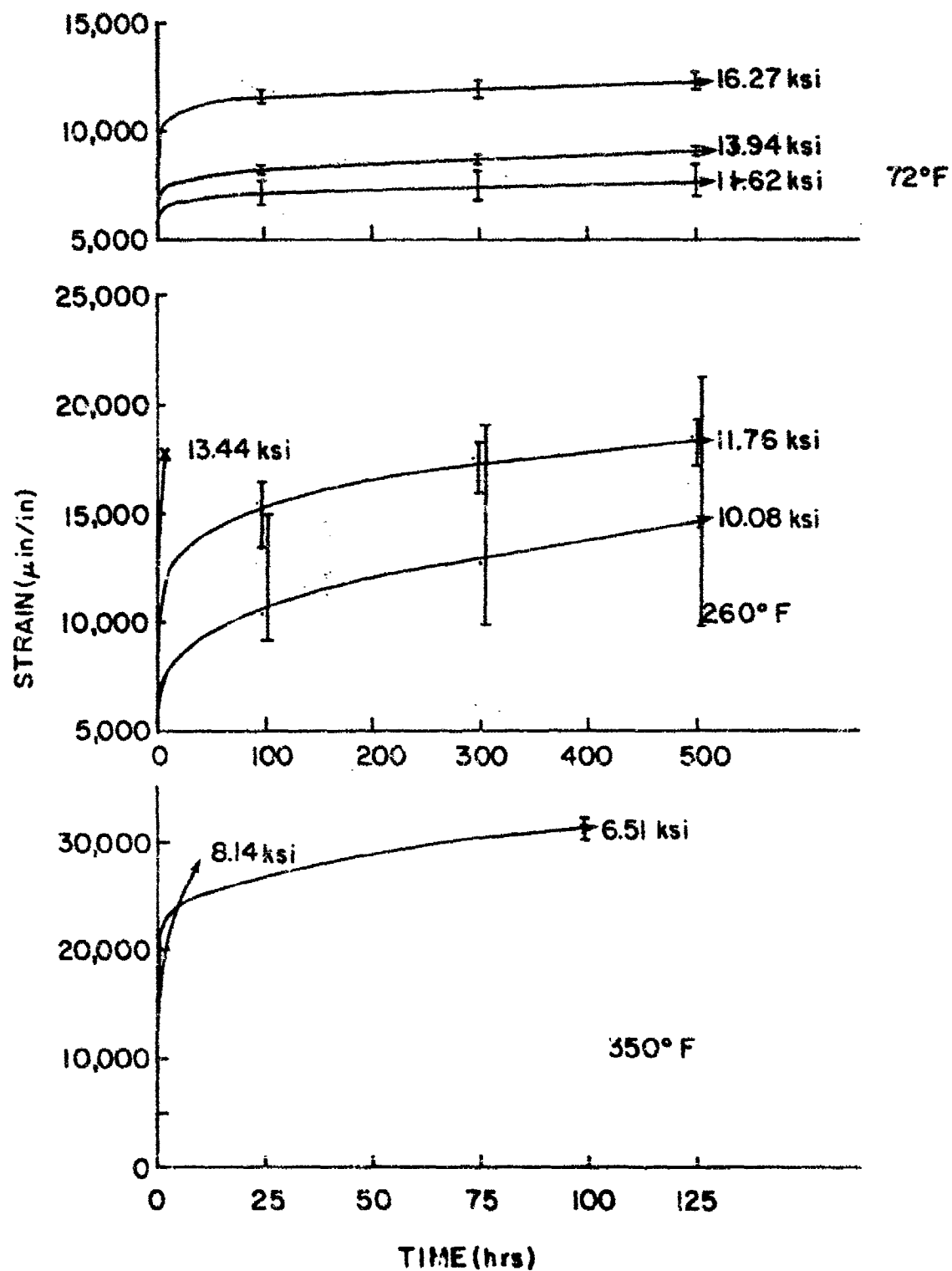


Figure 19. Tensile Creep Behavior of Bidirectional T300/APR800 Composite Laminates: $\pm 45^\circ$ Fiber Orientation.

TABLE 16
STRESS RUPTURE PROPERTIES OF T300/AFR800
COMPOSITE LAMINATES

Composite Material Properties							
Material System - T300/AFR800		Prepreg by - Hexcel		Graphite/Epoxy			
Fiber - T300		Matrix- AFR800		Laminate Sp. Gr. - 1.59			
Maximum Temperature Rating - 350°F				Nominal Ply Thickness - 0.0052 inch			
Resin Content - 27.5% by wt.				No. of panels from which specimens were tested in this table - 24			
Fiber Content - 68.0% by vol.				Thickness of each type specimen:			
Void Content - 40% by vol.				0° - 6 ply			
Test Method - Straight-sided tension		Reference - ASTM D2290 & D3039		90° - 15 ply			
				+45° - 8 ply			
STRESS RUPTURE							
Temperature	Fiber Orientation	0°		90°		+45°	
72°F(22°C)	Stress Level[ksi](MPa)	[163.8]	[1129]	[2.75]	[18.9]	[16.27]	[112]
	Time to Failure(hrs)	500		333		500	
	No. of Specimens	3		3		3	
	Residual Strength[ksi](MPa)	[211.5]	[1457]	[6.18]	[42.6]	[23.45]	[162]
	No. of Specimens	2		2		3	
	Stress Level[ksi](MPa)	[143.4]	[987]	[2.29]	[15.8]	[13.94]	[96]
	Time to Failure(hrs)	500 ¹		500 ¹		500 ¹	
	No. of Specimens	3		3		3	
	Residual Strength[ksi](MPa)	---		[5.60]	[38.6]	---	
	No. of Specimens	---		2		---	
260°F(127°C)	Stress Level[ksi](MPa)	[174.5]	[1202]	[2.81]	[19.4]	[13.44]	[93]
	Time to Failure(hrs)	167 ³		167 ³		0.2 ⁴	
	No. of Specimens	3		3		3	
	Residual Strength[ksi](MPa)	[208.8]	[1439]	[6.11]	[42.1]	---	
	No. of Specimens	1		1		---	
	Stress Level[ksi](MPa)	[155.1]	[1068]	[2.58]	[17.8]	[11.76]	[81]
	Time to Failure(hrs)	336 ²		500 ¹		500 ¹	
	No. of Specimens	3		3		3	
	Residual Strength[ksi](MPa)	[199.7]	[1376]	[5.08]	[35.0]	[23.08]	[159]
	No. of Specimens	2		3		3	
350°F(177°C)	Stress Level[ksi](MPa)	[156.2]	[1076]	[2.71]	[18.7]	[9.76]	[67]
	Time to Failure(hrs)	500 ¹		23 ⁴		156 ⁴	
	No. of Specimens	3		3		3	
	Residual Strength[ksi](MPa)	[217.1]	[1496]	---		---	
	No. of Specimens	3		0		0	
	Stress Level[ksi](MPa)	[138.8]	[956]	[2.17]	[15.0]	[8.14]	[56]
	Time to Failure(hrs)	500 ¹		235 ¹		500 ¹	
	No. of Specimens	4		3		3	
	Residual Strength[ksi](MPa)	[216.9]	[1494]	[5.01]	[34.5]	[19.35]	[133]
	No. of Specimens	4		1		3	

Notes: All values represent arithmetic averages. All residual strengths determined by tensile test at 72°F (22°C).

1. No failures within 500 hours.
2. Average of one failure and two 500-hour survivals.
3. Average of two failures and one 500-hour survival.
4. Average of three failures.

TABLE 17
FATIGUE PROPERTIES OF T300/AFR800
COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/AFR800		Prepreg by - Hexcel	Graphite/Epoxy	
Fiber - T300 Matrix - AFR800		Laminate Sp. Gr. - 1.59		
Maximum Temperature Rating - 350°F (177°C)		Nominal Ply Thickness - 0.0052 inch		
Resin Content - 26.9% by wt.		No. of panels from which specimens were tested		
Fiber Content - 68.6% by vol.		in this table - 25		
Void Content - ± 0% by vol.		Thickness of each type specimen:		
Test Method - Straight-sided tension		Reference - ASTM D3479	0° - 6 ply	
			90° - 15 ply	
			+45° - 8 ply	
TENSILE FATIGUE, R=0.1				
Temperature	Fiber Orientation	0°	90°	+45°
72°F (22°C)	Max. Stress[ksi] (MPa)	[143.7] (990)	[3.21] (22.1)	[16.27] (112)
	Lifetime (cycles)	45,336	52,038	17,688
	No. of Specimens	5	6	5
	Residual Strength[ksi] (MPa)	---	---	---
	No. of Specimens	0	0	0
	Max. Stress[ksi] (MPa)	[134.7] (928)	[2.98] (20.5)	[15.11] (104)
	Lifetime (cycles)	3,960,636	29,091	47,600
	No. of Specimens	6	5	5
	Residual Strength[ksi] (MPa)	[211.0] (1454)	---	---
	No. of Specimens	4	0	0
	Max. Stress[ksi] (MPa)	[125.7] (866)	[2.75] (18.9)	[13.94] (96)
	Lifetime (cycles)	2,124,065	1,164,422	1,403,780
No. of Specimens	6	5	5	
Residual Strength[ksi] (MPa)	[203.3] (1401)	[5.49] (37.8)	---	
No. of Specimens	3	2	0	
260°F (127°C)	Max. Stress[ksi] (MPa)	[174.5] (1202)	[2.98] (20.5)	[12.60] (87)
	Lifetime (cycles)	8,052	8723	84,080
	No. of Specimens	5	3	5
	Residual Strength[ksi] (MPa)	---	---	---
	No. of Specimens	0	0	0
	Max. Stress[ksi] (MPa)	[155.1] (1069)	[2.81] (19.4)	[11.76] (81)
	Lifetime (cycles)	136,078	51,608	68,513
	No. of Specimens	5	5	5
	Residual Strength[ksi] (MPa)	---	[7.28] (50.2)	---
	No. of Specimens	0	1	0
	Max. Stress[ksi] (MPa)	[145.4] (1002)	[2.57] (17.7)	[10.92] (75)
	Lifetime (cycles)	1,759,820	10 +	3,449,829
	No. of Specimens	4	1	5
	Residual Strength[ksi] (MPa)	[187.6] (1292)	[6.10] (42.0)	[21.20] (146)
	No. of Specimens	1	1	1

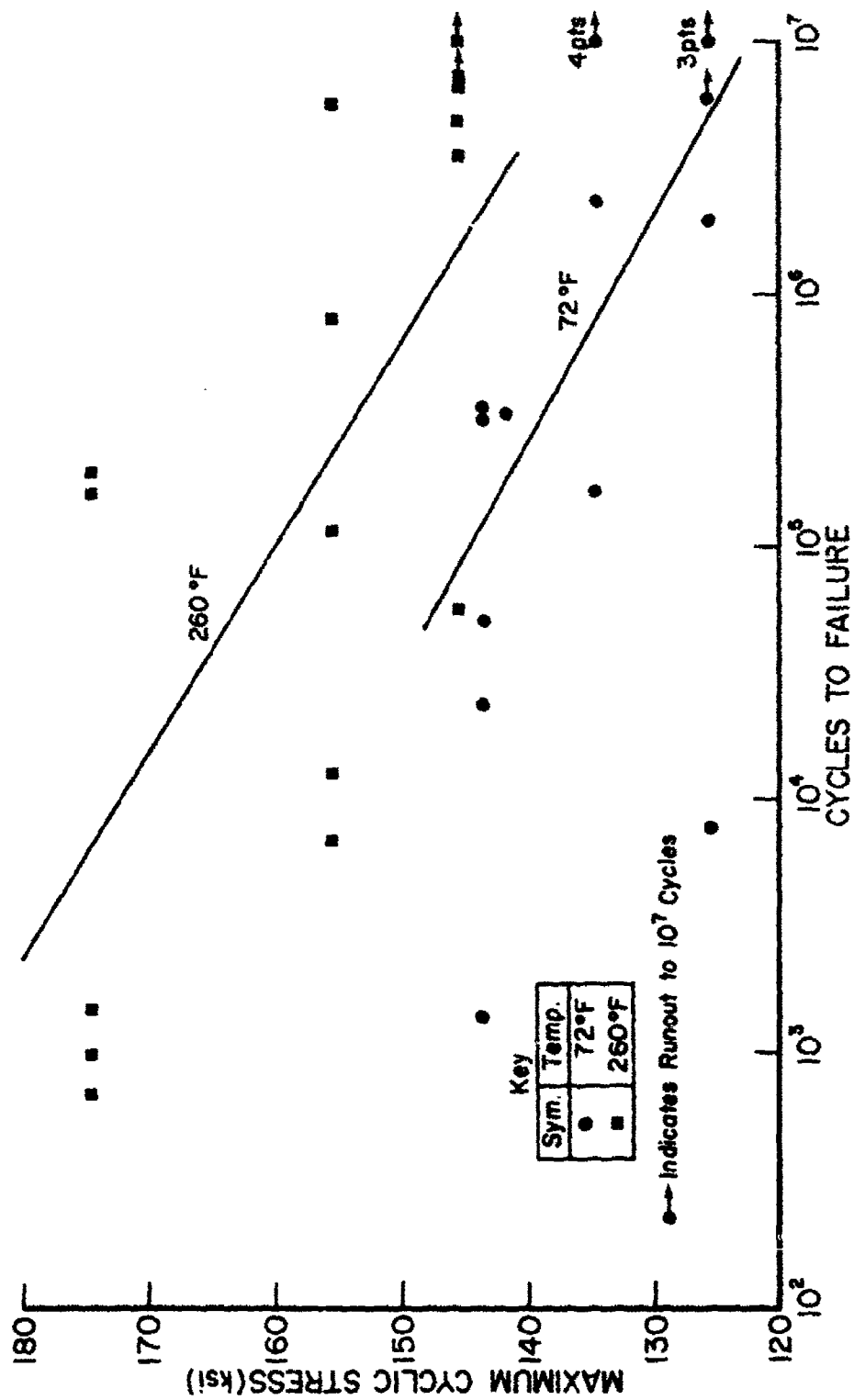


Figure 20. Tensile-Tensile Fatigue Behavior of Unidirectional T300/APR800 Composite
Laminates: 0° Fiber Orientation, R = 0.10, 10 Hz.

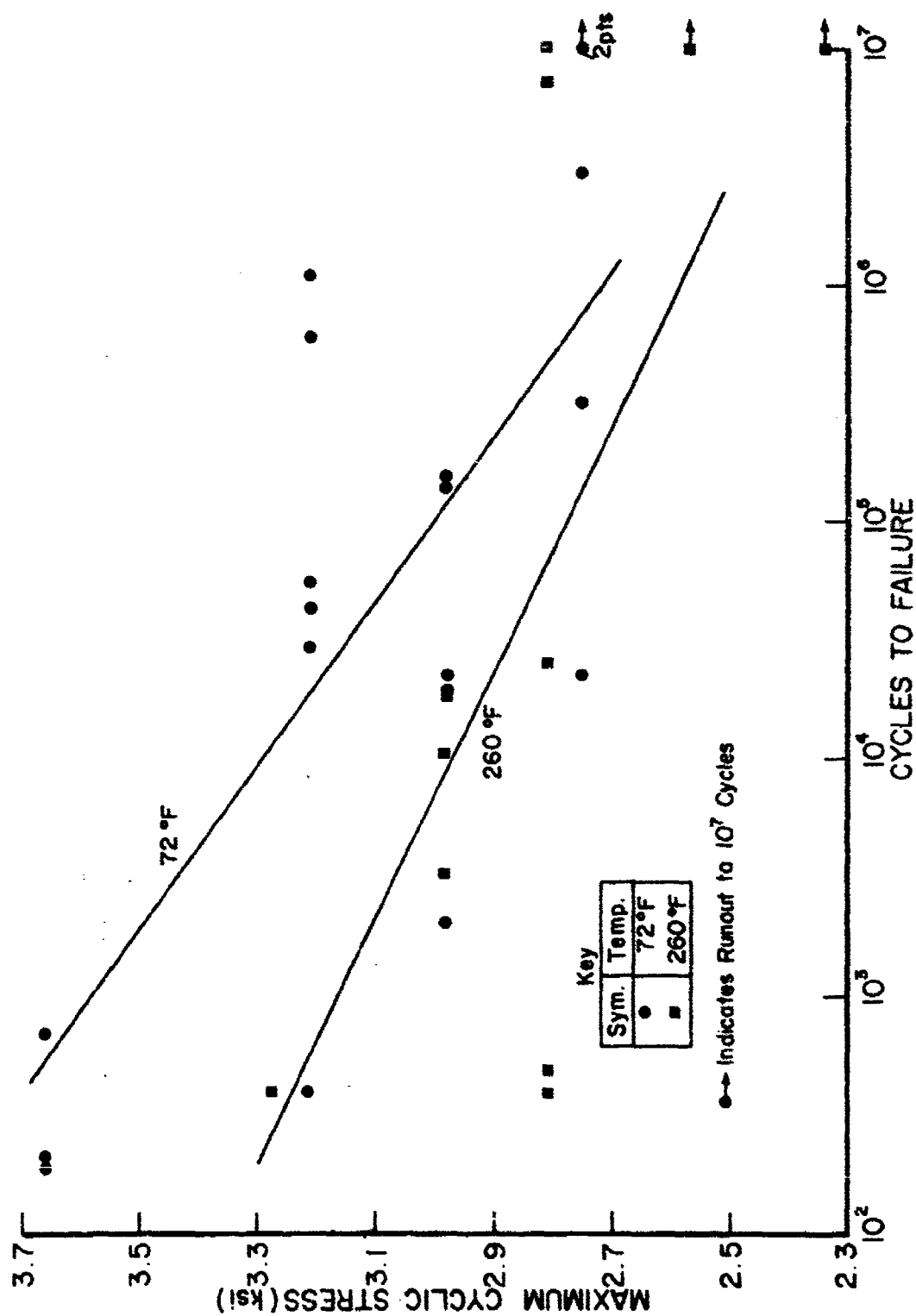


Figure 21. Tensile-Tensile Fatigue Behavior of Unidirectional T300/AFR800 Composite Laminates: 90° Fiber Orientation, $R = 0.10$, 10 Hz.

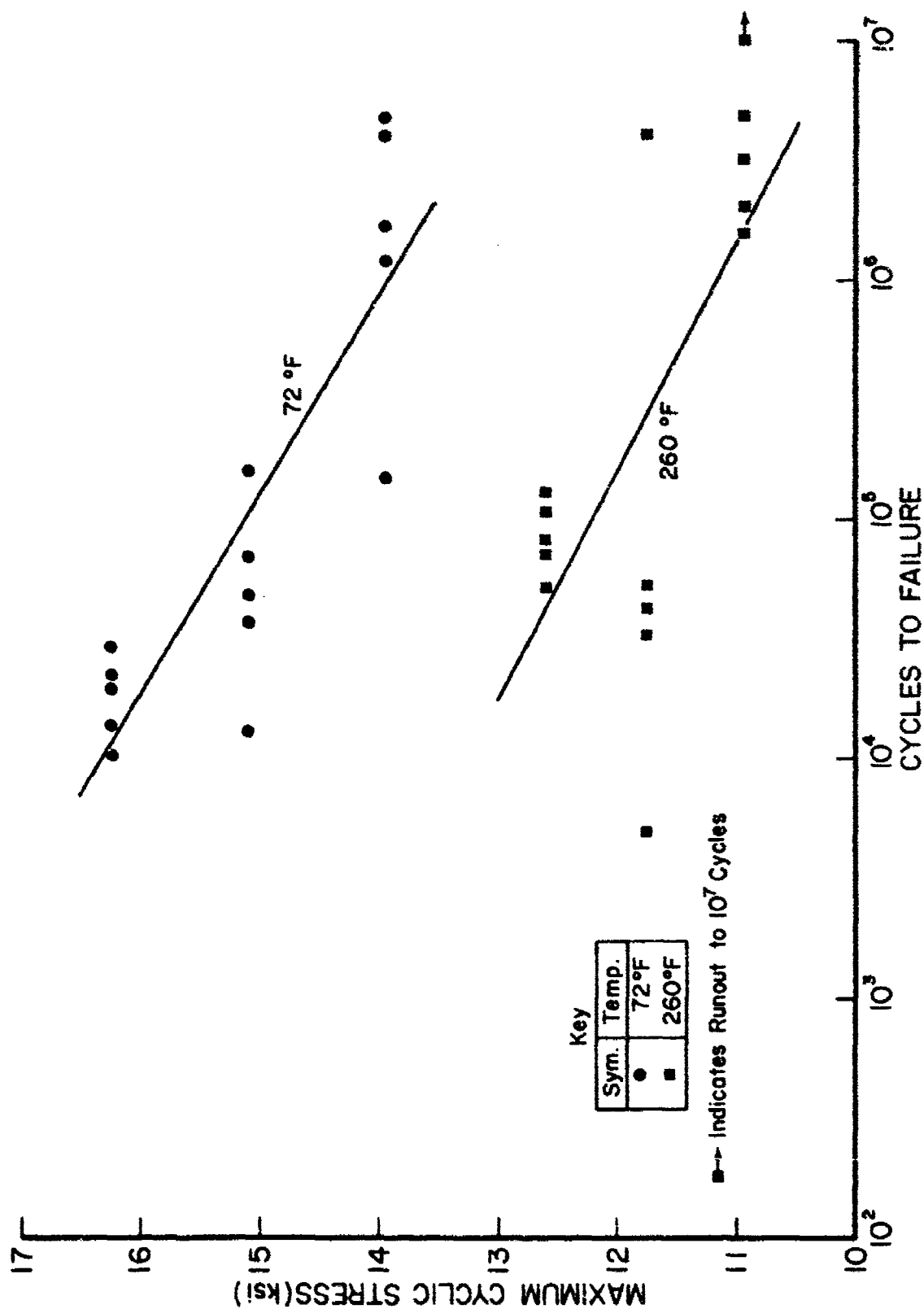


Figure 22. Tensile-Tensile Fatigue Behavior of Bidirectional T300/APR800 Composite Laminates: +45° Fiber Orientation, R = 0.10, 10 Hz.

TABLE 18
THERMOPHYSICAL PROPERTIES OF T300/AFR800
COMPOSITE LAMINATES

Composite Material Properties					
Material System - T300/AFR 800		Prepreg by - Hexcel		Graphite/Epoxy	
Fiber - T300 Matrix - AFR 800		Laminate Sp. Gr. - 1.59			
Maximum Temperature Rating - 350°F (177°C)		Average Ply Thickness - 0.0052 inch			
Resin Content - 26.7% by wt.		No. of panels from which specimens were tested			
Fiber Content - 66.5% by vol.		in this table - 2			
Void Content - ± 0% by vol.					
Thickness of each type specimen:		Therm. Exp. - 50 ply		Spec. Ht. - 1 ply	
		Therm. Cond. - 50 ply		Glass Trans. - 14 ply	
THERMOPHYSICAL PROPERTIES: 0°					
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)	Test Method
Thermal Expansion ¹					TMA ²
α_x [μ in/in-°F] (μ cm/cm-°C)	-0.08	-0.37	-0.14	-0.20	
α_y [μ in/in-°F] (μ cm/cm-°C)	12.9	13.6	14.5	16.9	
No. of Specimens per direction	3	3	3	3	
Specific Heat					DSC ³
C_p [btu/lb.-°F] (J/kg-°C)	[0.081] (339)	[0.203] (849)	[0.302] (1263)	[0.308] (1288)	
No. of Specimens	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.371] (0.642)	[0.433] (0.749)	[0.517] (0.894)	[0.555] (0.960)	
No. of Specimens	3	3	3	3	
Glass Transition Temp.					DMA ⁴
Dry [°F] (°C)	[468] (242)				
Wet [°F] (°C)	[381] (194)				
THERMOPHYSICAL PROPERTIES: +45°					
Thermal Expansion ¹					TMA ²
α_x [μ in/in-°F] (μ cm/cm-°C)	2.6	2.4	2.8	3.2	
No. of Specimens per direction	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.311] (0.538)	[0.351] (0.607)	[0.406] (0.702)	[0.433] (0.749)	
No. of Specimens	3	3	3	3	

NOTES: 1. On the unidirectionally reinforced specimens, the x-direction is along the fiber axis, the y-direction is across the fiber axis, and the z-direction is through the thickness (identical to the y-direction). On +45° bidirectionally reinforced specimens, the x and y directions are identical and oriented at 45° to either fiber direction, while the z-direction is through the thickness.

2. Thermo-Mechanical Analysis.

3. Differential Scanning Calorimetry.

4. Dynamic Mechanical Analysis.

4.2 SiC/5506

This system consisted of 5.6 mil (0.14 mm) silicon carbide fiber (on a carbon core) in an epoxy matrix resin. Both the fiber and resin were AVCO products (Specialty Materials Division, Lowell, Massachusetts). The resin is a 350°F (177°C) curing system which is modified for extra toughness.

Tables 19 through 32 present the data generated for this silicon carbide-epoxy system. Figures 23 through 40 illustrate the stress-strain, fatigue, and creep behavior of this material, as well as the effects of humidity aging upon selected composite properties.

Perhaps the most obvious feature of this system is the substantial decrease in property levels, particularly the resin dominated properties, at the 350°F (177°C) test temperature relative to the 260°F (127°C) test temperature.

The high 0° compressive properties exhibited by this system relative to the other systems tested reflect the beneficial effect of the much larger filament diameter compared to graphite in resisting buckling.

TABLE 19

PROCESSING CONDITIONS FOR SiC/5506 COMPOSITE LAMINATES

Composite Processing Information	
Material System - SiC/5506	SiC/Epoxy
Fiber - 5.6mil SiC Matrix - AVCO 5506	
Maximum Rated Temperature - 350°F	Prepreg by - AVCO
<p align="center">Laminate Processing Schedule</p> <p>Layup Procedure: The prepreg was stored in a closed wrapper at 0°F (-18°C). Prepreg was warmed to room temperature before removal from wrapper to prevent moisture condensation on prepreg. Plies were cut to desired size with razor knife and stacked in desired sequence (release paper removed from each ply). The stack was placed in the autoclave according to the layup system illustrated in Figure 23. The corprene edge dam serves to restrict fiber flow.</p> <p>Cure Schedule: Apply full vacuum and hold it throughout the cure cycle. Pressurize to 85 psi above bladder and heat at 4-6°F/min to 350°F. Hold at 350°F for 1 1/2 hours. Cool under pressure and vent vacuum.</p> <p>Postcure Schedule: After trimming of flash, panels were placed, unrestrained in a circulating air oven and heated to 375°F at 4-6°F/min. They were held at 375°F for four hours then cooled to room temperature.</p>	

NOTE: This cure schedule represents one which differs from that originally recommended by AVCO. Due to the slower response of the large autoclave used to fabricate our panels, the cure schedule had to be modified. The original schedule recommended by AVCO was as follows:

Apply full vacuum. Pressurize to 50 psi above bladder and heat at 4-6°F/min to 350°F, venting vacuum when temperature reaches 135°F. Hold at 350°F for 1-1/2 hours and cool under pressure.

This cure schedule, when followed in our autoclave, produced laminates having a specific gravity of 2.19 and void content of 5.7%.

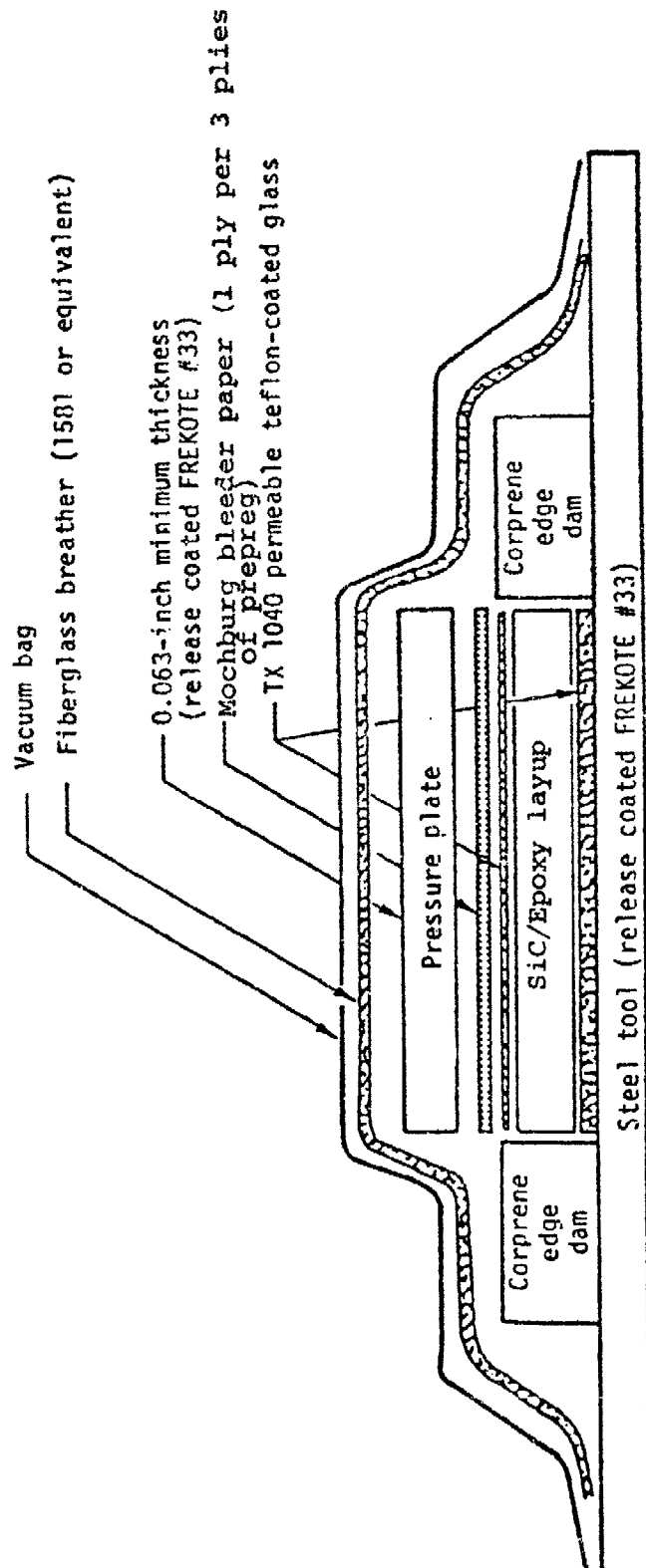


Figure 23. Layup System for SiC/5506 Laminates.

TABLE 20
PREPREG AND COMPOSITE PHYSICAL PROPERTIES

Composite Physical Property Information				
Material System - SiC/5506				
Fiber - 5.6 mil SiC	Matrix - AVCO 5506		SiC/Epoxy	
Maximum Rated Temperature - 350°F (177°C)		Prepreg by - AVCO		
Prepreg Physical Properties				
(Property)	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
Volatile Content- 1.40%	0.08%	1.34-1.52%	Advanced	Para. 4.2.3.3
Resin Content- 27.9%	0.6%	27.4-28.6%	Composite	4.2.3.2.1
Resin Flow-			Design Guide	
No. of Rolls Involved- 4				
No. of Batches Involved- 1				
Laminate Physical Properties ¹				
	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
No. of Panels- 31				
Fiber Content- 58.6% by vol.	1.3%	53.9-61.2%	Acid Digestion	
Resin Content- 19.0% by wt.	0.9%	17.4-22.0%	AFML-TR-67-243	
Void Content- 0.7% by vol.	0.7%	0.0-2.2%	D2734	ASTM
Laminate Sp. Gr.- 2.36	0.02	2.30-2.41	D792	ASTM
Fiber Sp. Gr.- 3.08 ²	As reported by manufacturer.			
Matrix Sp. Gr.-1.23	As reported by manufacturer.			
Thickness per ply-0.0064 in. 0.0002 in. 0.0061-0.0069 in---				---

¹The properties reported here represent averages for all panels of this material used throughout the program.

²Pregreg also contains a glass scrim cloth (4.5% by wt.) with a fiber specific gravity of 2.40.

HPLC ANALYSIS

SAMPLE (CONC) AVCO 5506 SAMPLE SIZE 15⁰⁰ ml
MOBILE PHASE 1 ACETONITRILE MOBILE PHASE 2 WATER
FLOW RATE 2.0 ml/min PROGRAM METH. 0
COLUMN(S) ODS DETECTOR TRACOR 970
ATTENUATION 32 WAVE LENGTH 230 nm
CHART SPEED 0.5 cm/min FULL SCALE (mV) 20 mV
DATE NOVEMBER 28 79 OPERATOR WOLFE

TIME	WATER	ACETD.
0	76%	24%
20 MIN	18%	82%
21 MIN	1%	99%

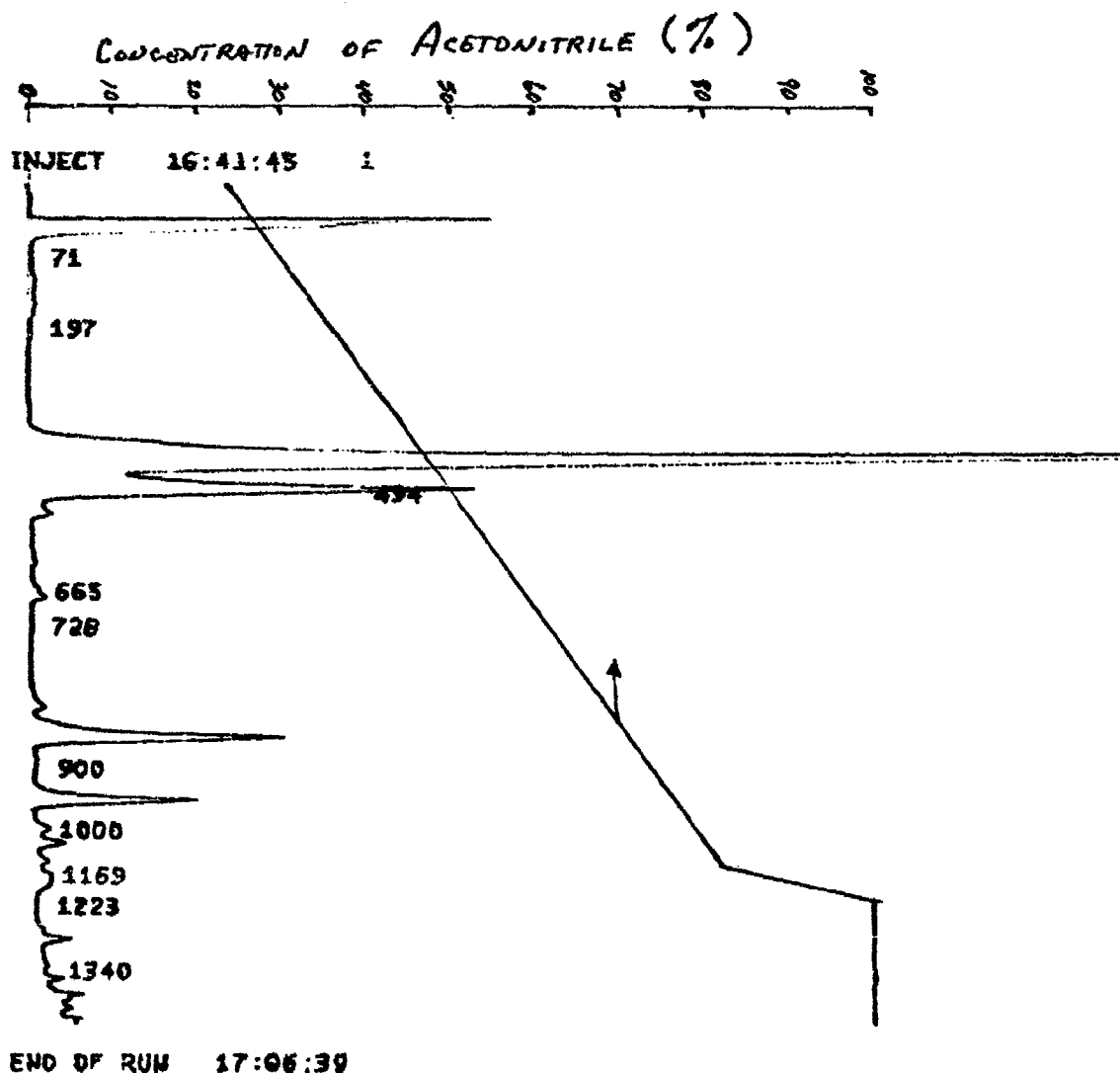


Figure 24. HPLC Analysis of AVCO 5506 Epoxy Resin.

HPLC ANALYSIS

SAMPLE (CONC.) Benzaldehyde SAMPLE SIZE 0.2 mg/ml
 MOBILE PHASE 1 Acetonitrile MOBILE PHASE 2 Water
 FLOW RATE 2.0 ml/min PROGRAM method 0
 COLUMN(S) ODS DETECTOR Tracor 970
 ATTENUATION 32 WAVE LENGTH 230 nm
 CHART SPEED 0.5 cm/min FULL SCALE (mV) 20 mV
 DATE NOVEMBER 28 79 OPERATOR WOLFE

TIME 0 WATER 76% ACETO. 24%
 20 MIN 18% 82%
 21 MIN 1% 99%
 CONCENTRATION OF ACETONITRILE (%)

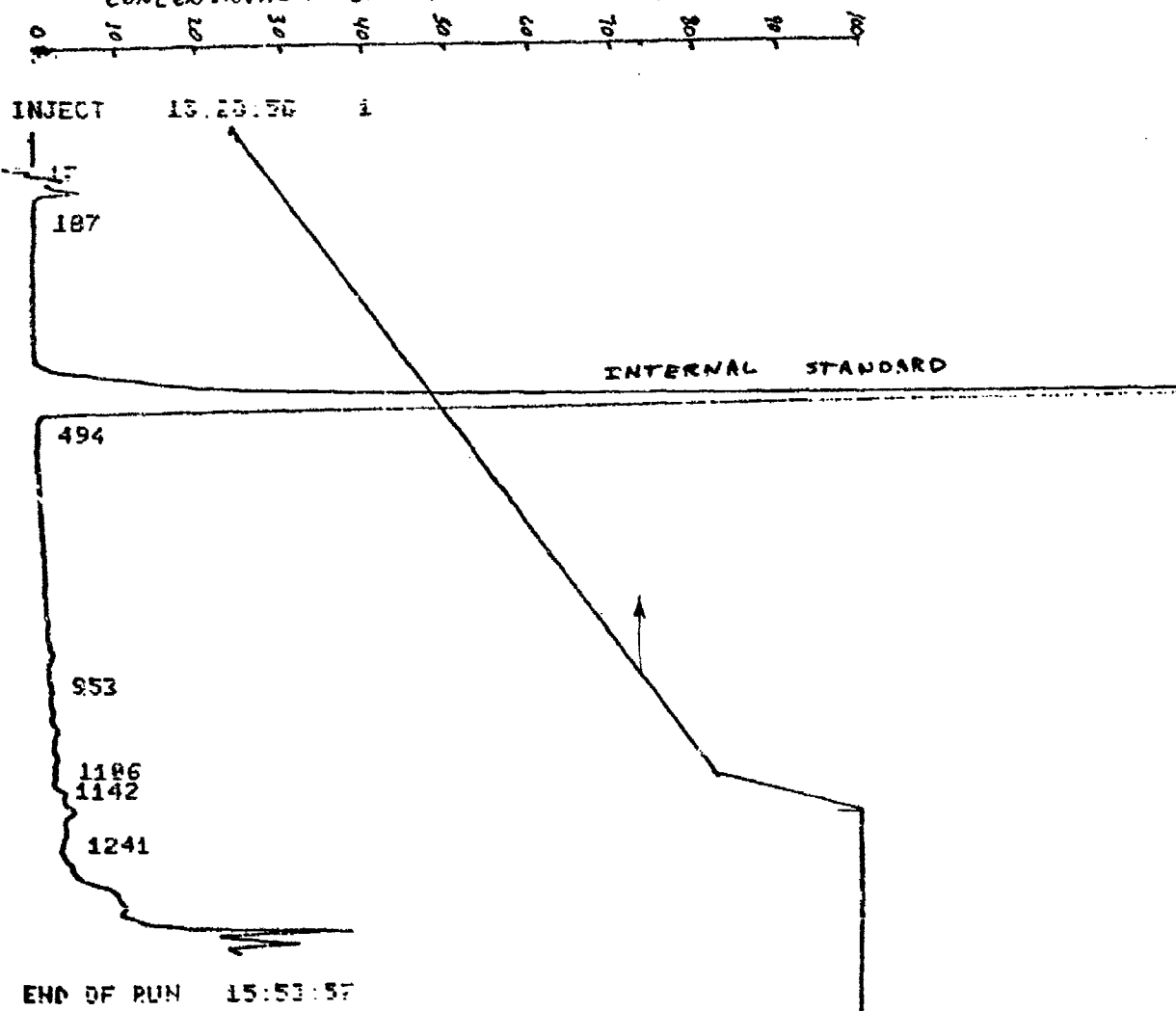


Figure 25. HPLC Analysis of Benzaldehyde.

HPLC ANALYSIS

SAMPLE (CONC.) EPON 828 SAMPLE SIZE 1.5 mg/ml
MOBILE PHASE 1 Acetonitrile MOBILE PHASE 2 Water
FLOW RATE 2.0 ml/min PROGRAM METH 0
COLUMN(S) ODS DETECTOR Tracor 970
ATTENUATION 32 WAVE LENGTH 280 nm
CHART SPEED 0.5 cm/min FULL SCALE (mV) 20mV
DATE DEC 3 79 OPERATOR WOLFE

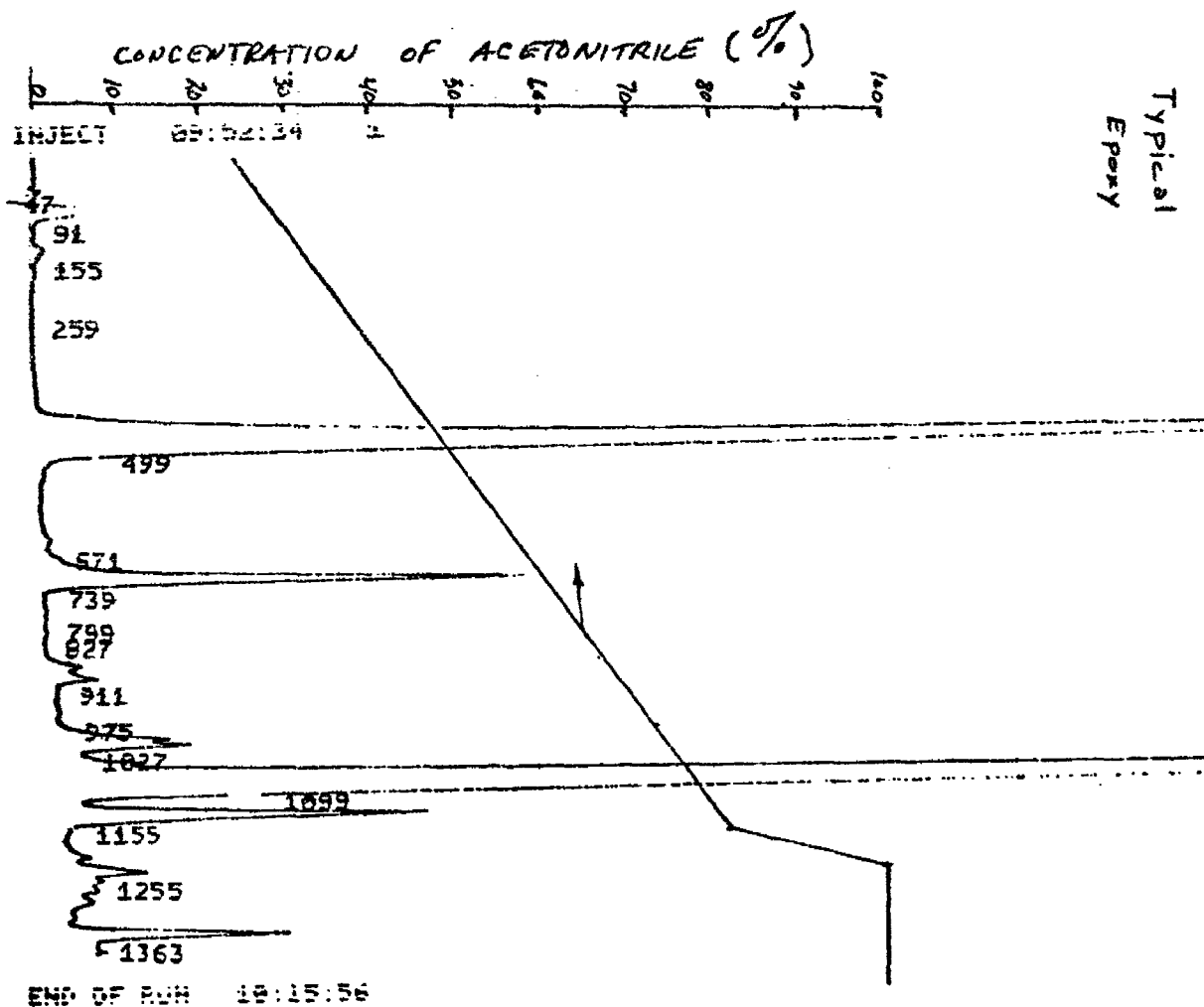


Figure 26. HPLC Analysis of Epon 828 Epoxy Resin.

TABLE 21
TENSILE PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties				
Material System - SiC/5506		Prepreg by - AVCO	SiC/Epoxy	
Fiber - 5.6 mil SiC Matrix - AVCO 5506		Laminate Sp. Gr. - 2.38		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0062 inch		
Resin Content - 18.8% by wt.		No. of panels from which specimens were tested		
Fiber Content - 59.9% by vol.		in this table - 6		
Void Content - 0.3% by vol.				
Thickness of each type specimen: 0° - 6 ply		90° - 15 ply		
TENSION: 0°				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
F_x^{tu} [ksi] (MPa)	[221.6] (1527)	[229.1] (1578)	[190.6] (1313)	[174.5] (1202)
Std. Dev. [ksi] (MPa)	[18.2] (125)	[8.4] (58)	[13.3] (92)	[11.0] (76)
Range [ksi] (MPa)	[198.8 - 235.8] (1370 - 1625)	[220.3 - 241.7] (1518 - 1665)	[178.8 - 205.0] (1232 - 1412)	[161.7 - 181.0] (1114 - 1247)
No. of Specimens	5	5	3 ¹	3 ¹
F_y^{tpl} [ksi] (MPa)	[129.5] (892)	[71.4] (492)	[86.7] (59)	[57.4] (395)
Std. Dev. [ksi] (MPa)	[36.2] (249)	[20.4] (141)	[12.5] (86)	[19.5] (134)
No. of Specimens	5	5	3	3
E_x^t [ksi] (GPa)	[32.3] (223)	[33.4] (230)	[33.2] (229)	[33.0] (227)
Std. Dev. [ksi] (GPa)	[1.1] (7.6)	[1.3] (9.0)	[0.4] (2.8)	[2.4] (1.7)
No. of Specimens	5	5	3	3
ϵ_x^{tu} [in/in] (µm/cm)	7600	7660	6800	5130 ²
Std. Dev.	190	760	—	N.A.
No. of Specimens	5	5	2	3
ν_{xy}^t	0.22	0.23	0.25	0.32
Std. Dev.	0.03	0.02	0.05	0.15
No. of Specimens	5	4	3	3
Test Method	ASTM D3039			
Reference				
TENSION: 90°				
F_y^{tu} [ksi] (MPa)	[9.78] (67.4)	[9.71] (66.9)	[6.44] (44.4)	[4.34] (29.9)
Std. Dev. [ksi] (MPa)	[1.42] (9.78)	[0.51] (3.5)	[0.10] (0.7)	[0.40] (2.8)
Range	[8.31 - 11.55] (57.3 - 79.6)	[8.92 - 10.43] (61.9 - 71.9)	[6.34 - 6.56] (43.7 - 45.2)	[3.84 - 4.92] (26.5 - 33.9)
No. of Specimens	5	5	5	5
F_y^{tpl} [ksi] (MPa)	[6.17] (42.5)	[4.24] (29.2)	[2.84] (19.6)	[1.75] (12.1)
Std. Dev. [ksi] (MPa)	[1.21] (8.3)	[0.62] (4.3)	[0.17] (1.2)	[0.13] (0.9)
No. of Specimens	5	5	5	5
E_y^t [ksi] (GPa)	[3.86] (26.6)	[2.99] (20.6)	[1.97] (13.6)	[1.04] (7.2)
Std. Dev. [ksi] (GPa)	[0.12] (0.83)	[0.10] (0.69)	[0.16] (1.1)	[0.13] (0.9)
No. of Specimens	5	5	5	5
ϵ_y^{tu} [in/in] (µm/cm)	2,748	3,727	4,695	7,550
Std. Dev.	470	194	373	975
No. of Specimens	5	5	5	5
ν_{yx}^t	0.025 ³	0.021 ³	0.015 ³	0.010 ³
Std. Dev.				
No. of Specimens				
Test Method	ASTM D3039			
Reference				

¹Excludes data from two specimens from bad panel (had very high void content).

²Strain gages failed before end of test on two of three specimens.

³Computed using elastic moduli and longitudinal Poisson's ratio.

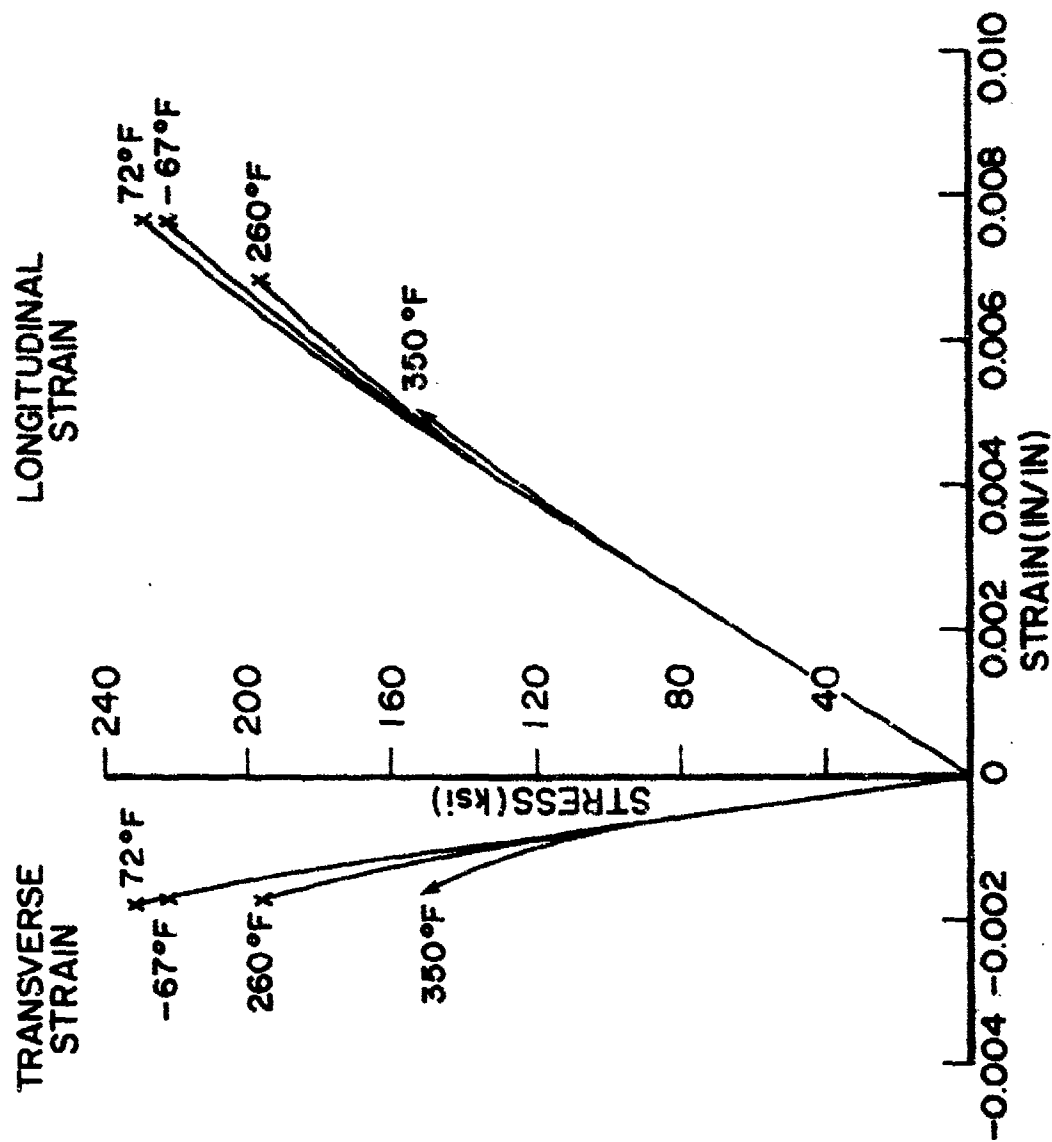


Figure 27. Tensile Stress-Strain Curves for Unidirectional SiC/5506 Composite
Laminates: 0° Fiber Orientation.

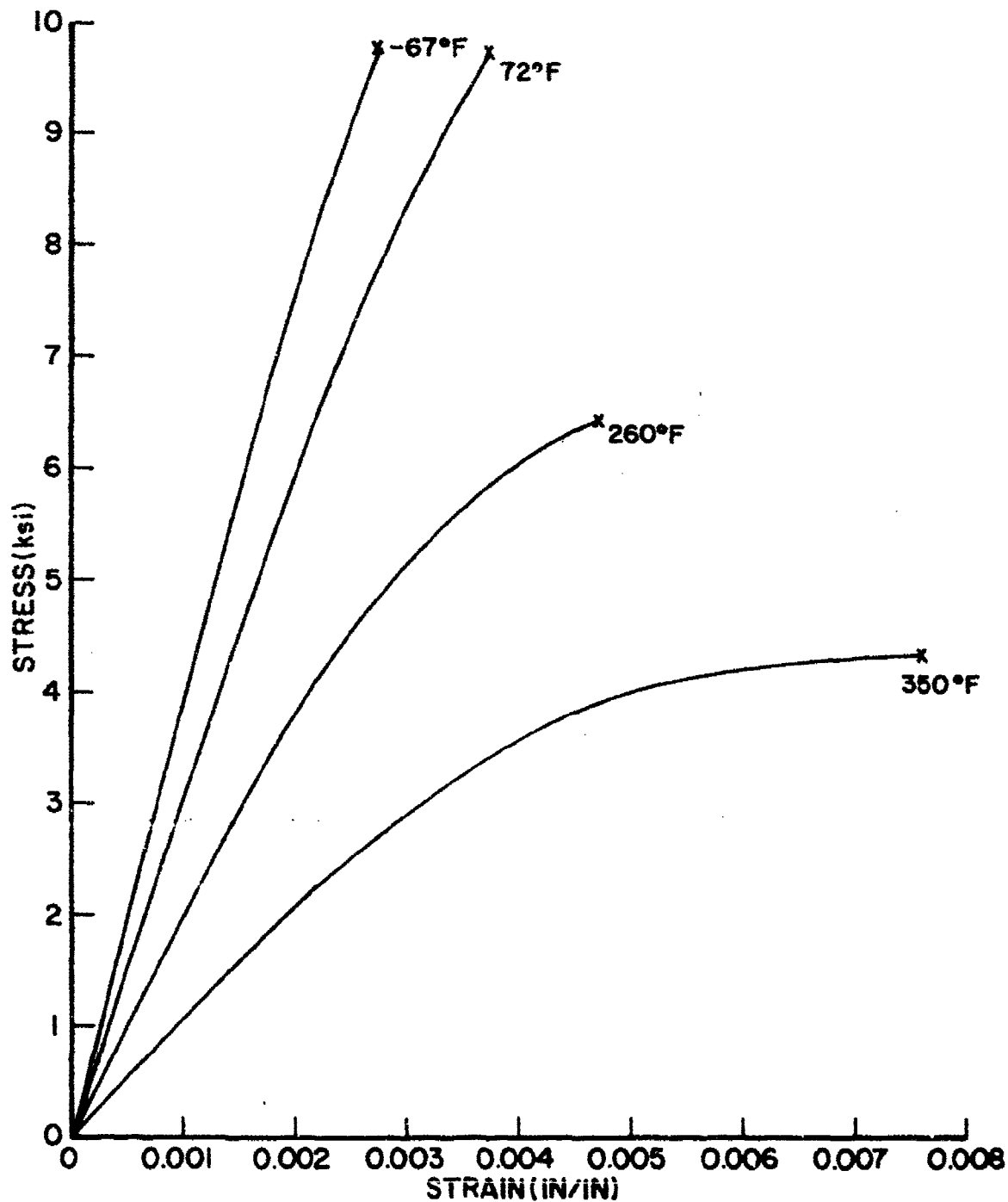


Figure 28. Tensile Stress-Strain Curves for Unidirectional SiC/5506 Composite Laminates: 90° Fiber Orientation.

TABLE 22
TENSILE PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties				
Material System - SiC/5506		Prepreg by - AVCO		SiC/Epoxy
Fiber - 5.6 mil SiC Matrix - AVCO 5506		Laminate Sp. Gr. - 2.33		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0064 inch		
Resin Content - 20.2% by wt.		No. of panels from which specimens were tested		
Fiber Content - 56.8% by vol.		in this table - 4		
Void Content - 0.7% by vol.		Thickness of specimen - 8 ply		
TENSION: +45°				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
P_x^{tu} [ksi] (MPa)	[19.72] (135.9)	[17.32] (119)	[11.52] (79)	[7.93] (54.6)
Std.Dev. [ksi] (MPa)	[1.19] (8.2)	[0.58] (4.0)	[0.34] (5.8)	[0.18] (1.2)
Range [ksi] (MPa)	[17.69 - 20.63] (121.9 - 142.1)	[16.52-17.95] (114 - 124)	[10.66-12.45] (79 - 99)	[7.67 - 8.17] (52.8 - 56.3)
No. of Specimens	5	5	5	5
F_x^{tpl} [ksi] (MPa)	[6.25] (43.1)	[5.14] (35)	[1.59] (11)	[0.93] (6.4)
Std.Dev. [ksi] (MPa)	[0.57] (3.9)	[0.92] (6.3)	[0.37] (2.5)	[0.32] (2.2)
No. of Specimens	5	5	5	5
E_x^t [Msi] (GPa)	[3.71] (25.6)	[2.97] (20)	[1.63] (11)	[0.51] (3.5)
Std.Dev. [Msi] (GPa)	[0.22] (1.5)	[0.30] (2.1)	[0.27] (1.9)	[0.19] (1.3)
No. of Specimens	5	5	5	5
ϵ_x^{tu} [μ in/in] (μ cm/cm)	8,600	15,510	35,100 ¹	30,900 ¹
Std. Dev.	1,234	544	7,280	6,540
No. of Specimens	5	5	5	5
ν_{xy}^t	0.66	0.74	0.89	0.74
Std. Dev.	0.07	0.08	0.11	0.11
No. of Specimens	5	5	5	5
Test Method	ASTM D3039			
Reference				

¹Ultimate strain exceeded limits of strain gages.

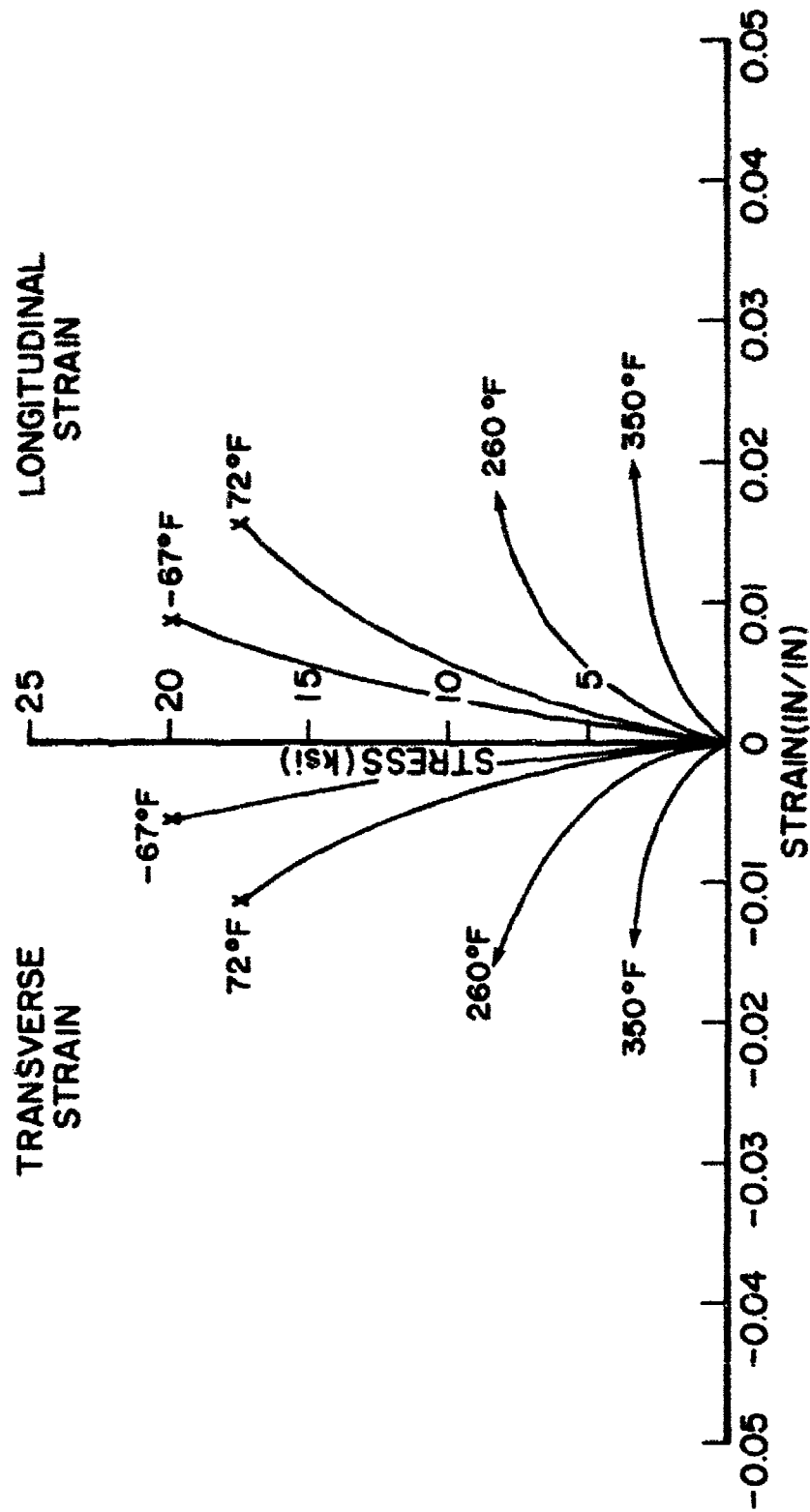


Figure 29. Tensile Stress-Strain Curves for Bidirectional SiC/5506 Composite
Laminates: +45° Fiber Orientation.

TABLE 23

TENSILE PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties				
Material System - SiC/5506		Prepreg Ly - AVCO		SiC/Epoxy
Fiber - 5.6 mil SiC		Matrix - AVCO 5506		
Maximum Rated Temperature - 350°F (177°C)		Laminate Sp. Gr. - 2.35		
Resin Content - 18.9% by wt.		Nominal Ply Thickness - 0.0062 inch		
Fiber Content - 58.6% by vol.		No. of panels from which specimens were tested		
Void Content - 0.9% by vol.		in this table - 8		
Thickness of each type specimen: 20 ply				
TENSION: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0) _g				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
σ_{xx}^{tu} [ksi] (MPa)		[119.3] (822)	[117.2] (807)	[107.2] (739)
Std. Dev. [ksi] (MPa)		[8.2] (56)	[7.7] (53)	[6.0] (41)
Range [ksi] (MPa)		[108.2 - 125.6]	[107.4 - 126.2]	[102.1 - 115.6]
No. of Specimens		[745 - 865] 4	[740 - 870] 5	[703 - 796] 4
σ_{xx}^{tpl} [ksi] (MPa)		[38.6] (266)	[49.1] (338)	[60.3] (415)
Std. Dev. [ksi] (MPa)		[18.8] (130)	[15.0] (102)	[11.1] (76)
No. of Specimens		5	5	4
ϵ_{xx}^t [ksi] (GPa)		[20.5] (141)	[19.0] (131)	[18.1] (125)
Std. Dev. [ksi] (GPa)		[2.0] (14)	[0.4] (2.8)	[0.6] (4)
No. of Specimens		5	5	4
ϵ_{xx}^{tu} [in/in] ($\mu\text{cm/cm}$)		5725	5740	5190
Std. Dev.		100	100	670
No. of Specimens		4	5	4
ν_{xy}		0.31	0.45	0.40
Std. Dev.		0.10	0.11	0.06
No. of Specimens		4	5	4
Test Method	ASTM D3039			
Reference				
TENSION: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0) _g with hole ¹				
σ_y^{tu} [ksi] (MPa)		[102.5] (706)		
Std. Dev. [ksi] (MPa)		[3.5] (24)		
Range		[97.6 - 105.8]		
No. of Specimens		[672 - 729] 5		
σ_y^{tpl} [ksi] (MPa)				
Std. Dev. [ksi] (MPa)				
No. of Specimens				
ϵ_y^t [ksi] (GPa)				
Std. Dev. [ksi] (GPa)				
No. of Specimens				
ϵ_y^{tu} [in/in] ($\mu\text{cm/cm}$)				
Std. Dev.				
No. of Specimens				
ν_{yx}				
Std. Dev.				
No. of Specimens				
Test Method	ASTM D3039			
Reference				

¹ These specimens had a 0.1915 inch (0.491 cm) hole in the center of the test section. Stresses were calculated using net cross-sectional area.

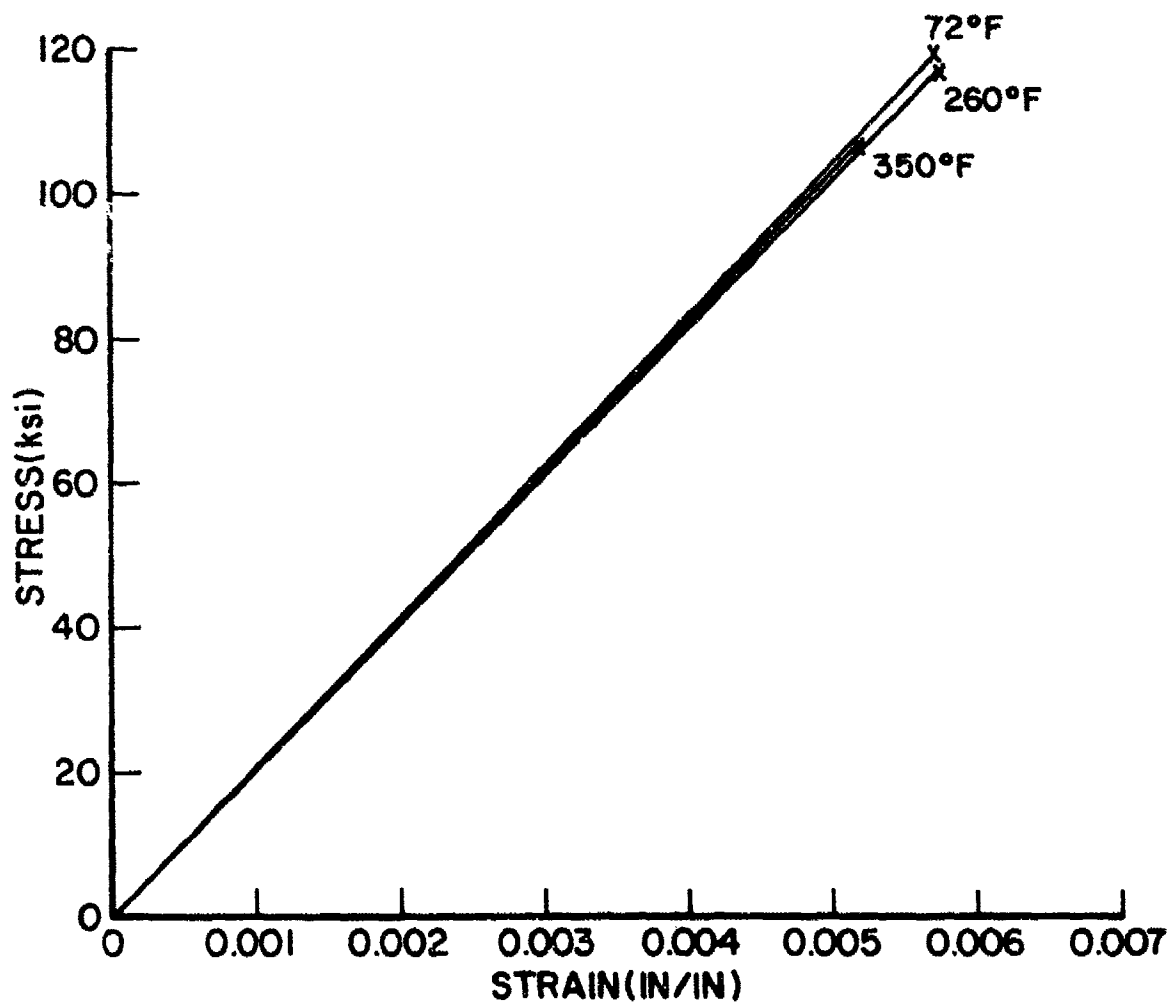


Figure 30 . Tensile Stress-Strain Curves for Multidirectional SiC/5506 Composite Laminates: (0,45,-45,0,0,-45,45,0,90,0)_s Fiber Orientation.

TABLE 24
COMPRESSIVE PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties					
Material System - SiC/5506		Prepreg by - AVCO		SiC/Epoxy	
Fiber - 5.6 mil SiC Matrix - AVCO 5506		Laminate Sp. Gr. - 2-38			
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0061 inch			
Resin Content - 18.5% by wt.		No. of panels from which specimens were tested			
Fiber Content - 59.7% by vol.		in this table - 1			
Void Content - 0.1% by vol.					
Thickness of each type specimen: 0° - 16 ply ; 90° - 16 ply					
COMPRESSION: 0°					
		-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F_x^{cu}	[ksi](MPa)	[391] (2694)	[326] (2246)	[232] (1598)	[131] (903)
Std.Dev.	[ksi](MPa)	[36] (248)	[20] (138)	[8] (55)	[29] (200)
Range	[ksi](MPa)	[335 - 435] (2308 - 2997)	[305 - 350] (2171 - 2412)	[221 - 240] (1523 - 1654)	[97 - 154] (668 - 1061)
No. of Specimens		5	5	5	5
F_x^{cpl}	[ksi](MPa)	[239] (1647)	[117] (806)	[141] (1269)	[95] (655)
Std.Dev.	[ksi](MPa)	[65] (448)	[61] (420)	[32] (220)	[9] (62)
No. of Specimens		5	3	5	5
E_x^c	[Msi](GPa)	[33.1] (228)	[35.5] (245)	[33.9] (233)	[34.0] (234)
Std.Dev.	[Msi](GPa)	[3.0] (21)	[2.8] (19)	[3.2] (22)	[8.0] (55)
No. of Specimens		5	5	5	5
ϵ_x^{cu}	[μ in/in](μ m/cm)	12,920 ^{+1,2}	6,220 ⁺³	7,760	3,560 ^{+1,2}
Std. Dev.		4,310	1,730	1,110	300
No. of Specimens		5	5	5	5
Test Method Reference	ASTM D3410				
COMPRESSION: 90°					
F_y^{cu}	[ksi](MPa)	[56.7] (391)	[34.4] (237)	[25.7] (177)	[19.8] (136)
Std.Dev.	[ksi](MPa)	[3.6] (25)	[1.7] (12)	[1.5] (10)	[1.2] (8)
Range		[53.4-62.3] (368-429)	[31.8-36.3] (219-250)	[23.0-26.9] (158-185)	[18.7-21.6] (129-149)
No. of Specimens		5	5	5	5
F_y^{cpl}	[ksi](MPa)	[15.5] (107)	[18.0] (124)	[14.3] (99)	[9.4] (65)
Std.Dev.	[ksi](MPa)	[7.1] (49)	[9.1] (63)	[3.2] (22)	[2.2] (15)
No. of Specimens		5	5	5	5
E_y^c	[Msi](GPa)	[3.41] (23.5)	[3.58] (24.7)	[2.40] (16.5)	[1.88] (13.0)
Std.Dev.	[Msi](GPa)	[0.97] (6.7)	[0.60] (4.1)	[0.12] (0.8)	[0.32] (2.2)
No. of Specimens		5	5	5	5
ϵ_y^{cu}	[μ in/in](μ m/cm)	22,200	9,240 ⁺³	20,540 ^{+1,2}	27,100
Std. Dev.		3,340	4,820	3,620	3,070
No. of Specimens		5	5	5	4
Test Method Reference	ASTM D3410				

¹Ultimate strain values represent ~~maximum~~ observed strain rather than ultimate values.

²Two of five specimens exhibited evidence of buckling.

³Tab debonded during first test attempt at about 65% of ultimate strength. Tabs were rebonded with a different adhesive and the tests were rerun. Modulus and proportional limit were obtained from data recorded during first test. Ultimate strain values could not be obtained during second test because of strain gage damage when first set of tabs debonded. Value reported represents strain when tabs debonded on first test.

⁴Three of five specimens exhibited evidence of buckling.

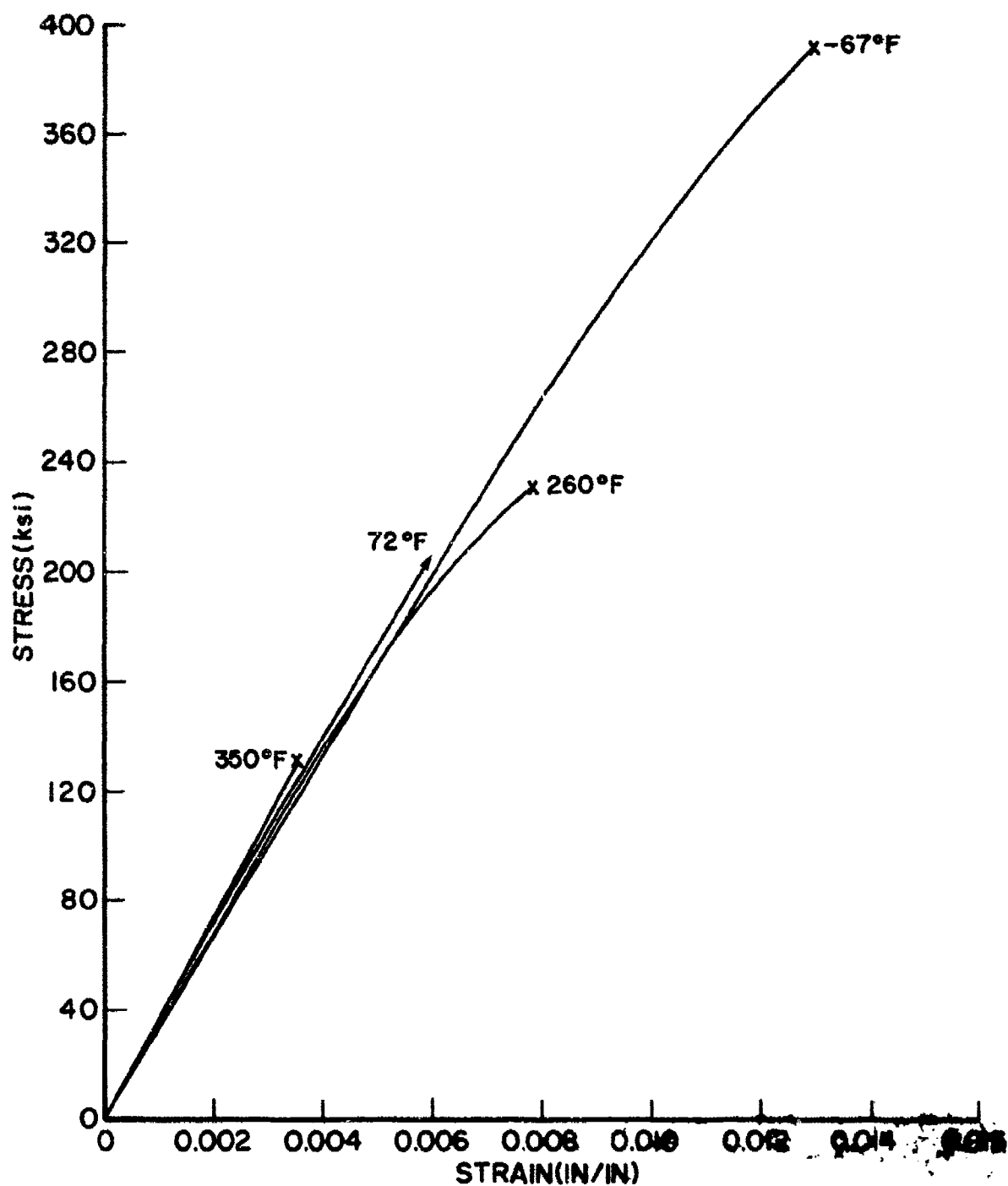


Figure 31. Compressive Stress-Strain Curves for Undirectional SiC/5506 Composite Laminates: 0° Fiber Orientation.

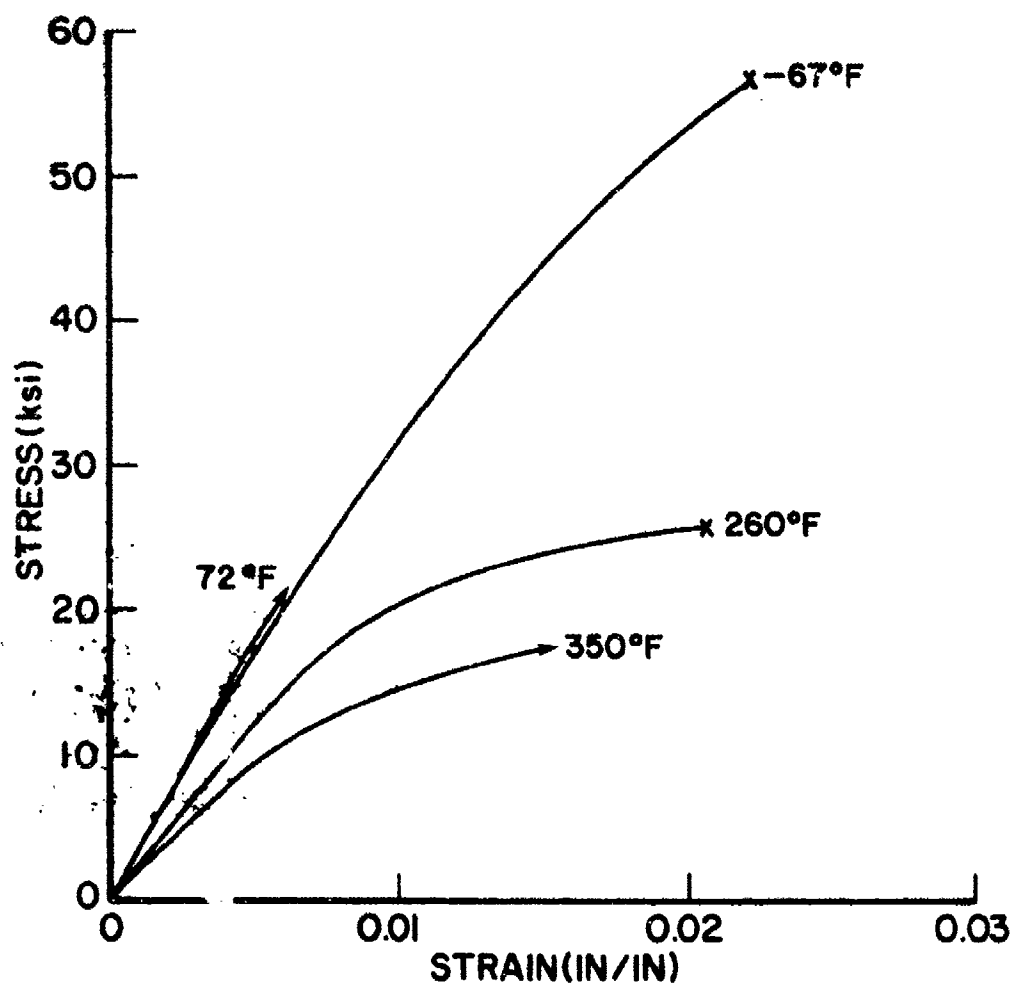


Figure 32. Compressive Stress-Strain Curves for Unidirectional SiC/5506 Composite Laminates: 90° Fiber Orientation.

TABLE 25
FLEXURAL PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties				
Material System - SiC/5506		Prepreg by - AVCO	SiC/Epoxy	
Fiber - 5.6mil SiC Matrix - AVCO 5506		Laminate Sp. Gr. - 2.37		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0069 inch		
Resin Content - 19.4% by wt.		No. of panels from which specimens were tested		
Fiber Content - 58.9% by vol.		in this table - 2		
Void Content - ± 0% by vol.				
Thickness of each type specimen: 0° - 14 ply ; 90° - 14 ply				
FLEXURE: 0°				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
R_x^{fu} [ksi] (MPa)	[324.9] (2239)	[314.6] (2168)	[189.3] (1304) ^{1,2}	[120.0] (827) ^{1,2}
Std.Dev. [ksi] (MPa)	[8.1] (56)	[10.1] (69.6)	[21.6] (148)	[6.5] (45)
Range [ksi] (MPa)	[317.9-336.4] (2190-2318)	[298.0-324.1] (2053-2233)	[166.1-217.2] (1144-1497)	[109.9-126.2] (757-870)
No. of Specimens	5	5	5	5
E_x^f [Msi] (GPa)	[31.9] (220)	[31.8] (219)	[29.6] (204)	[30.4] (209)
Std.Dev. [Msi] (GPa)	[0.71] (4.9)	[0.48] (3.3)	[0.94] (6.5)	[1.8] (12)
No. of Specimens	5	5	5	5
Test Method Reference	4 pt. flexure Design Guide, Jan. 1971 } Corresponds to ASTM D790 except for loading points and loading speed			
FLEXURE: 90°				
R_y^{fu} [ksi] (MPa)	[15.86] (109)	[14.53] (100)	[11.08] (76)	[6.96] (48) ²
Std.Dev. [ksi] (MPa)	[1.3] (8.9)	[0.78] (5.4)	[1.35] (9.3)	[0.63] (4.3)
Range [ksi] (MPa)	[14.94-17.26] (103-119)	[13.45-15.53] (93-107)	[9.96-13.21] (69-91)	[6.09-7.74] (42-53)
No. of Specimens	5	5	5	5
E_y^f [Msi] (GPa)	[2.71] (19)	[2.34] (16)	[1.44] (9.9)	[0.85] (5.9)
Std.Dev. [Msi] (GPa)	[0.18] (1.2)	[0.13] (0.9)	[0.18] (1.2)	[0.03] (0.2)
No. of Specimens	5	5	5	5
Test Method Reference	4 pt. flexure Design Guide, Jan. 1971 } Corresponds to ASTM D790 except for loading points and loading speed			

¹Specimens underwent abnormally large deformations and exhibited interlaminar shear failure rather than tensile failure on bottom ply.

²See following table for flexure properties using a three-point loading mode.

TABLE 26
FLEXURAL PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties				
Material System - SiC/5506		Prepreg by - AVCO	SiC/Epoxy	
Fiber - 5.6 mil SiO ₄ matrix - AVCO 5506		Laminate Sp. Gr. - 2.41		
Maximum Rated Temperature - 350°F		Nominal Ply Thickness - 0.0061 inch		
Resin Content - 17.4% by wt.		No. of panels from which specimens were tested in this table - 1		
Fiber Content - 61.1% by vol.				
Void Content - 0.5% by vol.				
Thickness of each type specimen: 0° - 14 plies; 90° - 14 plies				
FLEXURE: 0°				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
F_x^{fu} [ksi] (MPa)			[316.7] (2182)	[175.5] (1209) ¹
Std.Dev. [ksi] (MPa)			[7.2] (49)	[5.4] (37)
Range [ksi] (MPa)			[308.7-322.9] (2127-2225)	[173.8-182.9] (1197-1260)
No. of Specimens			4	4
E_x^f [Msi] (GPa)			[29.0] (200)	[24.6] (169)
Std.Dev. [Msi] (GPa)			[0.9] (6)	[0.8] (6)
No. of Specimens			4	4
Test Method Reference	ASTM D790, Method 1 (3 pt. flexure)			
FLEXURE: 90°				
F_y^{fu} [ksi] (MPa)				[9.89] (68)
Std.Dev. [ksi] (MPa)				[1.51] (10)
Range [ksi] (MPa)				[8.20-11.30] (56-78)
No. of Specimens				4
E_y^f [Msi] (GPa)				[1.03] (7.1)
Std.Dev. [Msi] (GPa)				[0.11] (0.8)
No. of Specimens				4
Test Method Reference	ASTM D790, Method 1 (3 pt. flexure)			

¹Specimens failed by interlaminar shear rather than tensile failure on bottom ply.

TABLE 27
SHEAR PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties				
Material System - SiC/5506		Prepared by - KUDCO		SiC/5506
Fiber - 5.6 mil SiC Matrix - KUDCO 5506		Laminates Sp. Gr. - 2.33		
Maximum Tested Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0064 inch		
Resin Content - 18.3% by wt.		No. of panels from which specimens were tested in this table - 4		
Fiber Content - 60.1% by vol.				
Void Content - ~0				
Thickness of each type specimen: Inplane - 8 ply ; Interlaminar - 15 ply				
INPLANE SHEAR				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
τ_{xy} [ksi] (MPa)	[9.86] (67.9)	[8.66] (59.7)	[5.76] (39.5)	[3.97] (27.3)
Std. Dev. [ksi] (MPa)	[0.60] (4.1)	[0.29] (4.0)	[0.42] (2.9)	[0.09] (0.6)
Range [ksi] (MPa)	[8.85 - 10.32] (60.9 - 71.1)	[8.26 - 8.98] (56.9 - 61.9)	[5.33 - 6.23] (39.5 - 49.5)	[3.83 - 4.09] (26.4 - 28.2)
No. of Specimens	5	5	5	5
G_{xy}^* [ksi] (GPa)	[1.07] (7.37)	[0.74] (5.10)	[0.36] (2.46)	[0.14] (0.98)
Std. Dev. [ksi] (GPa)	[0.003] (0.02)	[0.06] (0.41)	[0.04] (0.25)	[0.03] (0.21)
No. of Specimens	5	5	5	5
Test Method	+45° straight-sided tension			
Reference	J. Composite Mtl's. [Vol. 6, p. 252 & Vol. 7, p. 124]			
INTERLAMINAR SHEAR				
τ_{isu} [ksi] (MPa)	[21.3] (147)	[15.0] (103)	[9.1] (63)	[8.0] (55)
Std. Dev. [ksi] (MPa)	[0.2] (1.4)	[0.2] (1.4)	[0.3] (2.1)	[0.4] (2.8)
Range	[21.1 - 21.7] (145 - 150)	[14.8 - 15.3] (102 - 105)	[8.8 - 9.6] (61 - 66)	[7.5 - 8.6] (52 - 59)
No. of Specimens	5	5	5	5
Test Method	ASTM D2344			
Reference				

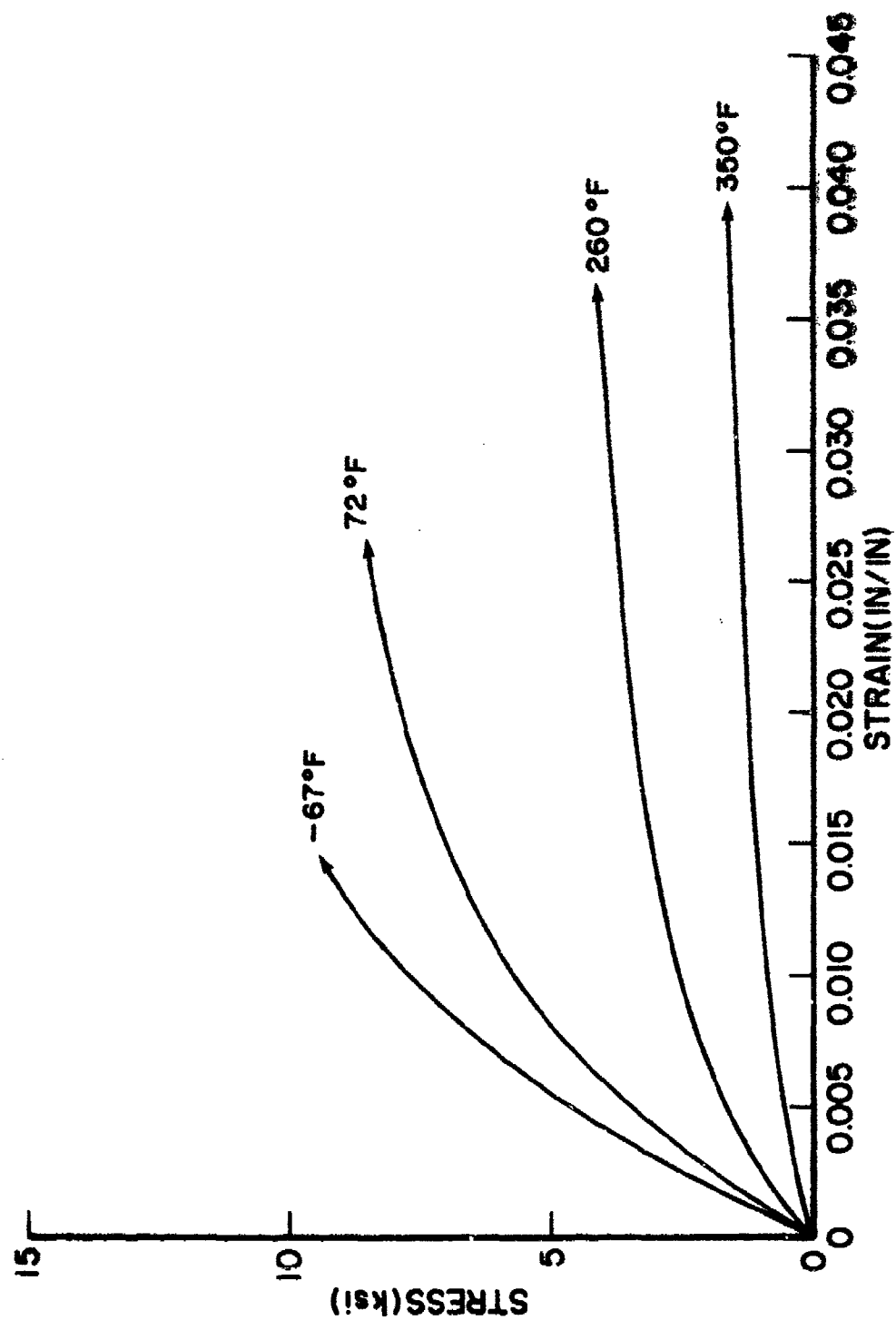


Figure 33. Inplane Shear Stress-Strain Curves for SiC/5506 Composite Laminates.

TABLE 28

**TENSILE, COMPRESSIVE AND SHEAR PROPERTIES OF SIC/5506
COMPOSITE LAMINATES AFTER HUMIDITY AGING**

Composite Material Properties									
Material System - SIC/5506		Prepreg by - AVCO		SIC/Epoxy		COMPRESSION: 90°			
Fiber - 5.6 mil SIC Matrix - AVCO 5506 Laminate Sp. Gr. - 2.38		Maximum Rated Temperature - 350°F		Nominal Ply Thickness - 0.0062 inch		72°F (22°C)		160°F (71°C)	
Resin Content - 18.8% by wt. (177°C)		No. of panels from which specimens were tested in this table - 7		Fiber Content - 59.5% by vol.		Exposure Time (hrs)		1752	
Void Content - 0.3% by vol.		Aging Conditions - 160°F (71°C) 100% R.H.		Thickness of each type specimen: Tension - 15 ply; Compr. - 16 ply; Shear - 15 ply		Wt. Gain (% of orig. dry wt.)		1.31 ¹	
						Std. Dev. (%)		0.08	
						No. of Specimens		4	
						F _{cu} [ksi] (MPa)		[24.5] (169)	
						Std. Dev. [ksi] (MPa)		[0.8] (6)	
						Range		[23.8-25.7] (164-177)	
						No. of Specimens		5	
						F _{cp} [ksi] (MPa)		[10.3] (71)	
						Std. Dev. [ksi] (MPa)		[3.8] (26)	
						No. of Specimens		5	
						E _y [ksi] (GPa)		[2.85] (20)	
						Std. Dev. [ksi] (GPa)		[0.6] (4)	
						No. of Specimens		5	
						E _{cu} [in/in] (μm/cm)		20,480	
						Std. Dev.		6,650	
						No. of Specimens		5	
						Test Method		ASTM D3410	
						Reference			
								INTERLAMINAR SHEAR	
						Exposure Time (hrs)		240	
						Wt. Gain (% of orig. dry wt.)		1.07 ¹	
						Std. Dev. (%)		0.31	
						No. of Specimens		10	
						F _{1au} [ksi] (MPa)		[12.06] (83.1)	
						Std. Dev. [ksi] (MPa)		[0.70] (4.9)	
						Range		[10.74-12.54] (7.01-7.33)	
						No. of Specimens		10	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std. Dev.		258	
						No. of Specimens		5	
						Test Method		ASTM D3039	
						Reference			
						E _{1u} [in/in] (μm/cm)		2763	
						Std			

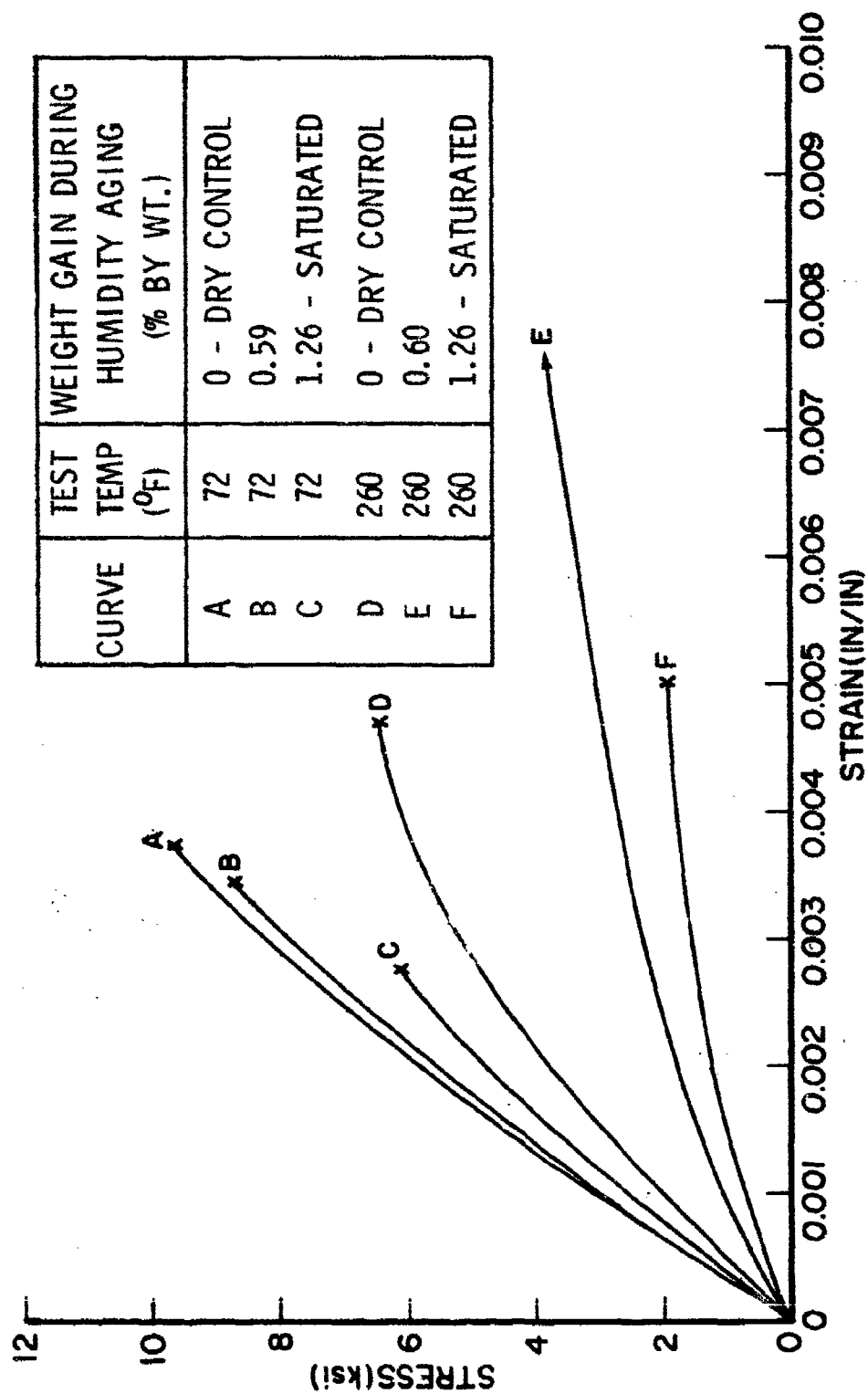


Figure 34. Tensile Stress-Strain Curves for Unidirectional SiC/5506 Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

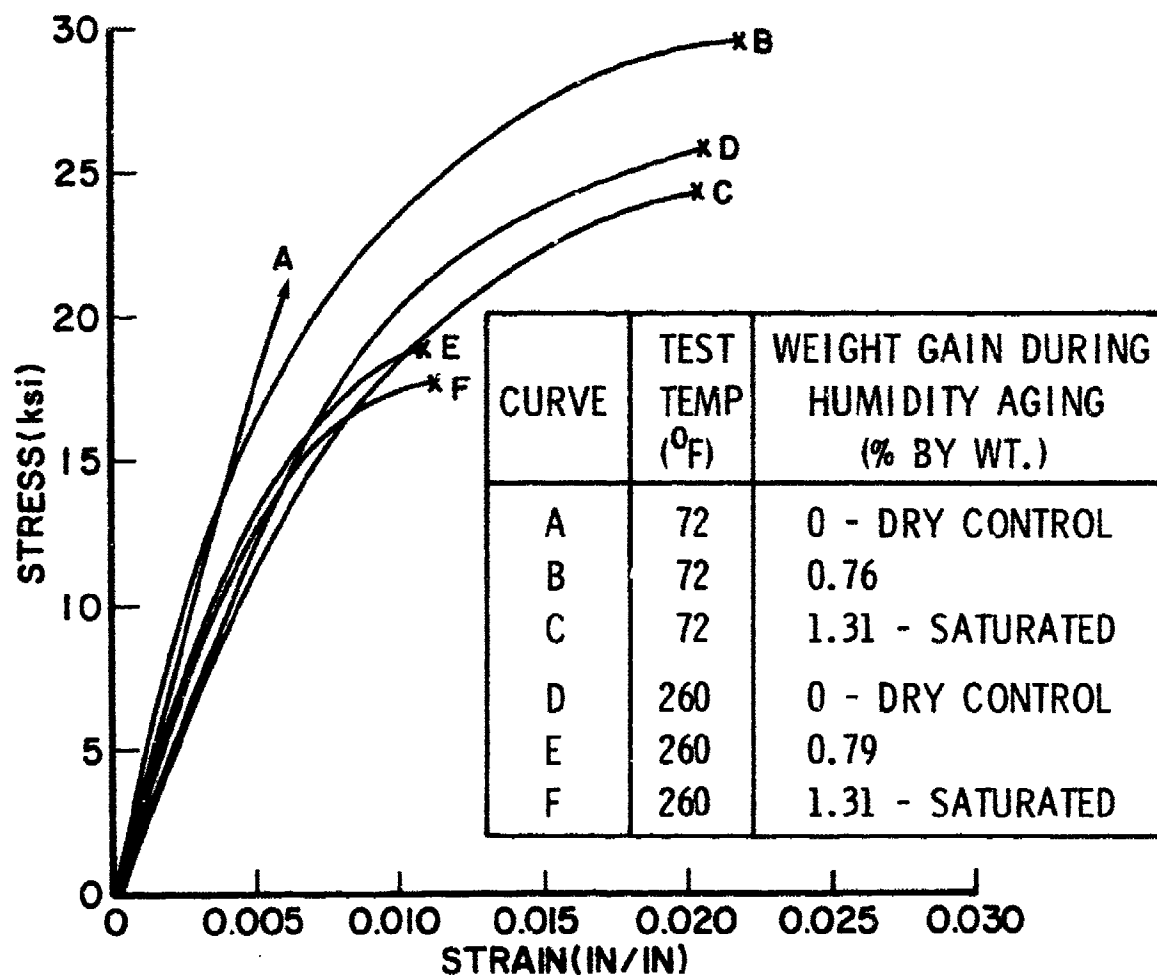


Figure 35. Compressive Stress-Strain Curves for Unidirectional SiC/5506 Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

TABLE 29
CREEP PROPERTIES OF SiC/5506 COMPOSITE LAMINATES

Composite Material Properties			
Material System - SiC/5506		Prepreg by - AVCO	SiC/Epoxy
Fiber - 5.6 mil SiC Matrix - AVCO 5506		Laminate Sp. Gr. - 2.34	Nominal Ply Thickness - 0.0065 inch
Maximum Temperature Rating - 350°F (177°C)		No. of panels from which specimens were tested in this table - 16	
Resin Content - 19.2% by wt.		Thickness of each type specimen:	
Fiber Content - 58.0% by vol.		(0/+45/90) - 20 ply	
Void Content - 1.1% by vol.		+45° - 8 ply	
Test Method - Straight-sided tension			
Reference - ASTM D2290 and D3039			
CREEP			
Temperature		(0,+45,-45,0,0,-45,+45,0,90,0)°	+45°
72°F (22°C)	Stress Level [ksi] (MPa)	[83.5] (575)	[13.86] (95.50)
	Creep Strain, 500 hr(%)	0.0121	1.0280
	No. of Specimens	3	3
	Residual Strength [ksi] (MPa)	[105.3] (726)	[16.13] (117)
	No. of Specimens	3	3
	Stress Level [ksi] (MPa)	171.6 (493)	[12.13] (83.58)
	Creep Strain, 500 hr(%)	0.0102	0.5312
	No. of Specimens	2	3
	Residual Strength [ksi] (MPa)	[102.7] (708)	[17.24] (119)
	No. of Specimens	2	3
	Stress Level [ksi] (MPa)	[59.6] (411)	[10.39] (71.59)
	Creep Strain, 500 hr(%)	0.0070	0.4480
	No. of Specimens	3	3
	Residual Strength [ksi] (MPa)	[102.5] (706)	[17.32] (119)
	No. of Specimens	3	3
260°F (127°C)	Stress Level [ksi] (MPa)	[82.0] (565)	[8.07] (55.60)
	Creep Strain, 500 hr(%)	0.0313 ⁶	---
	No. of Specimens	1	---
	Residual Strength [ksi] (MPa)	[106.6] (734)	[17.86] (123)
	No. of Specimens	3	1
	Stress Level [ksi] (MPa)	[70.3] (484)	[5.76] (39.69)
	Creep Strain, 500 hr(%)	0.0180	3.2171 ²
	No. of Specimens	15.7	2
	Residual Strength [ksi] (MPa)	[101.4] (699)	[15.87] (109)
	No. of Specimens	2	3
	Stress Level [ksi] (MPa)	[58.6] (404)	[5.12] (35.28)
	Creep Strain, 500 hr(%)	0.0216	1.3228 ²
	No. of Specimens	3	2
	Residual Strength [ksi] (MPa)	[105.6] (728)	[16.57] (114)
	No. of Specimens	3	3
350°F (177°C)	Stress Level [ksi] (MPa)	[60.4] (416)	[3.17] (21.84)
	Creep Strain, 500 hr(%)	0.0674	---
	No. of Specimens	15.7	3
	Residual Strength [ksi] (MPa)	[94.1] (648)	---
	No. of Specimens	2	0
	Stress Level [ksi] (MPa)		[1.59] (10.96)
	Creep Strain, 500 hr(%)		---
	No. of Specimens		3
	Residual Strength [ksi] (MPa)		[15.68] (108)
	No. of Specimens		2
	Stress Level [ksi] (MPa)		[1.19] (8.20)
	Creep Strain, 500 hr(%)		---
	No. of Specimens		3
	Residual Strength [ksi] (MPa)		[15.35] (106)
	No. of Specimens		3

NOTES: ¹Strain exceeded limits of gages early in test. Two specimens failed during test.
²Strain exceeded gage limit during test on one specimen.
³All three specimens failed within first ten minutes.
⁴Strain exceeded limits of gages early in test.
⁵One specimen failed on loading.
⁶Strain gages malfunctioned on two specimens.
⁷Strain gage malfunctioned on one specimen.

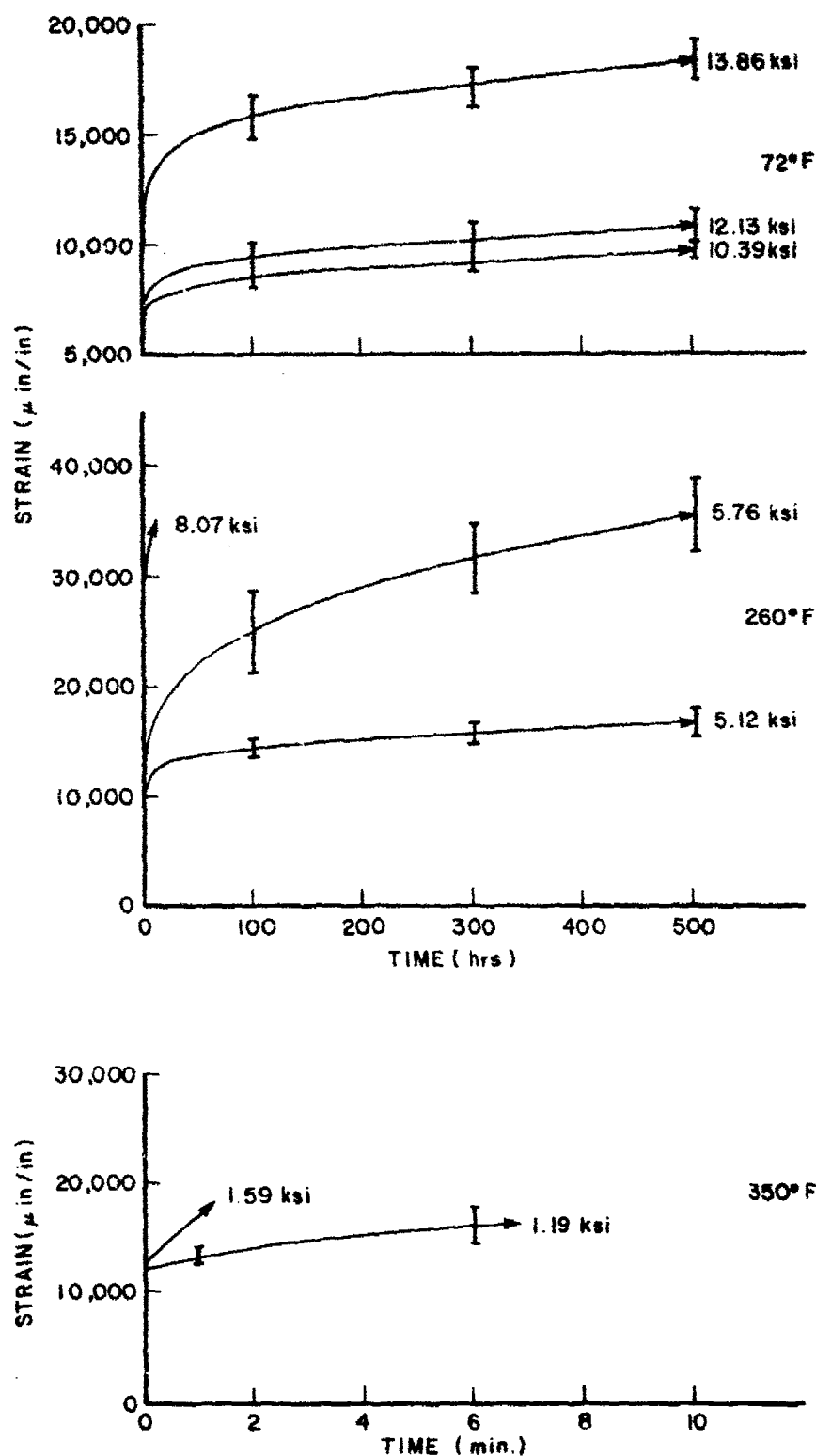


Figure 36. Tensile Creep Behavior of Bidirectional SiC/5506 Composite Laminates: $\pm 45^\circ$ Fiber Orientation.

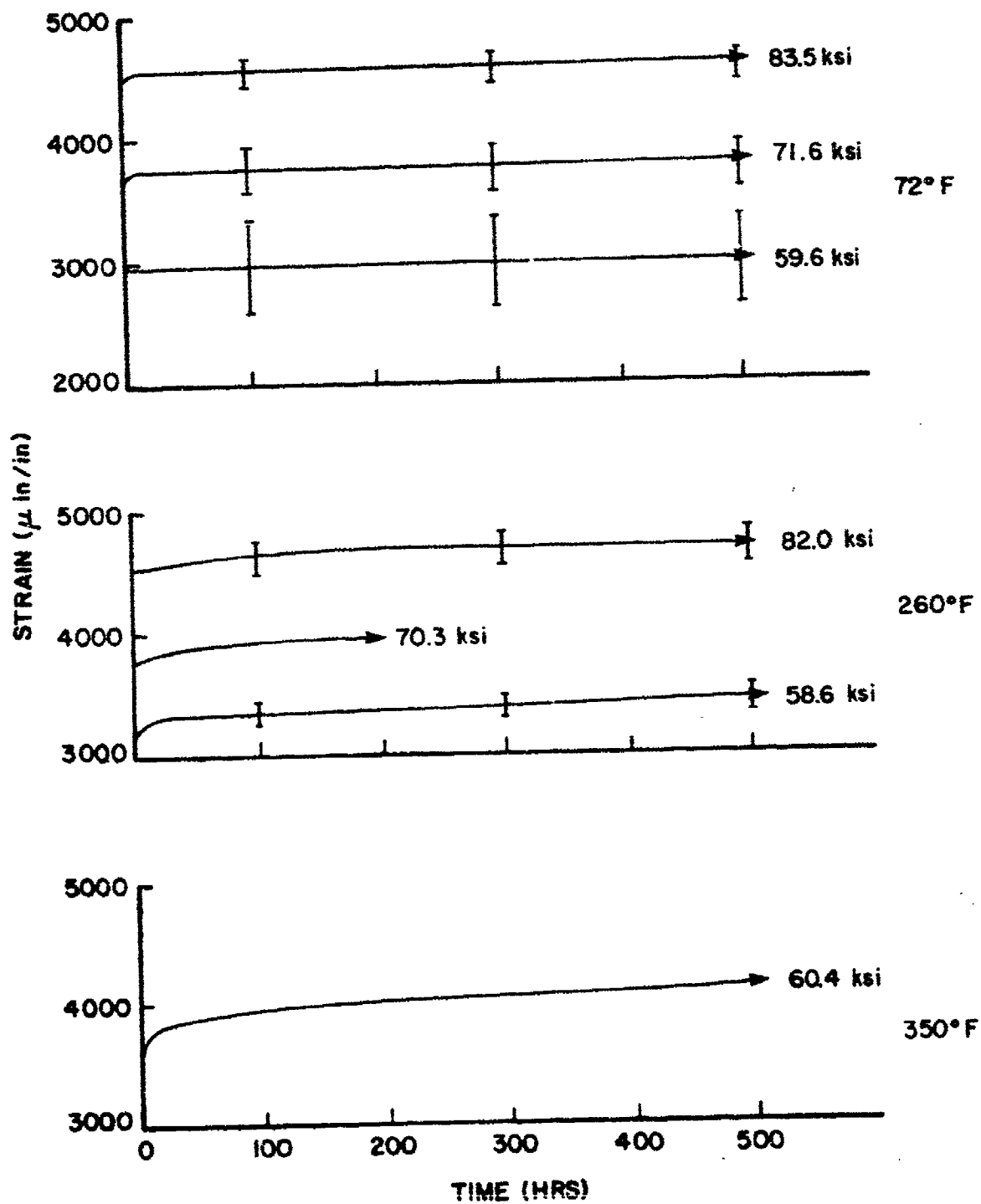


Figure 37. Tensile Creep Behavior of SiC/5506 Composite Laminates: (0,+45,-45,0,0,-45,+45,0,90,0)_s Fiber Orientation.

TABLE 30
STRESS RUPTURE PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties			
Material System - SiC/Epoxy			SiC/5506
Fiber - 5.6 mil SiC Matrix - AVCO 5506			
Maximum Temperature Rating - 350°F(177°C)			Prepreg by - AVCO
Resin Content - 19.2% by wt.			Laminate Sp. Gr. - 2.34
Fiber Content - 58.0% by vol.			Nominal Ply Thickness - 0.0065 inch
Void Content - 1.1% by vol.			No. of panels from which specimens were tested in this table - 16
Test Method - Straight-sided tension			Thickness of each type specimen:
Reference - ASTM D2290 and D3039			(0/+45/90) - 20 ply
			+45 - 8 ply
STRESS RUPTURE			
Temperature	Fiber Orientation	(0,+45,-45,0,0,-45,+45,0,90,0) _g	+45°
72°F (22°C)	Stress Level[ksi](MPa)	[83.5] (575)	[13.86] (95.50)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[105.3] (726)	[16.93] (117)
	No. of Specimens	3	3
	Stress Level[ksi](MPa)	[71.6] (493)	[12.13] (83.58)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
260°F(127°C)	Residual Strength[ksi](MPa)	[102.7] (708)	[17.24] (119)
	No. of Specimens	3	3
	Stress Level[ksi](MPa)	[82.0] (565)	[8.07] (55.6)
	Time to Failure(hrs)	500+	202 ¹
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[106.6] (734)	[17.86] (123.1)
	No. of Specimens	3	1
	Stress Level[ksi](MPa)	[70.3] (484)	[5.76] (39.7)
350°F(177°C)	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[101.4] (699)	[15.87] (109.3)
	No. of Specimens	2	3
	Stress Level[ksi](MPa)	[60.4] (416)	[3.17] (21.8)
	Time to Failure(hrs)	500+	0.08
	No. of Specimens	2	3
	Residual Strength[ksi](MPa)	[94.1] (648)	---
	No. of Specimens	2	0
	Stress Level[ksi](MPa)		[1.59] (11.0)
	Time to Failure(hrs)		346 ²
	No. of Specimens		3
	Residual Strength[ksi](MPa)		[15.68] (108.0)
	No. of Specimens		2

¹One specimen survived for 500 hrs. without failure.

²Two specimens survived for 500 hrs. without failure.

TABLE 31
FATIGUE PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties				
Material System - SiC/5506		Prepreg by - AVCO	SiC/Epoxy	
Fiber - 5.6 mil SiC Matrix - AVCO 5506		Laminate Sp. Gr. - 2.34		
Maximum Temperature Rating - 350°F(177°C)		Nominal Ply Thickness - 0.0066 inch		
Resin Content - 19.2% by wt.		No. of panels from which specimens were tested		
Fiber Content - 58.1% by vol.		in this table - 17		
Void Content - 1.0% by vol.		Thickness of each type specimen:		
Test Method - Straight-sided tension		Reference - ASTM D3039		
		+45° - 8 ply		
		0/+45/90 - 20 ply		
TENSILE FATIGUE, R=0.1				
Temperature	Fiber Orientation	+45°	0/+45/90 ⁽¹⁾	0/+45/90 ^(1,2)
72°F(22°C)	Max. Stress[ksi](MPa)	[12.12] (83.5)	[77.5] (534)	[83.3] (574)
	Lifetime (cycles)	3,534	11,644	7,237 ³
	No. of Specimens	5	5	4
	Residual Strength[ksi](MPa)	---	---	---
	No. of Specimens	0	0	0
	Max. Stress[ksi](MPa)	[9.53] (65.7)	[65.6] (452)	[75.0] (517)
	Lifetime (cycles)	94,974 ³	475,439 ³	114,479
	No. of Specimens	4	4	5
	Residual Strength[ksi](MPa)	---	---	---
	No. of Specimens	0	0	0
	Max. Stress[ksi](MPa)	[7.79] (53.7)	[59.6] (411)	[62.5] (431)
	Lifetime (cycles)	2,663,831	3,463,243	1,895,681 ³
	No. of Specimens	4	5	4
	Residual Strength[ksi](MPa)	---	---	---
	No. of Specimens	0	0	0
260°F(127°C)	Max. Stress[ksi](MPa)	[8.06] (55.5)	[70.3] (484)	
	Lifetime (cycles)	2,118	3,110	
	No. of Specimens	5	5	
	Residual Strength[ksi](MPa)	---	---	
	No. of Specimens	0	0	
	Max. Stress[ksi](MPa)	[6.34] (43.7)	[64.5] (444)	
	Lifetime (cycles)	75,744 ³	111,073 ³	
	No. of Specimens	4	4	
	Residual Strength[ksi](MPa)	---	---	
	No. of Specimens	0	0	
	Max. Stress[ksi](MPa)	[5.76] (39.7)	[58.6] (404)	
	Lifetime (cycles)	107 ³	346,552 ³	
	No. of Specimens	1	4	
	Residual Strength[ksi](MPa)	[14.6] (100)	---	
	No. of Specimens	1	0	

NOTES: 1. Stacking sequence was (0, +45, -45, 0, 0, -45, +45, 0, 90, 0)s.

2. These specimens had a 0.1935 inch (0.491 cm) hole in the center of the test section. Stresses calculated using net cross-sectional area.

3. Excludes data for one specimen from bad panel.

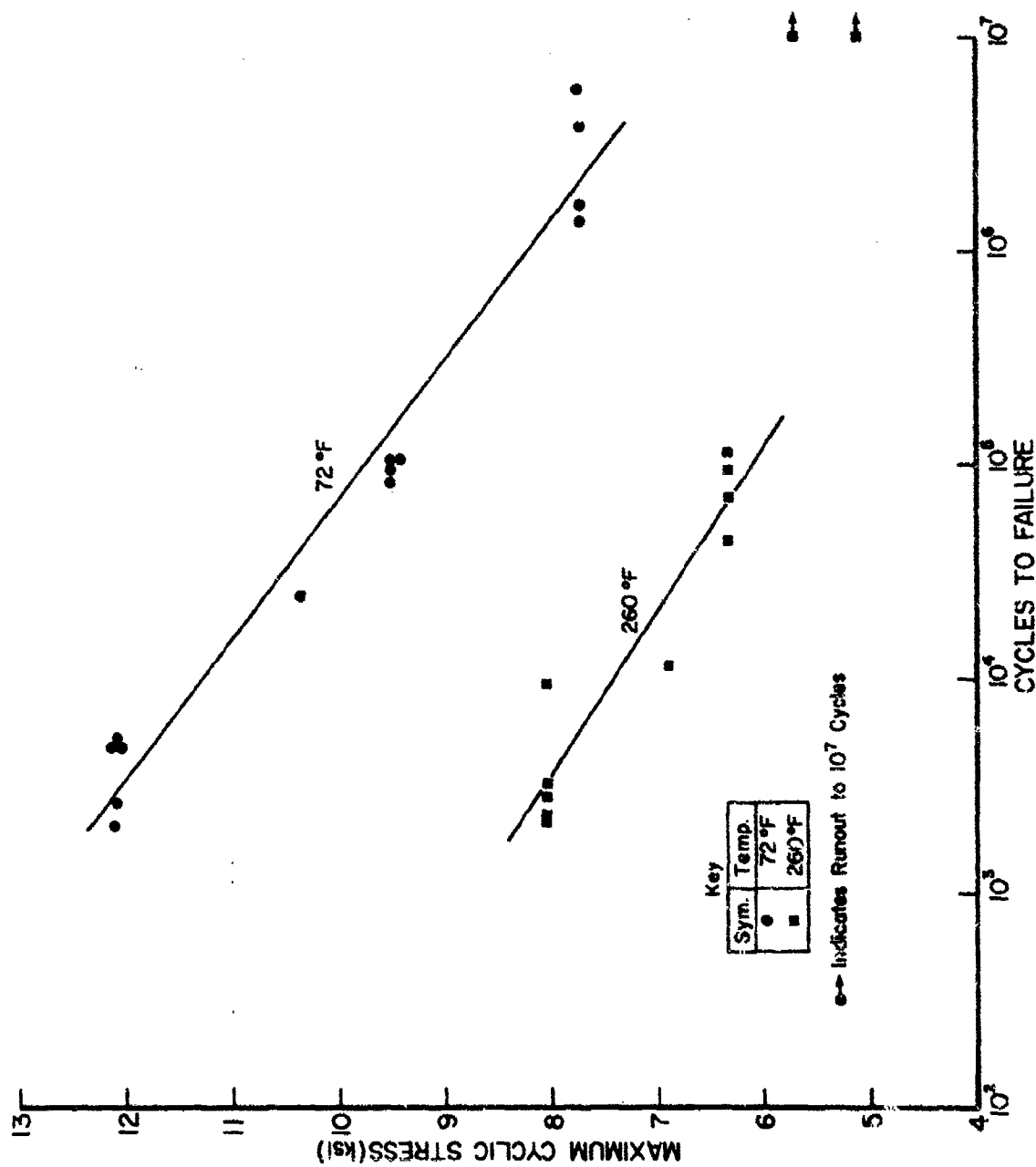


Figure 38. Tensile-Tensile Fatigue Behavior of Bidirectional SiC/5506 Composite Laminates: +45° Fiber Orientation, R = 0.10, 10 Hz.

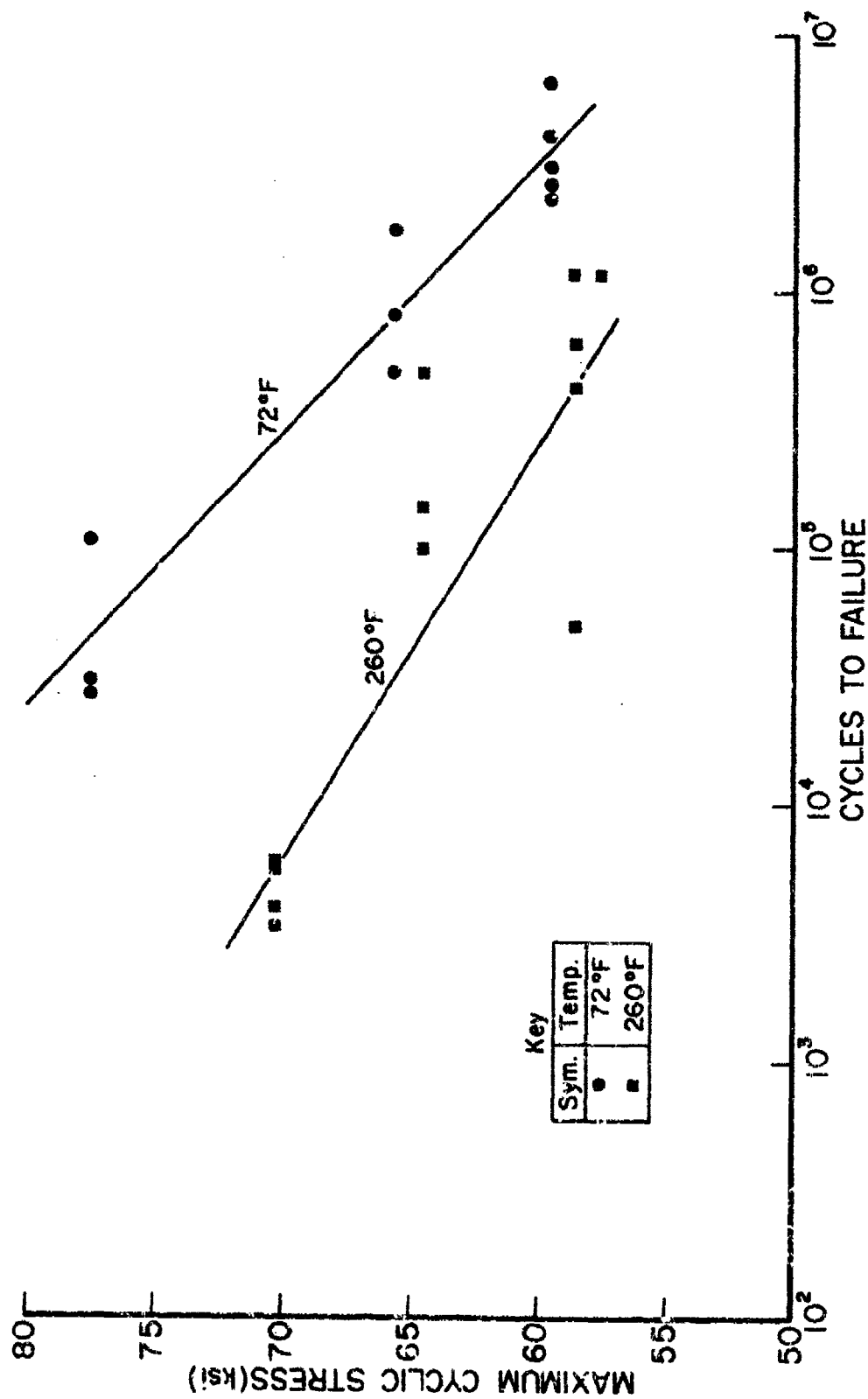


Figure 39. Tensile-Tensile Fatigue Behavior of Multidirectional SiC/5506 Composite
Laminates: (0,45,-45,0,0,-45,45,0,90,0)_s Fiber Orientation, R = 0.10, 10 Hz.

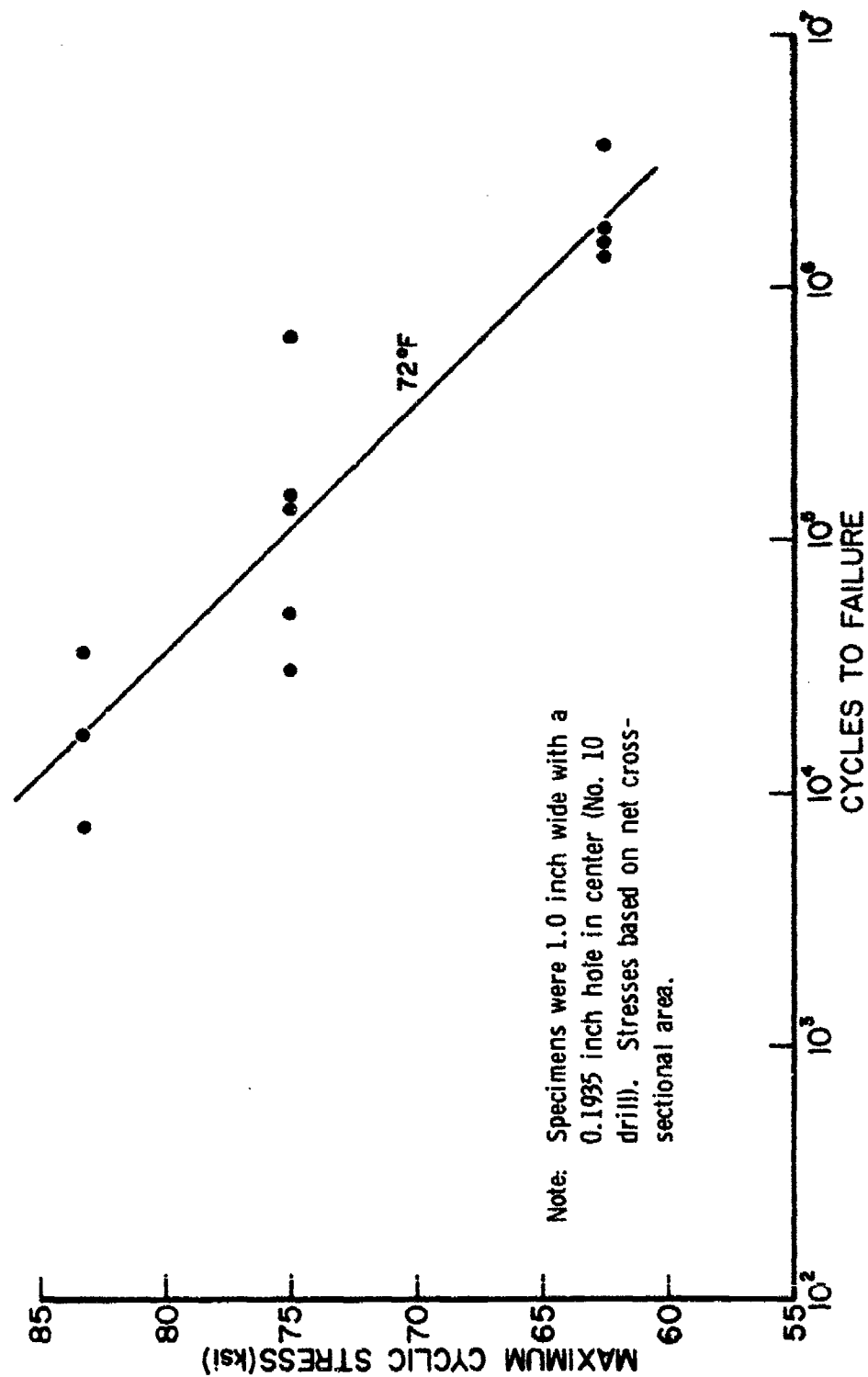


Figure 40. Tensile-Tensile Fatigue Behavior of Multidirectional SiC/5506 Composite
Laminates: (0,45,-45,0,0,-45,45,0,90,0)° Fiber Orientation, R = 0.10, 10 Hz.

TABLE 32
THERMOPHYSICAL PROPERTIES OF SiC/5506
COMPOSITE LAMINATES

Composite Material Properties					
Material System - SiC/5506		Prepreg by - AVCO		SiC/Epoxy	
Fiber - 5.6 mil SiC Matrix - AVCO 5506		Laminate Sp. Gr. - 2.35			
Maximum Temperature Rating - 350°F(177°C)		Average Ply Thickness - 0.0065 inch			
Resin Content - 19.1% by wt.		No. of panels from which specimens were tested			
Fiber Content - 58.4% by vol.		in this table - 4			
Void Content - 1.0% by vol.		Spec. Ht. - 1 ply			
Thickness of each type specimen:		Glass Trans. - 8 plies			
Therm. Exp. 0° to 90° - 40 ply		Therm. Cond. - 40 ply			
+ 45° - 8 ply					
THERMOPHYSICAL PROPERTIES: 0°					
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)	Test Method
Thermal Expansion ¹ α_x [in/in-°F] ($\mu\text{cm/cm-}^\circ\text{C}$)	[1.34] (2.41)	[1.56] (2.81)	[2.01] (3.62)	[2.23] (4.02)	TMA ²
α_y [in/in-°F] ($\mu\text{cm/cm-}^\circ\text{C}$)	[7.89] (14.2)	[9.56] (17.2)	[18.8] (33.9)	[37.8] (68.1)	
No. of Specimens per direction	3	3	3	3	
Specific Heat C_p [btu/lb.-°F] (J/kg-°C)	[0.186] (778)	[0.221] (924)	[0.279] (1170)	[0.309] (1292)	DSC ³
No. of Specimens	3	3	3	3	
Thermal Conductivity ¹ k_x [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.512] (0.885)	[0.572] (0.990)	[0.621] (1.074)	[0.615] (1.064)	Comparative
No. of Specimens	2	2	2	2	
Glass Transition Temp. Dry [°F] (°C) Wet [°F] (°C) ⁵	[394] (201) [293] (145)				DMA ⁴
THERMOPHYSICAL PROPERTIES: +45°					
Thermal Expansion ¹ α_x [in/in-°F] ($\mu\text{cm/cm-}^\circ\text{C}$)	[2.83] (5.10)	[3.33] (6.00)	[3.52] (6.33)	[4.07] (7.32)	TMA ²
No. of Specimens per direction	3	3	3	3	
Thermal Conductivity ¹ k_x [btu-ft/ft ² -hr-°F] (W/m-°C)					
No. of Specimens					

NOTES: 1. On the unidirectionally reinforced specimens, the x-direction is along the fiber axis, the y-direction is across the fiber axis, and the z-direction is through the thickness (identical to the y-direction). On +45° bidirectionally reinforced specimens, the x and y directions are identical and oriented at 45° to either fiber direction, while the z-direction is through the thickness.

2. Thermo-Mechanical Analysis.

3. Differential Scanning Calorimetry.

4. Dynamic Mechanical Analysis.

⁵ Specimen humidity aged to saturation at 160°F (71°C) and 100% R.H. prior to testing.

4.3 HyE 2034D

This graphite/epoxy system consists of a pitch-based graphite fiber (VSC-32) from Union Carbide in Fiberite's 934 epoxy resin system. The fiber has nominal tensile properties of 300 ksi (2067 MPa) strength, 75×10^6 psi (517 GPa) modulus and 0.4% elongation with a specific gravity of 2.05. It was given a finish treatment by Union Carbide to enhance its interfacial bonding to epoxy resins. The resin is a 350°F (177°C) curing epoxy system.

Tables 33 through 46 present the data generated for this graphite/epoxy system. Figures 41 through 57 illustrate the stress-strain, fatigue, and creep behavior of the material as well as the effects of humidity aging upon selected composite properties. In addition a preliminary data sheet, distributed by Fiberite, is presented at the end of the section with a few selected property values generated by various sources.

While the high modulus of the VSC-32 fiber is reflected in the composite properties, the static strength levels exhibited by this system are uniformly lower, and in most cases substantially lower, than those exhibited by the other five systems tested. This is probably due to a reduced level of interfacial fiber-to-resin bonding. The pitch based graphite reinforcing fiber in this system was given a finish treatment to enhance its bondability to the matrix resin but the treatment still does not appear to be capable of providing the level of interfacial bond strength which is achieved with the nominal 30 Msi (207 GPa) modulus PAN based graphite fibers used in the other systems (Thornel 300 or G-160).

TABLE 33
PROCESSING CONDITIONS FOR HyE2034D COMPOSITES

Composite Processing Information	
Material System - HyE 2034D	HMG/Epoxy
Fiber - VSC-32 Matrix - 934	
Maximum Rated Temperature - 350°F (177°C)	Prepreg by - Fiberite
<p style="text-align: center;">Laminate Processing Schedule</p> <p>Layup Procedure: The prepreg was stored in a closed wrapper at 0°F (-18°C). Prepreg was warmed to room temperature before removal from wrapper to prevent moisture condensation on prepreg. Plies were cut to desired size with razor knife and stacked in desired sequence (release paper removed from each ply). The stack was placed in the autoclave according to the layup system illustrated in Figure 41. The corprene edge dam serves to restrict fiber flow.</p> <p>Cure Schedule: Apply full vacuum and hold for 1/2 hour at room temperature. Heat to 250°F at a rate of 2-5°F/min. When temperature has reached 250°F apply 100 psi above bladder (while retaining vacuum). Hold at 250°F for 45 minutes then heat to 350°F at a rate of 2-5°F/min. Hold at 350°F for 2 hours then cool to 150°F at 2-5°F/min. Release pressure when temperature has reached 150°F, then release vacuum and remove panel from autoclave.</p> <p>Postcure Schedule: None.</p>	

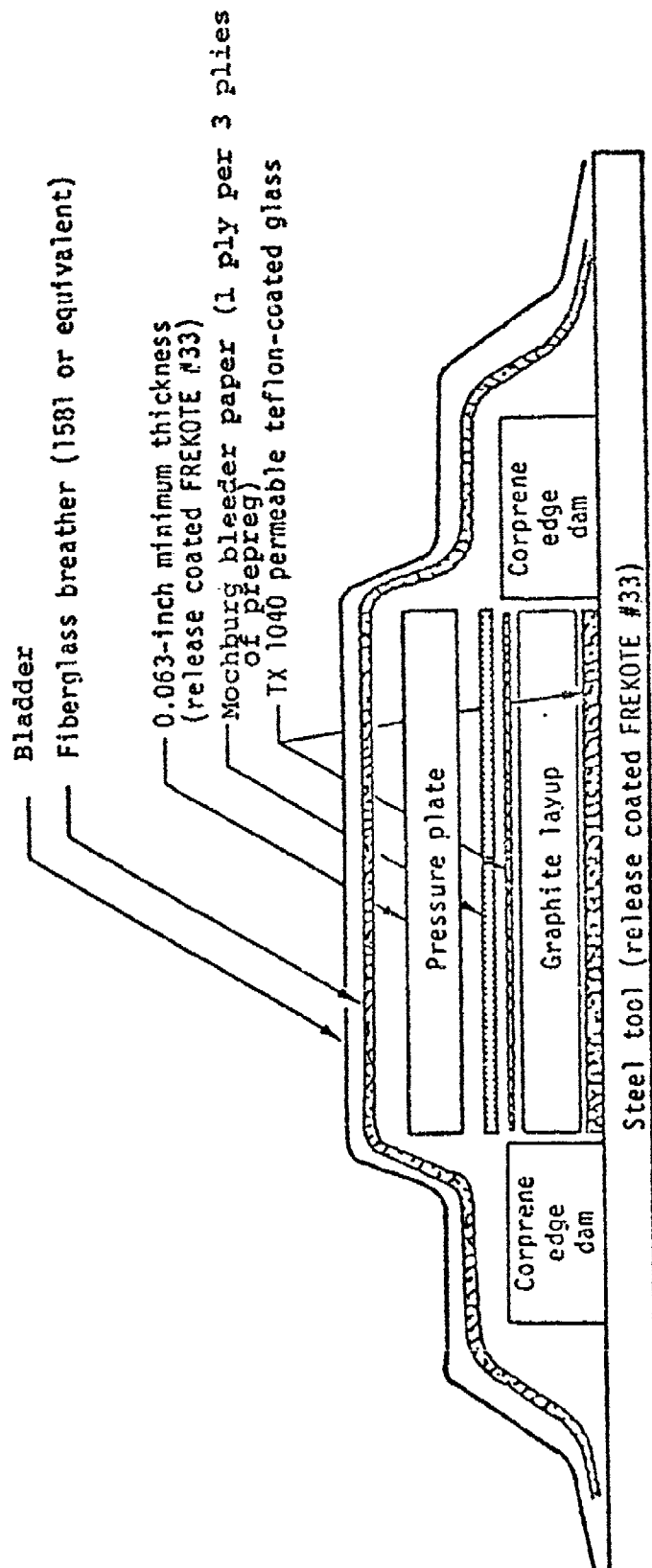


Figure 41. Layup System for HyE2034D Laminates.

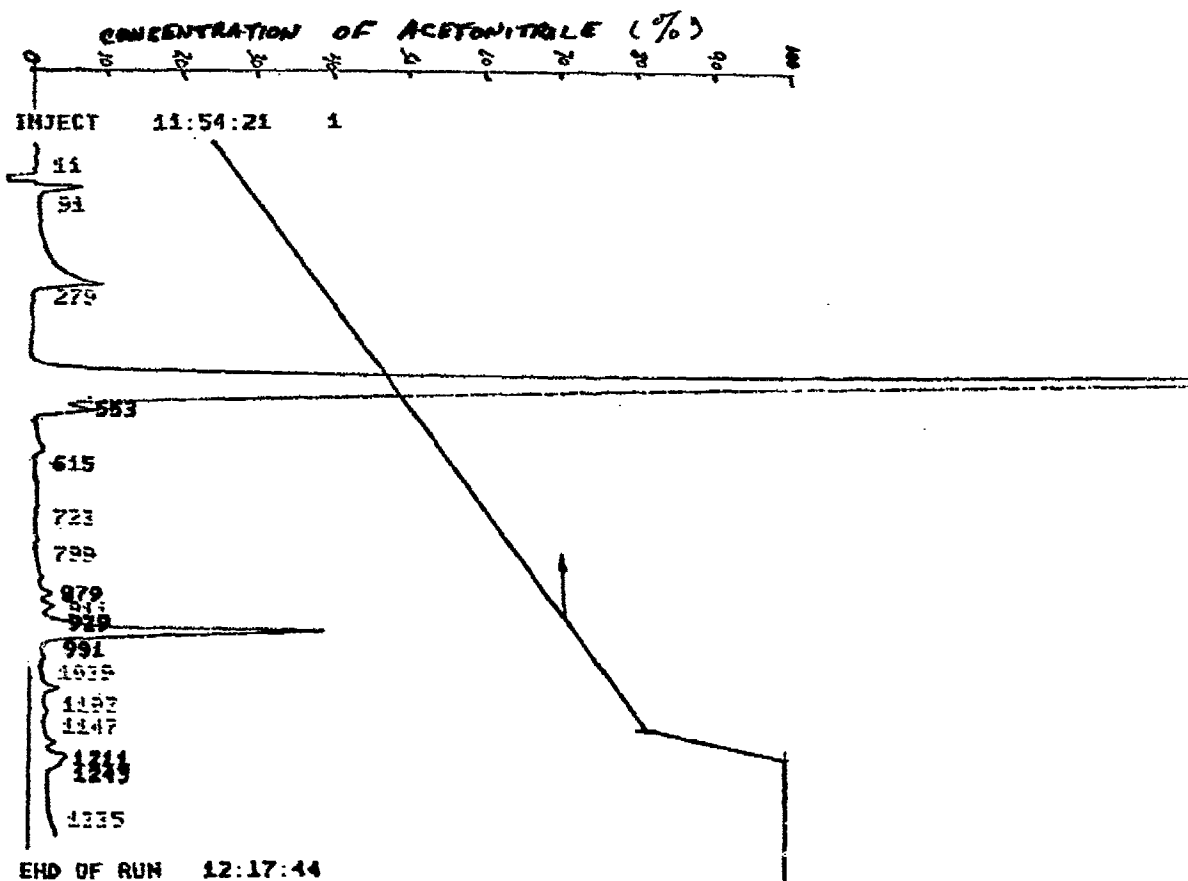
TABLE 34
PREPREG AND COMPOSITE PHYSICAL PROPERTIES

Composite Physical Property Information				
Material System - HyE 2034D			HMG/Epoxy	
Fiber - VSC-32 Matrix - 934				
Maximum Rated Temperature - 350°F(177°C)			Prepreg by - Fiberite	
Prepreg Physical Properties				
(Property)	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
Volatile Content- 0.67% by wt.	0.04%	0.62-0.69	QCI-C-V-14	Fiberite
Resin Content- 39.2% by wt.	0.9%	38.3-40.2	R15	Fiberite
Resin Flow- 22.4% by wt.	--	---	QCI-C-F-42	Fiberite
Gel Time - 12.45 min	0.20 min	12.23-12.63min	G2	Fiberite
No. of Rolls Involved - 1				
No. of Batches Involved - 1				
Laminate Physical Properties ¹				
	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
No. of Panels- 33				
Fiber Content- 68.0% by vol.	1.5%	62.9-70.1%	Acid Digestion AFML-TR-67-243 D2734 D792	ASTM ASTM
Resin Content- 24.5% by wt.	1.0%	23.0-27.0%		
Void Content- ~ 0				
Laminate Sp. Gr.- 1.80				
Fiber Sp. Gr.- 2.00		As reported by	Fiberite.	
Matrix Sp. Gr.- 1.30		As reported by	Fiberite.	
Thickness per ply- 0.0049 inch			---	---

¹ The properties reported here represent averages for all panels of this material used throughout the program.

HPLC ANALYSIS

SAMPLE (CONC.) HYE-2031D SAMPLE SIZE 1.52g/ml
MOBILE PHASE 1 Acetonitrile MOBILE PHASE 2 Water
FLOW RATE 2.0 ml/min PROGRAM Method @
COLUMN(S) ODS DETECTOR Tracor 970
ATTENUATION 32 WAVE LENGTH 230 nm
CHART SPEED 0.5 in/min FULL SCALE (mV) 20mV
DATE NOVEMBER 30 71 OPERATOR WOLFE



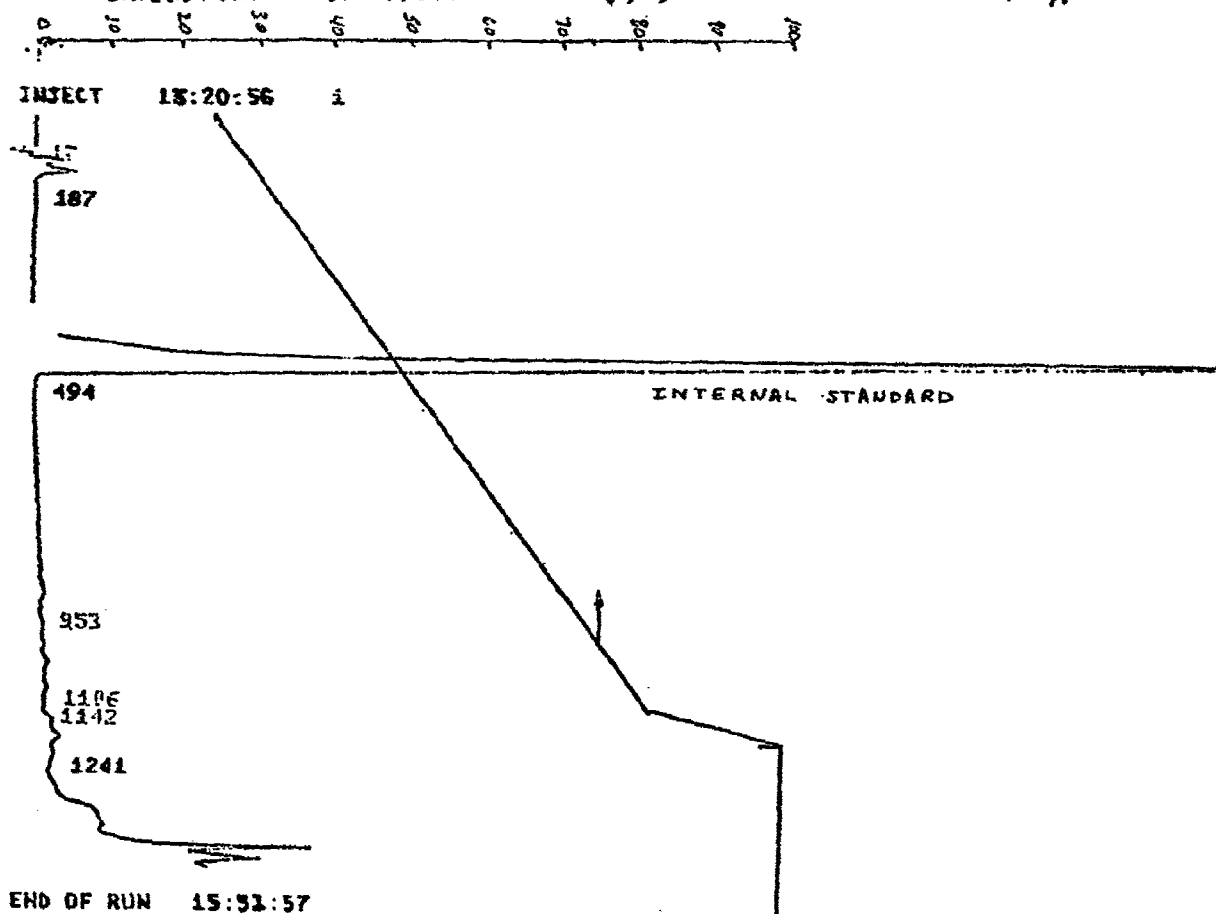
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Figure 42. HPLC Analysis of Fiberite 934 Epoxy Resin.

HPLC ANALYSIS

SAMPLE (CONC.) Benzaldehyde SAMPLE SIZE 0.2 mg/ml
MOBILE PHASE 1 Acetonitrile MOBILE PHASE 2 Water
FLOW RATE 2.0 ml/min PROGRAM Method 0
COLUMN(S) ODS DETECTOR Tracer 910
ATTENUATION 32 WAVE LENGTH 230 nm
CHART SPEED 0.5 cm/min FULL SCALE (mV) 20 mV
NOVEMBER 20 1977 OPERATOR WGLCE

TIME 0 WATER 76% ACETO. 24%
20 MIN 18% 82%
21 MIN 1% 99%
CONCENTRATION OF ACETONITRILE (%) 1%



000-25-75 15.26

Figure 43. HPLC Analysis of Benzaldehyde.

TABLE 35
TENSILE PROPERTIES OF HyE2034D COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 2034D		Prepreg by - Fibarite		IBMG/Epoxy
Filament - VSC-32 - Matrix - 934		Laminate Sp. Gr. - 1.81		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0049 inch		
Resin Content - 21.01 by wt.		No. of panels from which specimens were tested		
Fiber Content - 68.91 by vol.		in this table - 6		
Void Content - 0				
Thickness of each type specimen: 0° - 6 ply		; 90° - 15 ply		
TENSION: 0°				
	-67°F(-55°C)	72°F(22°C)	265°F(127°C)	350°F(177°C)
F_{tu} [ksi] (MPa)	[122.3] (843)	[106.5] (734)	[133.5] (920)	[135.0] (930)
Stand. Dev. [ksi] (MPa)	[29.2] (201)	[33.8] (233)	[26.7] (184)	[26.1] (180)
Range [ksi] (MPa)	[90.7-157.0]	[72.1-151.6]	[96.5-167.3]	[120.0-165.0]
No. of Specimens	5	5	5	5
F_{tpl} [ksi] (MPa)	[122.3] (843)	[106.5] (734)	[133.5] (920)	[135.0] (930)
Stand. Dev. [ksi] (MPa)	[29.2] (201)	[33.8] (233)	[26.7] (184)	[26.1] (180)
No. of Specimens	5	5	5	5
E_x [ksi] (GPa)	[55.9] (385)	[44.5] (307)	[48.4] (333)	[48.7] (336)
Stand. Dev. [ksi] (GPa)	[10.6] (73)	[3.1] (21)	[3.2] (22)	[3.8] (26)
No. of Specimens	5	5	5	5
ϵ_x [in/in] (cm/cm)	2150	2080	2780	2660
Stand. Dev.	550	570	250	520
No. of Specimens	4	5	5	5
ν_{xy}	0.30	0.22	0.32	0.30
Stand. Dev.	0.06	0.17	0.09	0.06
No. of Specimens	3	5	5	5
Test Method	Straight-sided tension			
Reference	ASTM D3039			
TENSION: 90°				
F_{tu} [ksi] (MPa)	[2.19] (15.1)	[2.07] (14.3)	[1.73] (11.9)	[1.47] (10.1)
Stand. Dev. [ksi] (MPa)	[0.52] (3.6)	[0.24] (1.7)	[0.38] (2.6)	[0.32] (2.2)
Range	[1.56-2.68]	[1.81-2.34]	[1.24-2.21]	[0.91-1.92]
No. of Specimens	5	5	5	9
F_{tpl} [ksi] (MPa)	[2.19] (15.1)	[2.07] (14.3)	[1.73] (11.9)	[0.97] (6.7)
Stand. Dev. [ksi] (MPa)	[0.52] (3.6)	[0.24] (1.7)	[0.38] (2.6)	[0.27] (1.9)
No. of Specimens	5	5	5	10
E_y [ksi] (GPa)	[0.92] (6.3)	[0.87] (6.0)	[0.79] (5.4)	[0.98] (6.8)
Stand. Dev. [ksi] (GPa)	[0.10] (0.7)	[0.03] (0.2)	[0.01] (0.07)	[0.18] (1.2)
No. of Specimens	5	5	5	10
ϵ_y [in/in] (cm/cm)	2260	2360	2220	1844
Stand. Dev.	490	297	507	436
No. of Specimens	5	5	5	9
ν_{yx}	0.005 ¹	0.004 ¹	0.005 ¹	0.006 ¹
Stand. Dev.	---	---	---	---
No. of Specimens	---	---	---	---
Test Method	Straight-sided tension			
Reference	ASTM D3039			

¹Computed using elastic moduli and longitudinal Poisson's ratio.

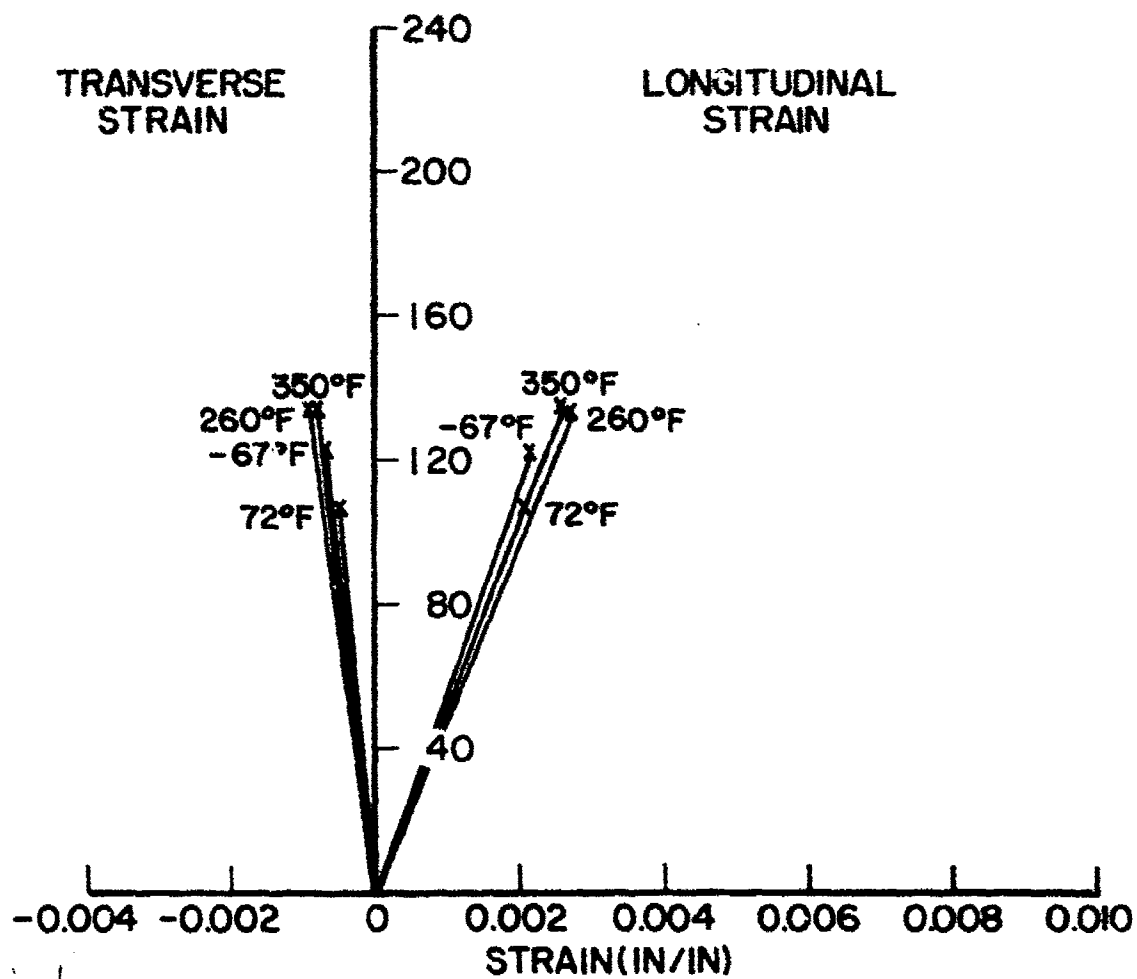


Figure 44. Tensile Stress-Strain Curves for Unidirectional HyE 2034D Composite Laminates: 0° Fiber Orientation.

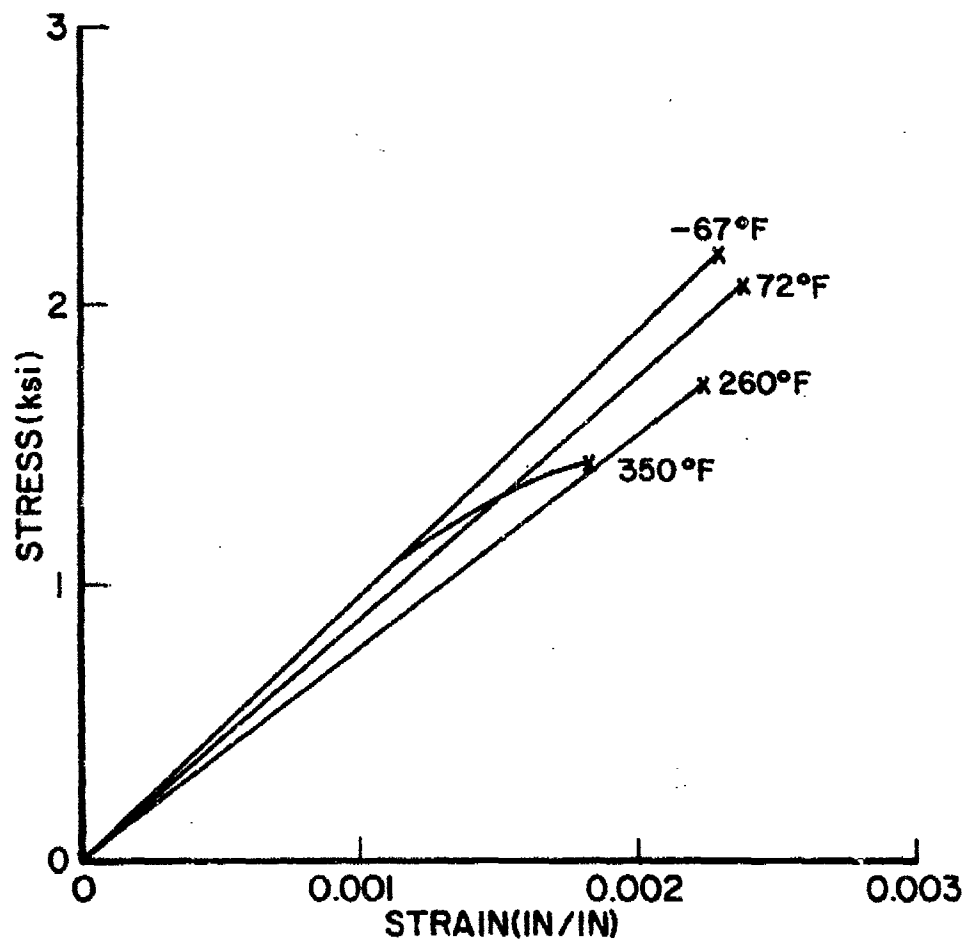


Figure 45. Tensile Stress-Strain Curves for Unidirectional HyE 2034D Composite Laminates: 90° Fiber Orientation.

TABLE 36
TENSILE PROPERTIES OF HyE2034D COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 2034D		Prepreg by - Fiberite		HMG/Epoxy
Fiber - VSC-32 Matrix - 934		Laminate Sp. Gr. - 1.80		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0051 inch		
Resin Content - 24.8% by wt.		No. of panels from which specimens were tested		
Fiber Content - 67.9% by vol.		in this table - 10		
Void Content - 20		Thickness of specimen - 8 ply		
TENSION: +45°				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
E_x^{tu} [ksi] (MPa)	[11.06] (81.7)	[10.85] (74.8)	[9.39] (64.7)	[8.76] (60.4)
Std. Dev. [ksi] (MPa)	[0.46] (3.2)	[0.35] (2.4)	[0.29] (2.0)	[0.34] (2.3)
Range [ksi] (MPa)	[11.34-12.45] (78.1-85.8)	[10.29-11.18] (70.9-77.0)	[8.95-9.75] (61.7-67.2)	[8.42-9.13] (58.0-62.9)
No. of Specimens	5	5	5	5
E_x^{tpl} [ksi] (MPa)	[4.26] (29.4)	[4.58] (31.6)	[3.50] (24.1)	[2.95] (20.3)
Std. Dev. [ksi] (MPa)	[0.38] (2.6)	[0.34] (2.3)	[1.03] (7.1)	[0.39] (2.7)
No. of Specimens	5	5	5	5
E_x^t [ksi] (GPa)	[3.50] (24.1)	[2.74] (18.9)	[2.23] (15.4)	[2.41] (16.6)
Std. Dev. [ksi] (GPa)	[0.11] (0.8)	[0.07] (0.5)	[0.51] (3.5)	[0.30] (2.1)
No. of Specimens	5	5	5	5
C_x^{tu} [in/in] (µcm/cm)	4500	5780	6390	7680
Std. Dev.	480	640	1480	950
No. of Specimens	5	5	5	5
ν_{xy}^t	0.74	0.87	0.85	0.96
Std. Dev.	0.04	0.12	0.11	0.14
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3039			

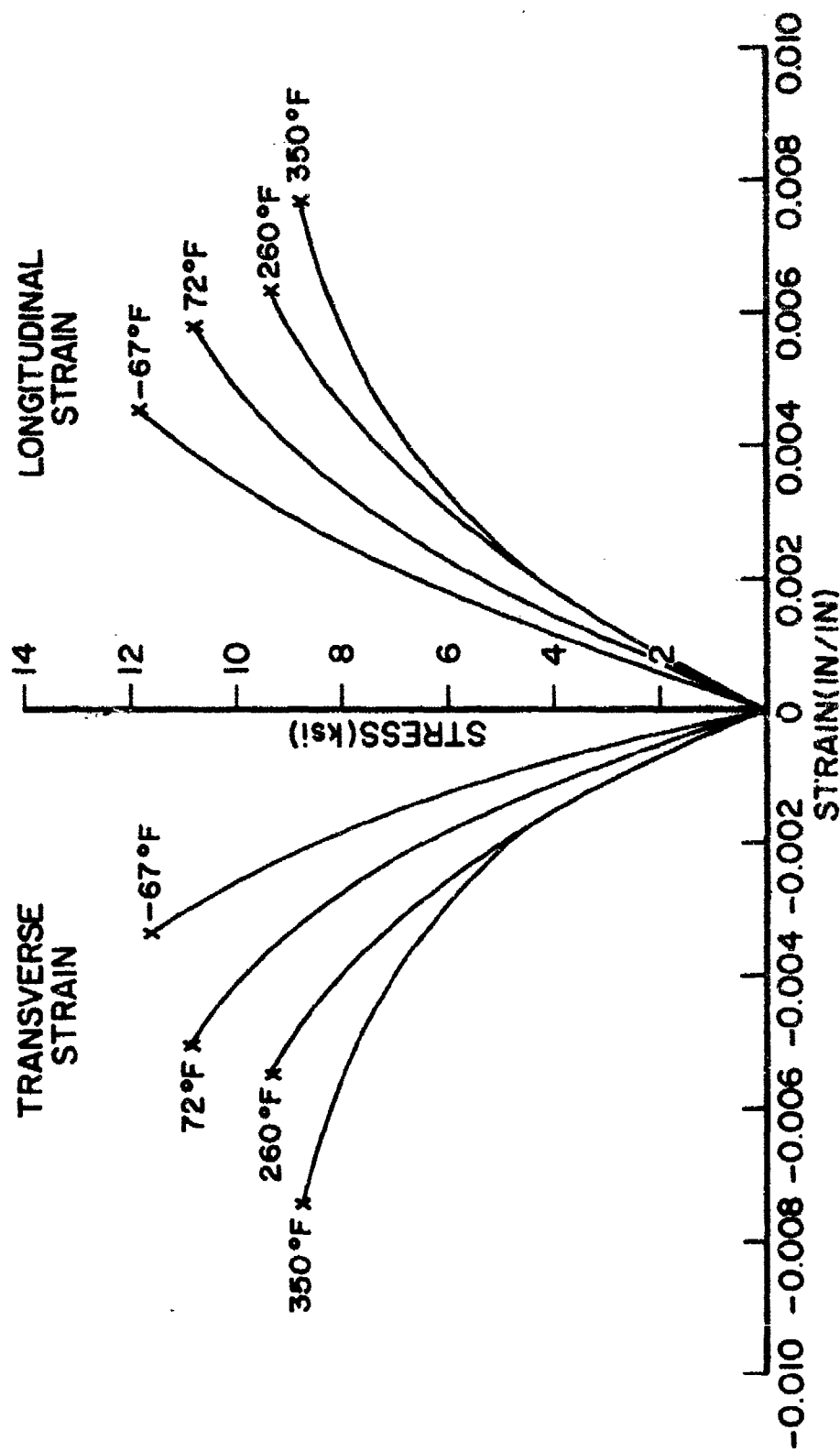


Figure 46. Tensile Stress-Strain Curves for Bidirectional HyE 2034D Composite Laminates: +45° Fiber Orientation.

TABLE 37
TENSILE PROPERTIES OF HyE2034D COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 2034D		Prepreg by - Fiberite		IMC/Epoxy
Fiber - VSC-12		Matrix - 934		
Maximum Rated Temperature - 350°F(177°C)		Laminate Sp. Gr. - 1.81		
Resin Content - 24.3% by wt.		Nominal Ply Thickness - 0.0049 inch		
Fiber Content - 67.7% by vol.		No. of panels from which specimens were tested		
Void Content - 0		in this table - 6		
Thickness of each type specimen: 20 ply				
TENSION: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0) _g				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
P_{tx} [ksi](MPa)		[75.8] (522)	[83.8] (577)	[82.8] (570)
Std.Dev. [ksi](MPa)		[8.1] (56)	[3.3] (23)	[8.7] (60)
Range [ksi](MPa)		[65.7-83.0]	[80.4-88.2]	[71.4-90.8]
No. of Specimens		(453-572)	(554-608)	(492-626)
		5	5	5
P_{tpl} [ksi](MPa)		[67.1] (462)	[83.8] (577)	[82.8] (570)
Std.Dev. [ksi](MPa)		[7.9] (54)	[3.3] (23)	[8.7] (60)
No. of Specimens		5	5	5
E_x^t [ksi](GPa)		[28.4] (196)	[26.7] (184)	[28.0] (193)
Std.Dev. [ksi](GPa)		[1.7] (12)	[1.1] (8)	[3.9] (27)
No. of Specimens		5	5	5
C_x^{tu} [µin/in](µm/cm)		2725	3100	2720
Std.Dev.		320	360	190
No. of Specimens		5	3	5
ν_{xy}^t		0.415	0.400	0.382
Std. Dev.		—	0.044	0.071
No. of Specimens		1	5	5
Test Method Reference	ASTM D3039			
TENSION: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0) _g with 0.1935 inch (0.491 cm) hole				
P_{ty} [ksi](MPa)		[64.7] (446)		
Std.Dev. [ksi](MPa)		[2.3] (16)		
Range		[61.2-67.1]		
No. of Specimens		(422-462)		
		5		
P_{tpl} [ksi](MPa)				
Std.Dev. [ksi](MPa)				
No. of Specimens				
E_y^t [ksi](GPa)				
Std.Dev. [ksi](GPa)				
No. of Specimens				
C_y^{tu} [µin/in](µm/cm)				
Std. Dev.				
No. of Specimens				
ν_{yx}^t				
Std. Dev.				
No. of Specimens				
Test Method Reference				

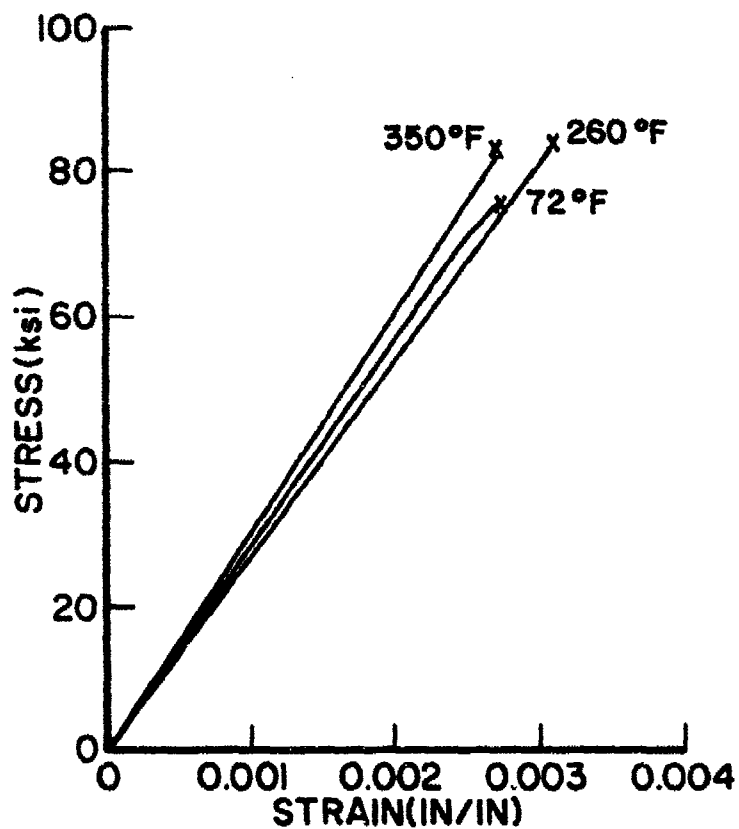


Figure 47. Tensile Stress-Strain Curves for Multidirectional HyE 2034D Composite Laminates: (0,45,-45,0,0,-45,45,0,90,0)_s Fiber Orientation.

TABLE 38
COMPRESSIVE PROPERTIES OF Hye2034D COMPOSITE LAMINATES

Composite Material Properties

Material System - Hye 2034D	Prepreg by - Fiberite	HMG/Epoxy
Fiber - VSC-32 Matrix - 934	Laminate Sp. Gr. - 1.81	
Maximum Rated Temperature - 350°F(177°C)	Nominal Ply Thickness - 0.0048 inch	
Resin Content - 23.7% by wt.	No. of panels from which specimens were tested	
Fiber Content - 69.1% by vol.	in this table - 2	
Void Content - % 0		
Thickness of each type specimen: 0° - 20 ply ; 90° - 20 ply		

COMPRESSION: 0°

	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F_x^{cu} [ksi] (MPa)	[53.81] (371)	[48.51] (334)	[42.00] (289)	[42.03] (290)
Std.Dev. [ksi] (MPa)	[5.69] (39)	[5.71] (39)	[6.63] (46)	[6.95] (48)
Range [ksi] (MPa)	[45.87 - 61.24] (316 - 422)	[41.91 - 55.56] (289 - 383)	[31.16 - 48.00] (215 - 331)	[32.21 - 48.53] (222 - 334)
No. of Specimens	5	5	5	4
F_{xpl} [ksi] (MPa)	[35.66] (246)	[25.77] (178)	[22.75] (157)	[25.27] (174)
Std.Dev. [ksi] (MPa)	[6.28] (43)	[12.81] (88)	[9.73] (67)	[8.08] (56)
No. of Specimens	5	5	5	4
E_x^C [Msi] (GPa)	[37.03] (255)	[45.90] (316)	[44.29] (305)	[43.42] (299)
Std.Dev. [Msi] (GPa)	[3.70] (25)	[10.67] (74)	[7.77] (54)	[8.42] (58)
No. of Specimens	5	5	5	5
ϵ_x^{cu} [in/in] ($\mu\text{cm/cm}$)	1740	1300	1320	1180
Std. Dev.	230	290	240	50
No. of Specimens	5	5	5	4
Test Method	ASTM D3410			
Reference				

COMPRESSION: 90°

F_y^{cu} [ksi] (MPa)	[19.08] (131)	[17.55] (121)	[13.05] (90)	[11.49] (79)
Std.Dev. [ksi] (MPa)	[2.67] (18)	[3.30] (23)	[1.13] (8)	[1.58] (11)
Range	[15.12-20.88] (104 - 144)	[15.07-22.38] (104 - 154)	[12.08-14.69] (83 - 101)	[8.75-12.50] (60 - 86)
No. of Specimens	4	4	5	5
F_{ypl} [ksi] (MPa)	[6.76] (47)	[3.17] (22)	[6.58] (45)	[2.19] (15)
Std.Dev. [ksi] (MPa)	[6.03] (41)	[2.44] (17)	[5.24] (36)	[1.39] (10)
No. of Specimens	4	4	5	5
E_y^C [Msi] (GPa)	[1.76] (12)	[1.62] (11)	[1.14] (8)	[0.92] (6)
Std.Dev. [Msi] (GPa)	[0.78] (5)	[0.24] (2)	[0.26] (2)	[0.12] (1)
No. of Specimens	4	4	5	5
ϵ_y^{cu} [in/in] ($\mu\text{cm/cm}$)	19,980	35,950	13,880	25,040
Std. Dev.	1,540	12,220	3,970	5,250
No. of Specimens	4	4	5	5
Test Method	ASTM D3410			
Reference				

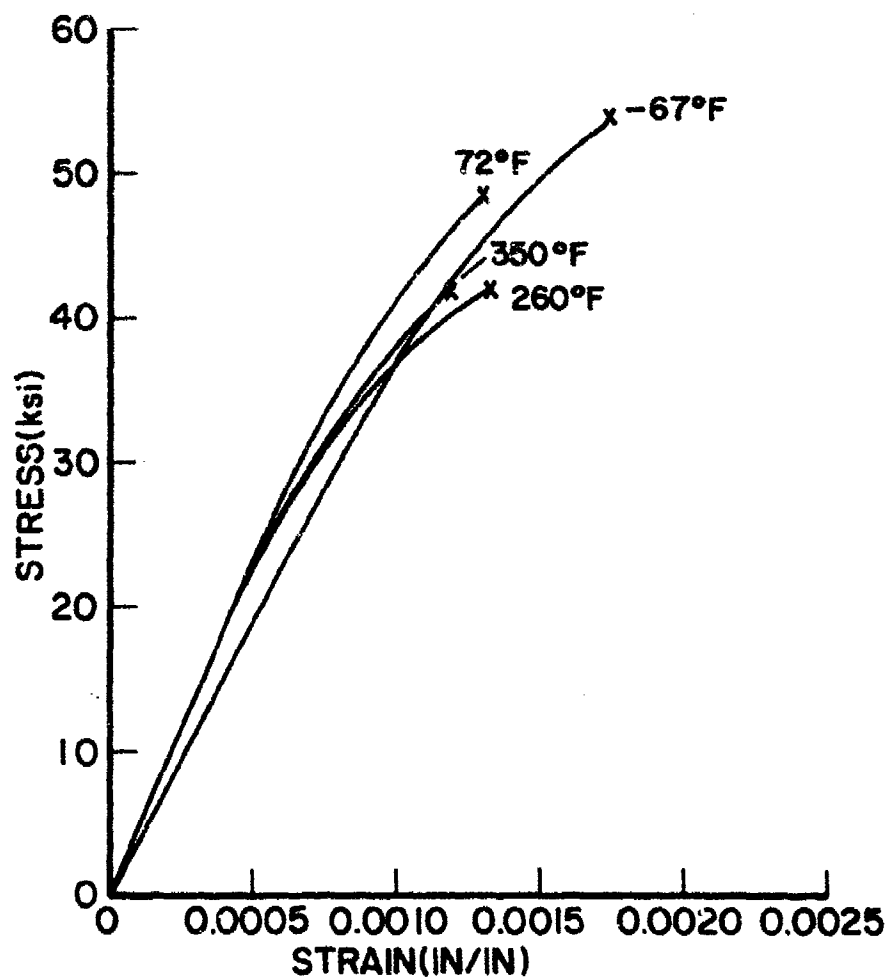


Figure 48 Compressive Stress-Strain Curves for Unidirectional HyE 2034D Composite Laminates: 0° Fiber Orientation.

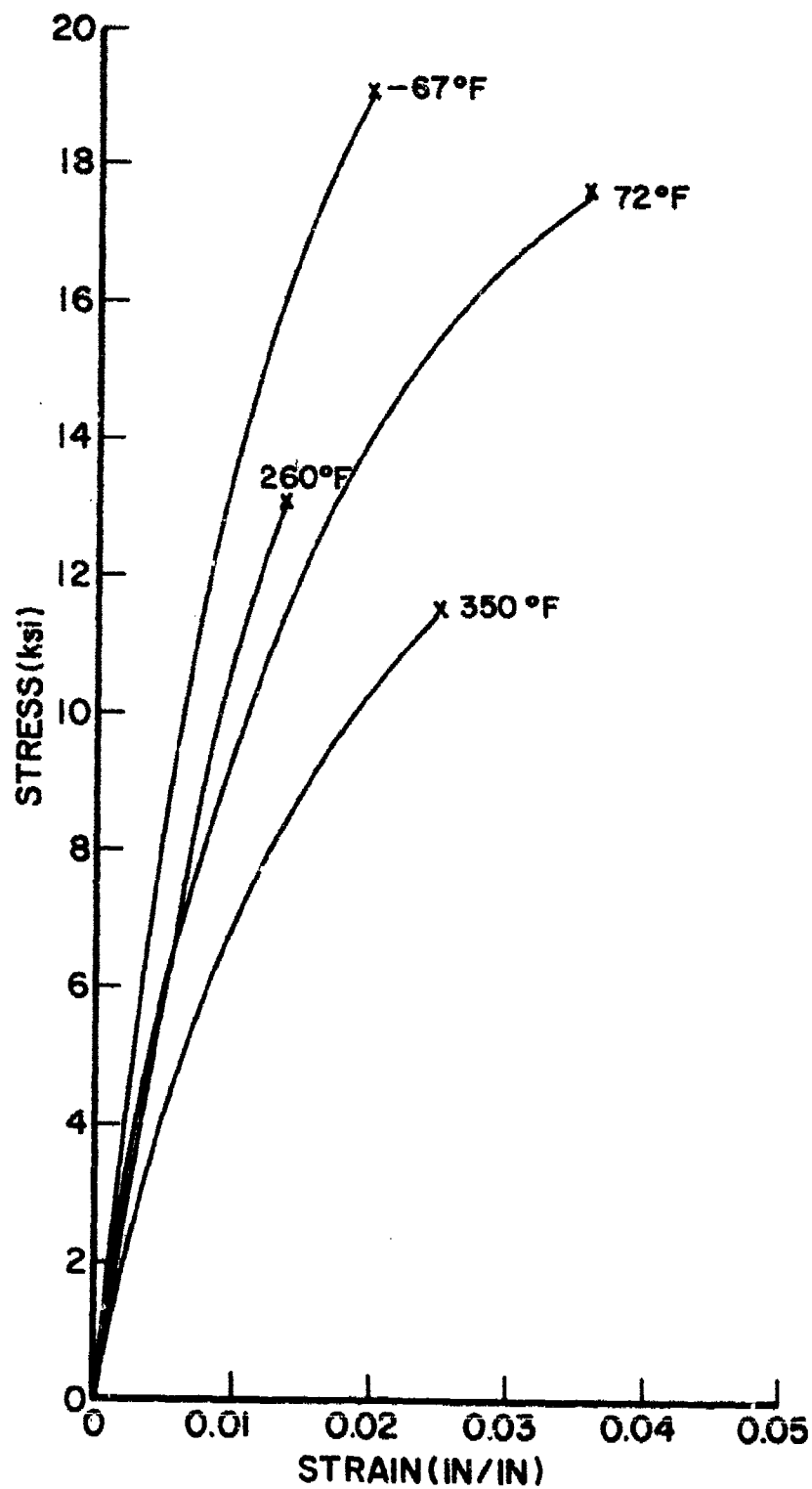


Figure 49. Compressive Stress-Strain Curves for Unidirectional HyE 2034D Composite Laminates: 90° Fiber Orientation.

TABLE 39
FLEXURAL PROPERTIES OF HyE2034D COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 2034D		Prepreg by - Fiberite		HMG/Epoxy
Fiber - VSC-32 Matrix - 934		Laminate Sp. Gr. - 1.82		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0049 inch		
Resin Content - 23.4% by wt.		No. of panels from which specimens were tested		
Fiber Content - 69.8% by vol.		in this table - 1		
Void Content - ~0				
Thickness of each type specimen: 0° - 14 ply ; 90° - 14 ply				
FLEXURE: 0°				
	-67°F(-55°C)	72°F(22°C)	260°F (127°C)	350°F (177°C)
F_x^{fu} [ksi] (MPa)	[86.9] (599)	[90.2] (621)	[66.6] (459)	[66.9] (461)
Std.Dev. [ksi] (MPa)	[17.1] (118)	[1.9] (13.1)	[2.5] (17.2)	[3.0] (21.0)
Range [ksi] (MPa)	[62.2-107.1] (429-738)	[87.4-91.9] (602-633)	[62.8-69.0] (433-475)	[63.3-70.0] (436-482)
No. of Specimens	5	5	5	5
E_x^f [Msi] (GPa)	[35.3] (243)	[41.6] (287)	[37.5] (258)	[40.3] (278)
Std.Dev. [Msi] (GPa)	[10.9] (75)	[1.6] (11.0)	[9.5] (65.5)	[3.0] (21.0)
No. of Specimens	5	5	5	5
Test Method	4 pt. flexure			
Reference	Design Guide, Jan. 1971 } Corresponds to ASTM D790 except for loading points and loading speed.			
FLEXURE: 90°				
P_y^{fu} [ksi] (MPa)	[5.57] (38.4)	[5.30] (36.5)	[3.67] (25.3)	[2.80] (19.3)
Std.Dev. [ksi] (MPa)	[0.19] (1.3)	[0.37] (2.54)	[0.17] (1.17)	[0.27] (1.5)
Range [ksi] (MPa)	[5.28-5.75] (36.4-39.6)	[4.80-5.72] (33.1-39.4)	[3.38-3.78] (23.3-26.0)	[2.51-3.20] (17.3-22.0)
No. of Specimens	5	5	5	5
E_y^f [Msi] (GPa)	[1.07] (7.4)	[1.09] (7.5)	[0.90] (6.2)	[0.77] (5.3)
Std.Dev. [Msi] (GPa)	[0.04] (0.3)	[0.06] (0.4)	[0.04] (0.3)	[0.02] (1.5)
No. of Specimens	5	5	5	5
Test Method	4 pt. flexure			
Reference	Design Guide, Jan. 1971 } Corresponds to ASTM D790 except for loading points and loading speed.			

TABLE 40
SHEAR PROPERTIES OF HyE2034D COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyK 2034D		Prepreg by - Fibertite		IM6/Epoxxy
Fiber - VSC-32 Matrix - 934		Laminate Sp. Gr. - 1.81		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0040 inch		
Resin Content - 24.9% by wt.		No. of panels from which specimens were tested in this table - 11		
Fiber Content - 67.9% by vol.				
Void Content - 0				
Thickness of each type specimen - Inplane - 8 ply ; Interlaminar - 15 ply				
INPLANE SHEAR				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
τ_{xy}^{su} [ksi] (MPa)	[5.93] (40.9)	[5.43] (37.4)	[4.69] (32.3)	[4.38] (30.2)
Std.Dev. [ksi] (MPa)	[0.23] (1.6)	[0.17] (1.2)	[0.14] (1.0)	[0.17] (1.2)
Range [ksi] (MPa)	[5.67-6.22] (39.1-42.9)	[5.14-5.59] (35.4-38.5)	[4.48-4.88] (30.9-33.6)	[4.20-4.50] (29.0-31.4)
No. of Specimens	5	5	5	5
G_{xy}^s [ksi] (GPa)	[1.07] (7.4)	[0.73] (5.0)	[0.66] (4.5)	[0.60] (4.2)
Std.Dev. [ksi] (GPa)	[0.14] (1.0)	[0.06] (0.4)	[0.02] (0.1)	[0.04] (0.3)
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D358			
INTERLAMINAR SHEAR				
τ_{12}^{isu} [ksi] (MPa)	[8.09] (55.7)	[7.18] (49.5)	[6.48] (44.6)	[5.83] (40.2)
Std.Dev. [ksi] (MPa)	[0.59] (4.1)	[0.46] (3.2)	[0.48] (3.3)	[0.26] (1.8)
Range	[7.51-9.06] (51.7-62.4)	[6.45-7.85] (44.4-54.1)	[6.04-7.12] (41.6-49.1)	[5.48-6.17] (37.7-42.5)
No. of Specimens	5	10	5	5
Test Method Reference	Short Beam Shear 4:1 Advanced Composite Design Guide - Jan., 1971			

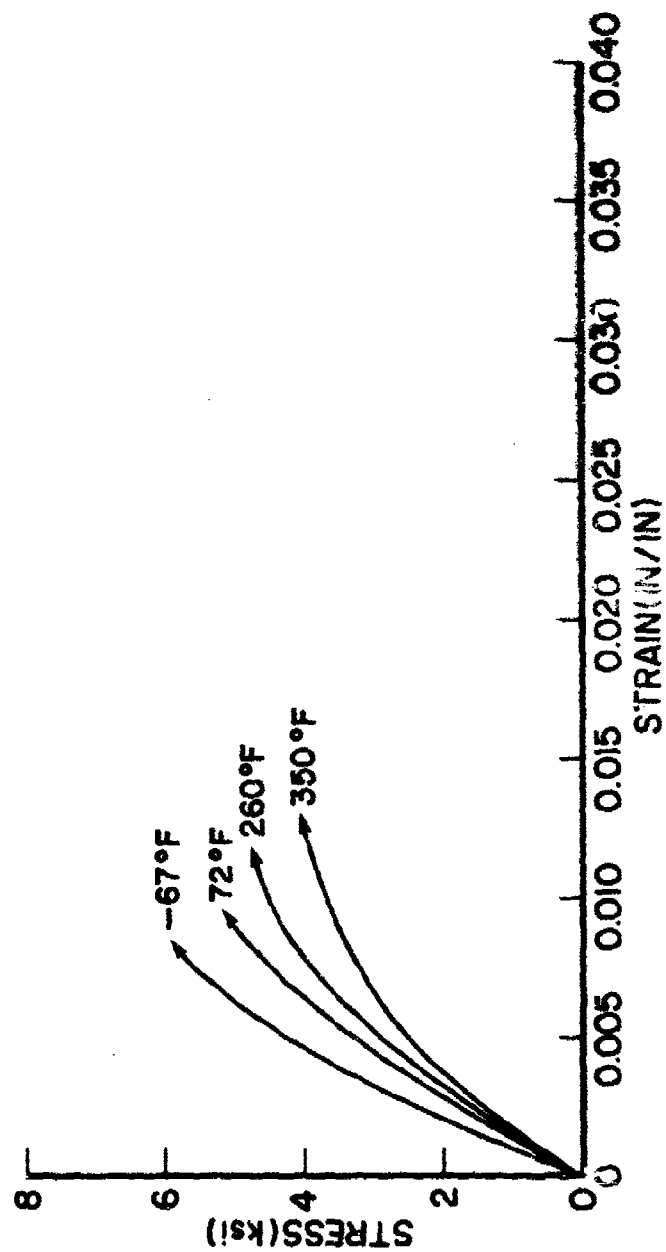


Figure 50. Inplane Shear Stress-Strain Curves for HYE 2034D Composite Laminates.

TABLE 41

TENSILE, COMPRESSIVE, AND SHEAR PROPERTIES OF HYE 2034D
COMPOSITE LAMINATES AFTER HUMIDITY AGING

Composite Material Properties									
Material System - HyE 2034D Fiber - VSC-32 Matrix - 934 Maximum Rated Temperature - 350°F Resin Content - 24.3% by wt. Fiber Content - 68.5% by vol. Void Content - ~ 0 Thickness of each type specimen: Tension - 15 ply; Compr. - 20 ply; Shear - 15 ply				Prepreg by - Fiberite Laminate Sp. Gr. - 1.80 Nominal Ply Thickness - 0.0048 inch No. of panels from which specimens were tested in this table - 9 Aging Conditions - 160°F & 95-100% R.H. Tension - 15 ply; Compr. - 20 ply; Shear - 15 ply		RMC/Epoxy		COMPRESSION: 90°	
TENSION: 90°		72°F (22°C)		260°F (127°C)		72°F (22°C)		260°F (127°C)	
Exposure Time (hrs)	217	0.79	1.1a1	982	982	145	1706	2183	2183
Wt. Gain (% of orig. dry wt.)	0.01	0.01	0.03	0.03	0.03	0.74	1.33 ¹	1.39 ¹	1.39 ¹
Std. Dev. (%)	5	5	5	5	5	0.03	0.03	0.12	0.12
No. of Specimens	5	5	5	5	5	5	5	5	5
F _{cu} [ksi] (MPa)	[2.53] (17.4)	[1.72] (11.9)	[2.05] (14.1)	[1.04] (7.2)	[1.04] (7.2)	[14.12] (97.3)	[13.39] (92.3)	[15.19] (104.3)	[10.04] (111)
Std. Dev. [ksi] (MPa)	[0.34] (2.3)	[0.17] (1.2)	[0.29] (2.0)	[0.13] (0.9)	[0.13] (0.9)	[2.56] (17.6)	[1.58] (10.9)	[2.38] (16.4)	[2.88] (20)
Range	[2.13-2.85]	[1.44-1.89]	[1.65-2.38]	[0.88-1.21]	[0.88-1.21]	[12.00-17.59]	[11.26-15.62]	[13.51-19.34]	[13.13-18.63]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.98] (6.7)	[0.80] (5.5)	[1.49] (10.3)	[0.89] (6.1)	[0.89] (6.1)	[2.83] (19.5)	[2.49] (17.2)	[3.58] (24.4)	[2.82] (19.4)
Std. Dev. [ksi] (MPa)	[0.20] (1.4)	[0.16] (1.1)	[0.29] (2.0)	[0.09] (0.6)	[0.09] (0.6)	[0.75] (5.2)	[0.27] (1.9)	[1.35] (9.3)	[0.86] (5.9)
No. of Specimens	5	5	5	5	5	4	4	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[1.92] (13.2)	[1.38] (9.5)	[1.05] (7.2)	[1.07] (7.4)
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[0.79] (5.4)	[0.38] (2.6)	[0.13] (0.9)	[0.17] (1.2)
No. of Specimens	5	5	5	5	5	4	5	5	5
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	[19.280]
Std. Dev. [ksi] (MPa)	[0.03] (0.2)	[0.04] (0.3)	[0.05] (0.3)	[0.09] (0.6)	[0.09] (0.6)	[7.360]	[4.600]	[2.620]	[5.140]
No. of Specimens	5	5	5	5	5	4	5	5	4
F _{cu} [ksi] (MPa)	[0.95] (6.5)	[0.71] (4.9)	[1.00] (6.9)	[0.52] (3.6)	[0.52] (3.6)	[20.480]	[18.490]	[15.180]	

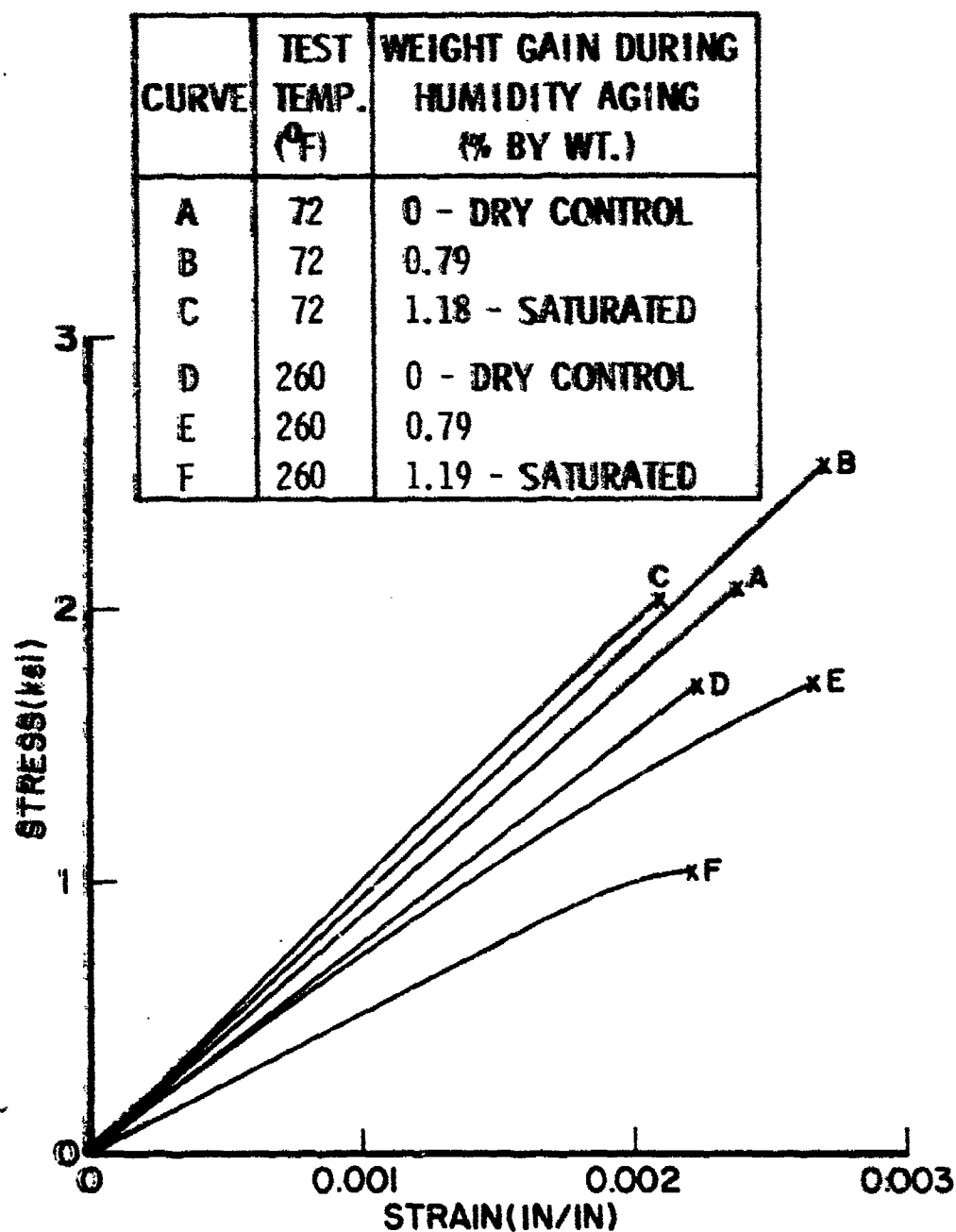


Figure 51 . Tensile Stress-Strain Curves for Unidirectional HyE 2034D Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

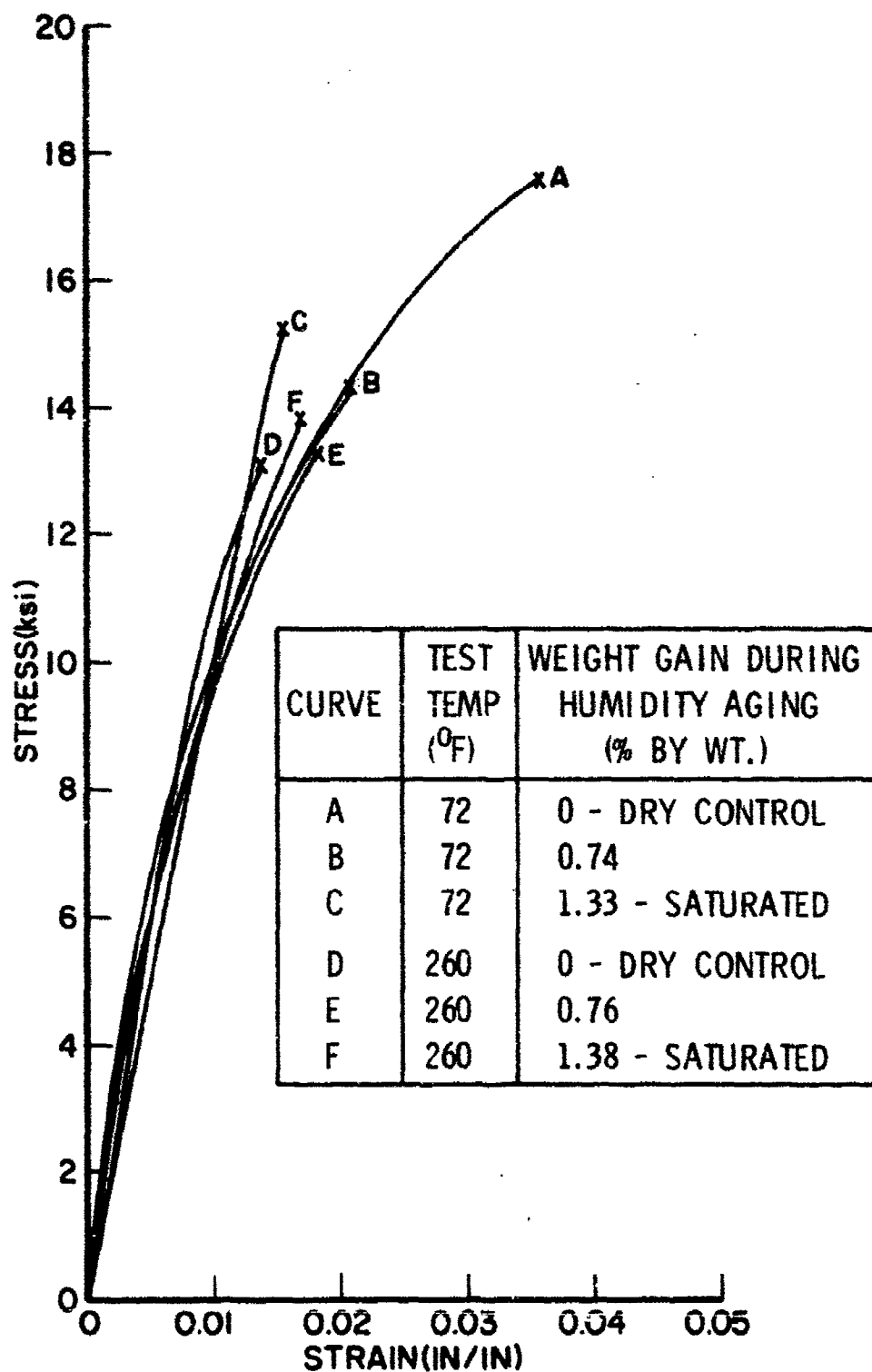


Figure 52. Compressive Stress-Strain Curves for Unidirectional HyE 2034D Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

TABLE 42
TENSILE CREEP PROPERTIES OF Hye2034D
COMPOSITE LAMINATES

Composite Material Properties			
Material System - HYE 2034D Fiber - VSC-32 Matrix - 934 Maximum Temperature Rating - 350°F (177°C) Resin Content - 23.8% by wt. Fiber Content - 67.9% by vol. Void Content - ± 0		Prepared by - Fibrexite Laminator Sp. Gr. - 1.80 Nominal Ply Thickness - 0.0050 inch No. of panels from which specimens were tested in this table - 18 Thickness of each type specimen: (0/+45/90) - 20 ply ±45° - 8 ply	
Test Method - Straight-sided tension Reference - ASTM D2290 and D3039		HMG/Epoxy	
CREEP			
Temperature		(0,+45,-45,0,0,-45,+45,0,90,0)°	±45°
72°F (22°C)	Stress Level [ksi] (MPa)	[60.7] (418)	[8.68] (59.8)
	Creep Strain, 500 hr(%)	0.0038 @ 191 hrs ³	0.1182
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[76.8] (529)	[11.24] (77.4)
	No. of Specimens	3	3
	Stress Level [ksi] (MPa)	[53.1] (366)	[7.30] (50.3)
	Creep Strain, 500 hr(%)	0.0071	0.0998
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[75.5] (520)	[11.30] (77.9)
	No. of Specimens	2	3
	Stress Level [ksi] (MPa)	[45.5] (313)	[5.43] (37.4)
	Creep Strain, 500 hr(%)	40	0.0605
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[77.4] (533)	[11.33] (78.1)
	No. of Specimens	3	3
260°F (127°C)	Stress Level [ksi] (MPa)	[60.0] (413)	[6.57] (45.3)
	Creep Strain, 500 hr(%)	0.0036 @ 7 hrs ¹	0.2981 @ 135 hrs ¹
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	---	[11.12] (76.6)
	No. of Specimens	0	2
	Stress Level [ksi] (MPa)	[50.0] (345)	[5.63] (38.8)
	Creep Strain, 500 hr(%)	-0.0088 ⁴	0.2154
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[77.0] (531)	[11.07] (82.5)
	No. of Specimens	3	3
	Stress Level [ksi] (MPa)	[40.0] (276)	[4.70] (32.4)
	Creep Strain, 500 hr(%)	-0.0036 ⁴	0.1419
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[80.4] (554)	[12.77] (89.0)
	No. of Specimens	3	3
350°F (177°C)	Stress Level [ksi] (MPa)	[66.2] (456)	[5.25] (36.2)
	Creep Strain, 500 hr(%)	0.0148 @ 342 hrs	0.3661 @ 1 hr. ¹
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[82.6] (569)	---
	No. of Specimens	2	0 ²
	Stress Level [ksi] (MPa)	[58.0] (400)	[4.38] (30.2)
	Creep Strain, 500 hr(%)	-0.0034 ⁴	0.8708 @ 95 hrs. ¹
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[76.7] (528)	[7.33] (50.5)
	No. of Specimens	3	3
	Stress Level [ksi] (MPa)	[49.4] (340)	[3.50] (24.1)
	Creep Strain, 500 hr(%)	-0.0020 ⁴	1.0004 @ 24 hrs. ¹
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[78.6] (542)	[5.51] (38.0)
	No. of Specimens	3	3

¹Strain exceeded gage limits during test.

²Three specimens failed during test.

³Cracking tabs debonded from one specimen at 226 hrs. Specimens were retested without strain measurement and ran out to 500 hrs without failure.

⁴Specimen contractions noted at lower stress levels at both 260°F (127°C) and 350°F (177°C). May be due to relaxation of residual curing stresses.

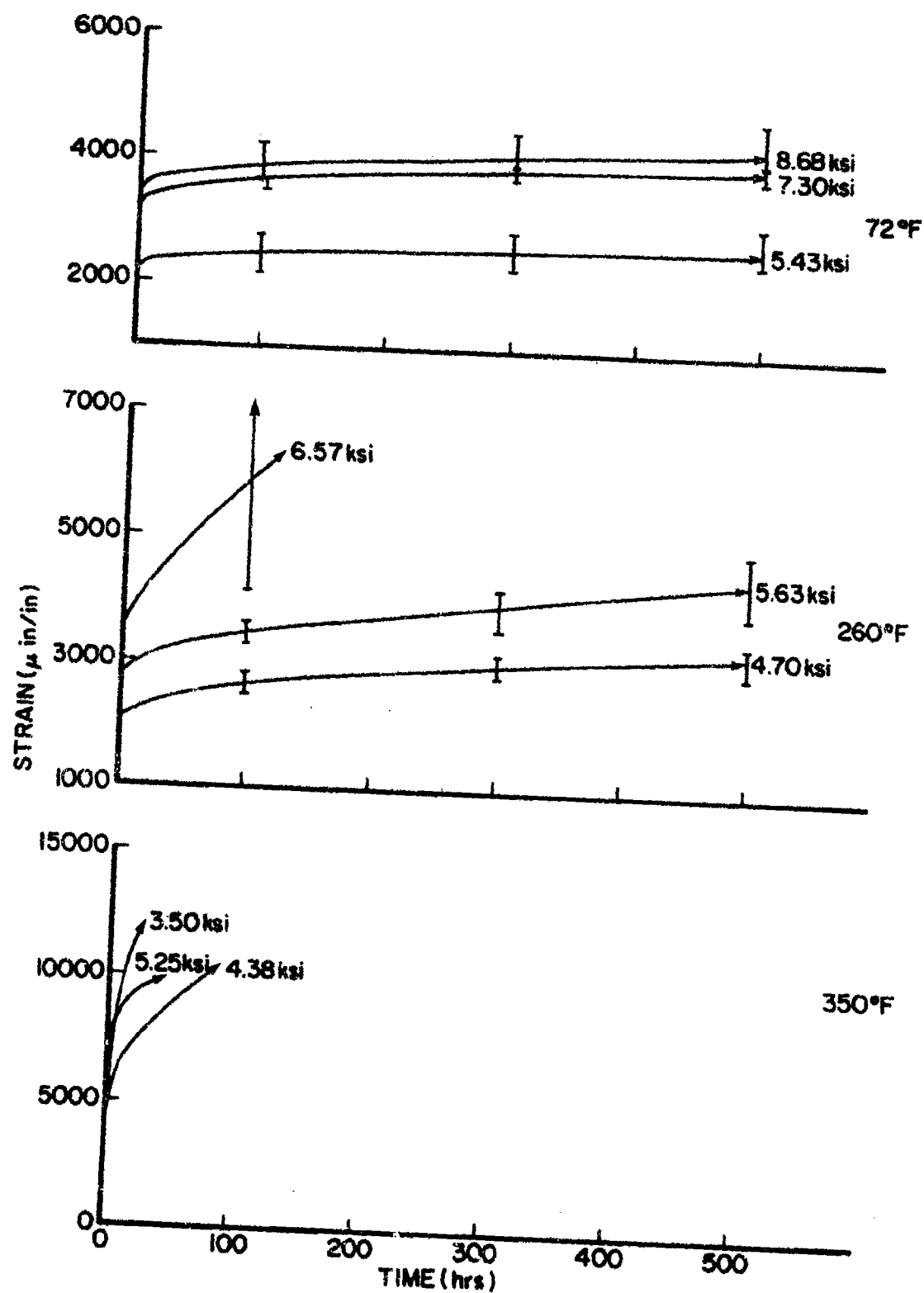


Figure 53. Tensile Creep Behavior of Bidirectional HyE2034D Composite Laminates: $\pm 45^\circ$ Fiber Orientation.

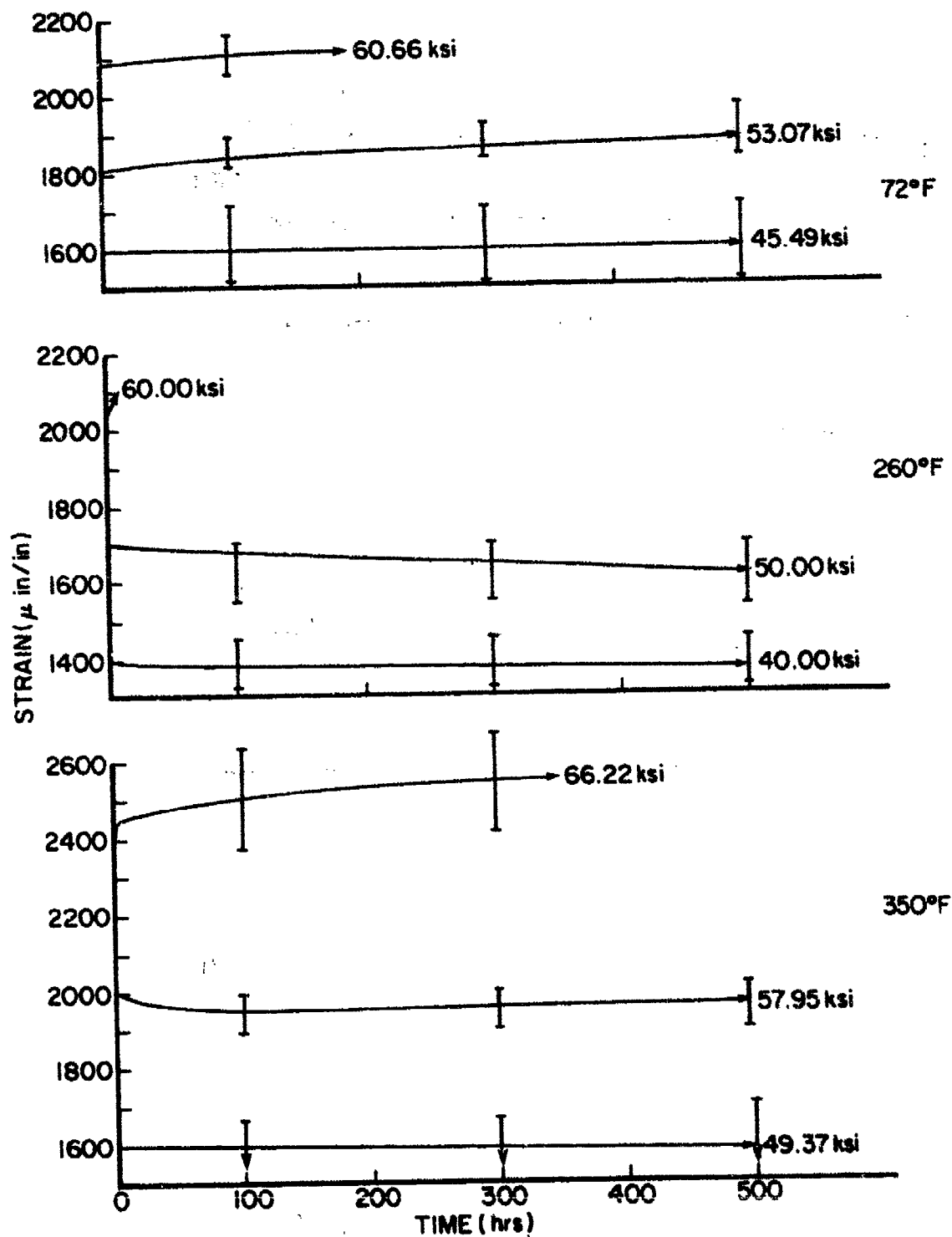


Figure 54. Tensile Creep Behavior of HyE2034D Composite Laminates: $(0,+45,-45,0,0,-45,+45,0,90,0)_s$ Fiber Orientation.

TABLE 43
TENSILE STRESS-RUPTURE PROPERTIES OF HyE2034D
COMPOSITE LAMINATES

Composite Material Properties			
Material System - HyE2034D Fiber - VSC-32 Matrix - 934 Maximum Temperature Rating - 350°F (177°C) Resin Content - 23.8% by wt. Fiber Content - 67.9% by vol. Void Content - ± 0 Test Method - Straight-sided tension Reference - ASTM D2290 and D3039			HMG/Epoxy
Prepreg by - Fiberite Laminate Sp. Gr. - 1.80 Nominal Ply Thickness - 0.0050 inch No. of panels from which specimens were tested in this table - 18 Thickness of each type specimen: (0/+45/90) - 20 ply +45 - 8 ply			
STRESS RUPTURE			
Temperature	Fiber Orientation	(0,+45,-45,0,0,-45,+45,0,90,0) _g	+45°
72°F (22°C)	Stress Level[ksi] (MPa)	[60.7] (418)	[8.68] (59.8)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[76.8] (529)	[11.24] (77.4)
	No. of Specimens	3	3
	Stress Level[ksi] (MPa)	[53.1] (366)	[7.30] (50.3)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
260°F (127°C)	Residual Strength[ksi] (MPa)	[75.5] (520)	[11.30] (77.9)
	No. of Specimens	3	3
	Stress Level[ksi] (MPa)	[60.0] (413)	[6.57] (45.3)
	Time to Failure(hrs)	21	425+ ¹
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	---	[11.12] (76.6)
	No. of Specimens	0	2
	Stress Level[ksi] (MPa)	[50.0] (345)	[5.63] (38.8)
350°F (177°C)	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[77.0] (531)	[11.97] (82.5)
	No. of Specimens	3	3
	Stress Level[ksi] (MPa)	[66.2] (456)	[5.25] (36.2)
	Time to Failure(hrs)	456+ ¹	116
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[82.6] (569)	---
	No. of Specimens	2	0
	Stress Level[ksi] (MPa)	[58.0] (399)	[4.38] (30.2)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi] (MPa)	[76.7] (528)	[7.33] (50.5)
	No. of Specimens	3	3

Two specimens survived for 500 hrs. without failure.

TABLE 44
TENSION-TENSION FATIGUE PROPERTIES OF HyE2034D
COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 2034D		Prepreg by - Fiberite		HMG/Epoxy
Fiber - VSC-32 Matrix - 934		Laminate Sp. Gr. - 1.81		
Maximum Temperature Rating - 350°F(177°C)		Nominal Ply Thickness - 0.0050 inch		
Resin Content - 24.8% by wt.		No. of panels from which specimens were tested		
Fiber Content - 67.9% by vol.		in this table - 10		
Void Content - ~ 0		Thickness of each type specimen:		
Test Method - Straight-sided tension		+45° - 8 ply		
Reference - ASTM D3039		0/+45/90° - 20 ply		
TENSILE FATIGUE, R=0.1 (3)				
Temperature	Fiber Orientation	+45°	0/+45/90°(1)	0/+45/90°(1,2)
72°F(22°C)	Max. Stress[ksi](MPa)	[8.68] (59.8)	[75.8] (522)	[61.5] (424)
	Lifetime (cycles)	22,706	34,123	5,148
	No. of Specimens	5	5	3
	Residual Strength[ksi](MPa)	---	---	---
	No. of Specimens	0	0	0
	Max. Stress[ksi](MPa)	[8.14] (56.1)	[73.9] (509)	[60.00] (413)
	Lifetime (cycles)	73,132	11,625	20,000
	No. of Specimens	5	3	3
	Residual Strength[ksi](MPa)	---	---	[67.2] (463)
	No. of Specimens	0	0	1
	Max. Stress[ksi](MPa)	[6.51] (44.9)	[72.0] (496)	[58.3] (401)
	Lifetime (cycles)	7,715,394	96,015	7,602,215+
	No. of Specimens	4	5	34
	Residual Strength[ksi](MPa)	[9.80] (68.0)	[79.2] (546)	[70.4] (485)
	No. of Specimens	3	2	1
260°F(127°C)	Max. Stress[ksi](MPa)	[7.98] (55.0)		
	Lifetime (cycles)	3,870		
	No. of Specimens	5		
	Residual Strength[ksi](MPa)	---		
	No. of Specimens	0		
	Max. Stress[ksi](MPa)	[7.04] (48.5)		
	Lifetime (cycles)	132,425		
	No. of Specimens	5		
	Residual Strength[ksi](MPa)	---		
	No. of Specimens	0		
	Max. Stress[ksi](MPa)	[6.57] (45.3)		
	Lifetime (cycles)	987,695		
	No. of Specimens	4		
	Residual Strength[ksi](MPa)	---		
	No. of Specimens	0		

- NOTES: 1. Stacking sequence (0, +45, -45, 0, 0, -45, +45, 0, 90, 0).
2. These specimens had a 0.1935 inch (0.491 cm) hole in the center of the test section. Stresses calculated using net cross-sectional area.
3. Fatigue lifetimes are log mean values. All residual strengths determined by tensile test at 72°F (22°C).
4. One specimen survived to 10⁷ cycles without failure.

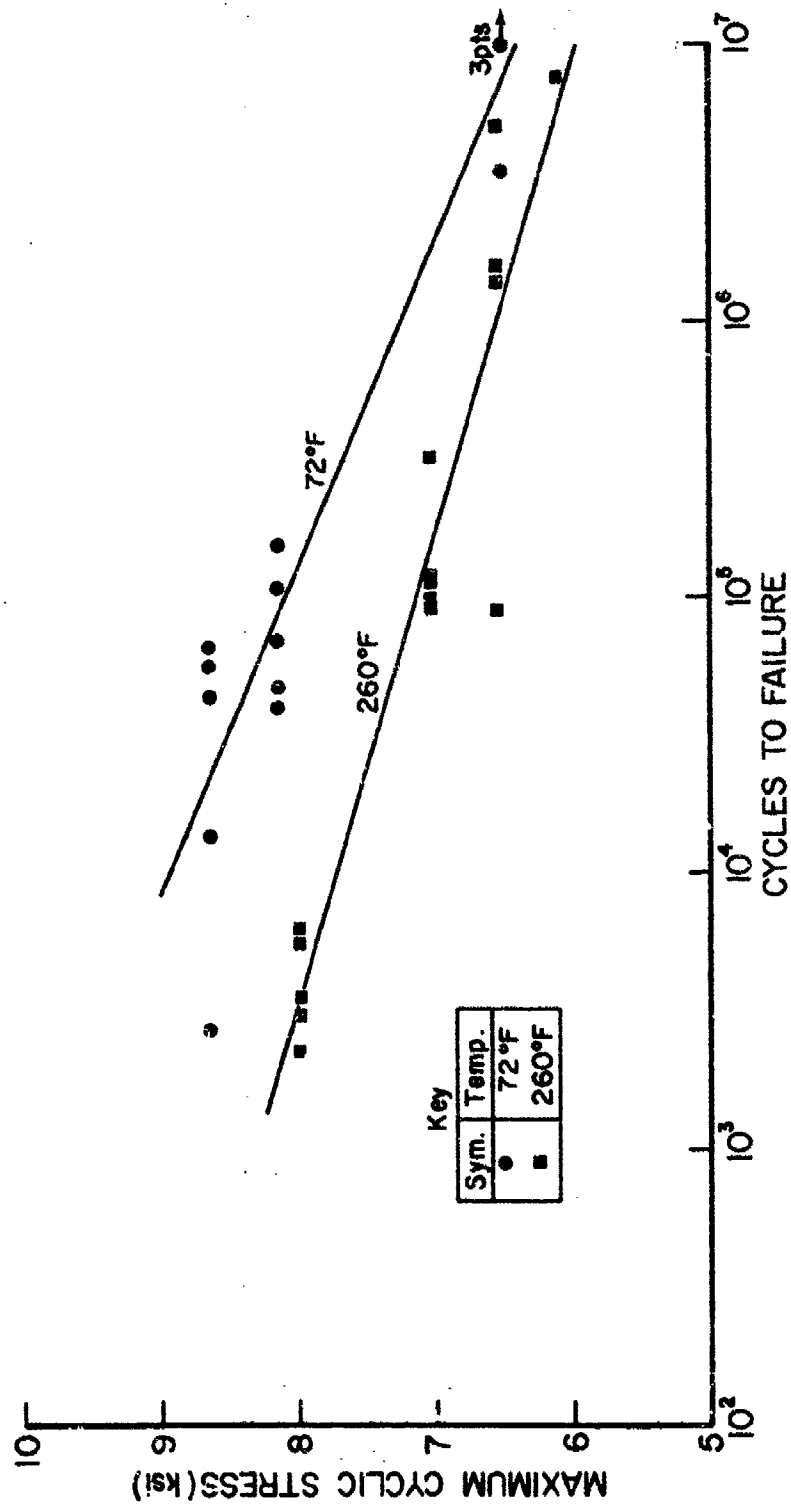


Figure 55 . Tensile-Tensile Fatigue Behavior of Bidirectional HyE 2034D Composite
Laminates: $\pm 45^\circ$ Fiber Orientation, $R = 0.10$, 10 Hz.

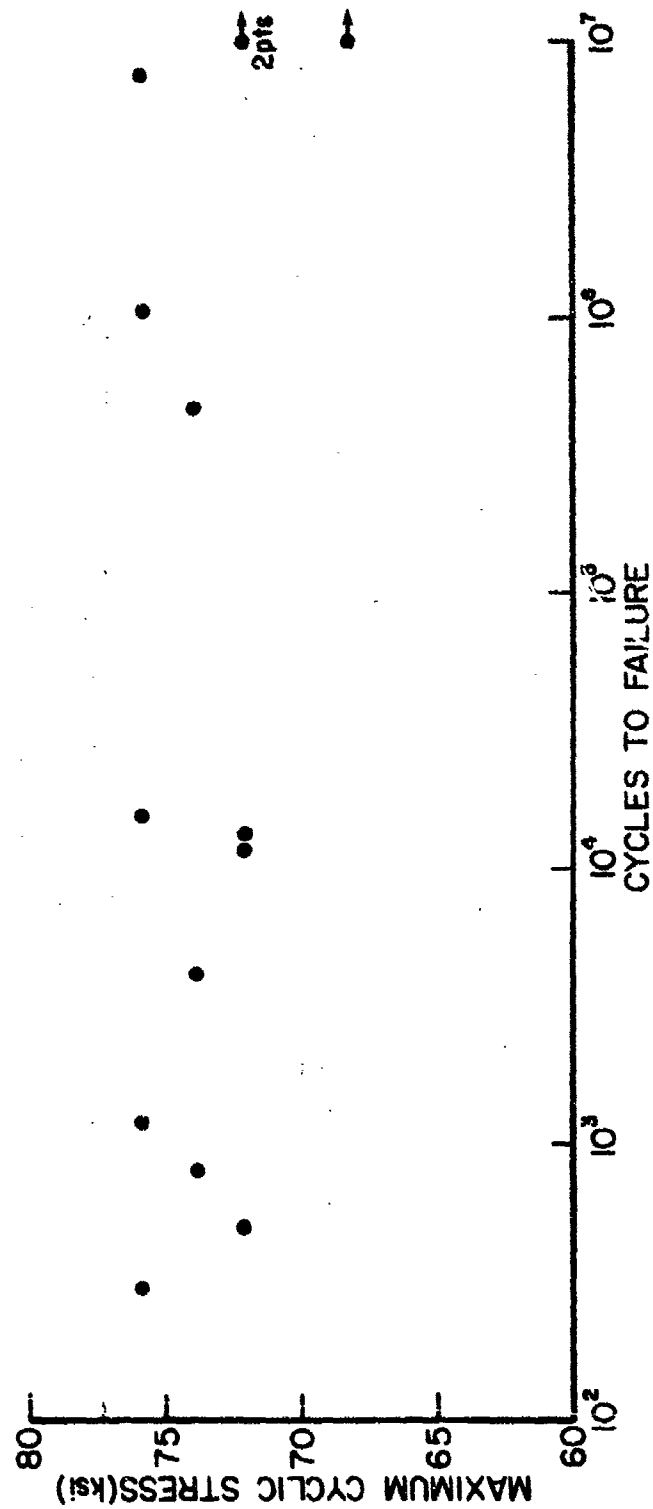
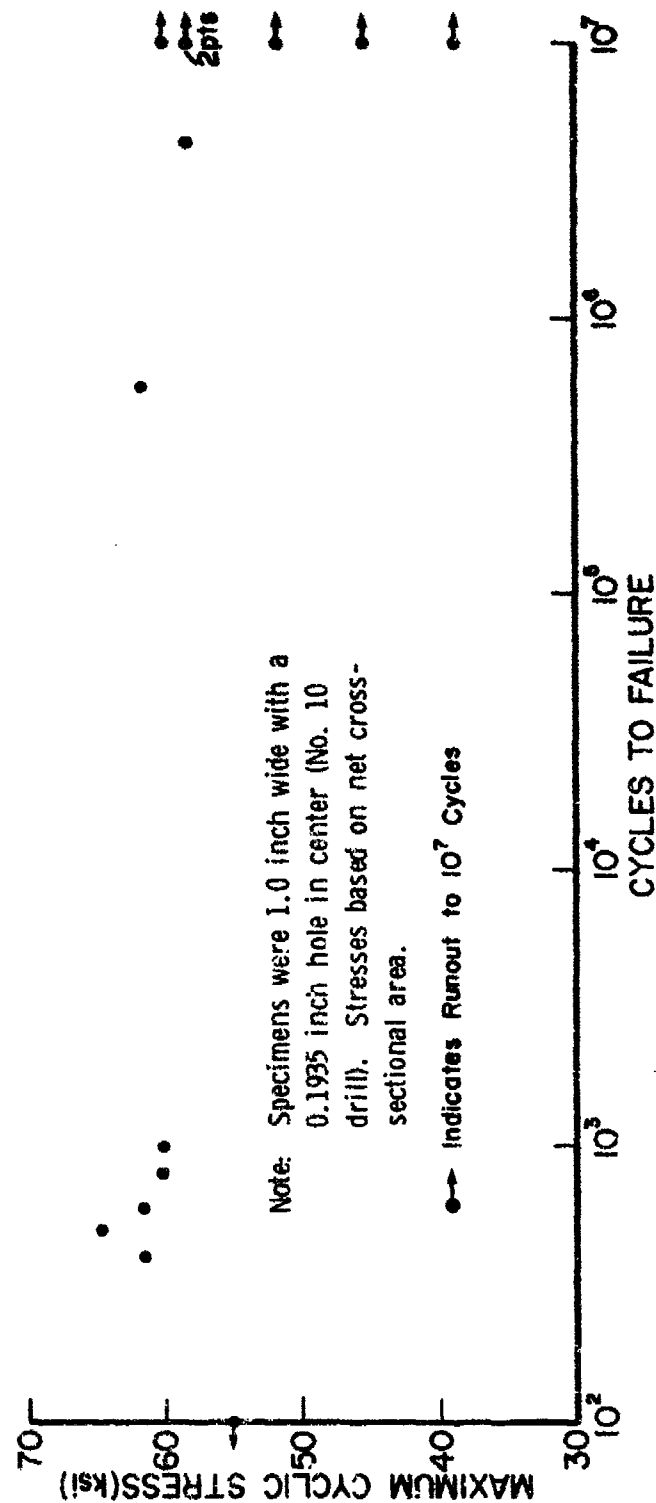


Figure 56. Tensile-Tensile Fatigue Behavior of Multidirectional HyE 2034D Composite Laminates at 72°F (22°C): (0,45,-45,0,0,-45,45,0,90,0)_s Fiber Orientation, R = 0.10, 10 Hz.



Note: Specimens were 1.0 inch wide with a 0.1935 inch hole in center (No. 10 drill). Stresses based on net cross-sectional area.

●→ Indicates Runout to 10^7 Cycles

Figure 57. Tensile-Tensile Fatigue Behavior of Multidirectional HYE 2034D Composite Laminates at 72°F (22°C): (0,45,-45,0,0,-45,45,0,90,0)° Fiber Orientation, R = 0.10, 10 Hz.

TABLE 45
THERMOPHYSICAL PROPERTIES OF HyE2034D
COMPOSITE LAMINATES

Composite Material Properties					
Material System - HyE 2034D		Prepreg by - Fiberite		HMC/Epoxy	
Fiber - VSC-32 Matrix - 934		Laminate Sp.-Gr. - 1.79			
Maximum Temperature Rating - 350°F(177°C)		Average Ply Thickness - 0.0050 inch			
Resin Content - 26.5% by wt.		No. of panels from which specimens were tested			
Fiber Content - 65.7% by vol.		in this table - 3			
Void Content - ~0		Thickness of each type specimen: Therm. Exp. - 40 ply		Spec. Ht. - 1 ply	
		Therm. Cond. - 40 ply		Glass Trans. - 8 ply	
THERMOPHYSICAL PROPERTIES: 0°					
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)	Test Method
Thermal Expansion ¹					TMA ²
α_x [μ in/in-°F] (μ cm/cm-°C)	[-0.68](-1.22)	[-0.86](-1.54)	[-0.89](-1.61)	[-1.08](-1.94)	
α_y [μ in/in-°F] (μ cm/cm-°C)	[32.1](57.8)	[22.0](39.6)	[17.0](30.6)	[15.1](27.1)	
No. of Specimens per direction	3	3	3	3	
Specific Heat					DSC ³
C_p [btu/lb.-°F] (J/kg-°C)	[0.110](460)	[0.202](846)	[0.642](2689)	[0.718](3010)	
No. of Specimens	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.52] (0.89)	[0.67] (1.16)	[0.89] (1.53)	[0.99] (1.70)	
No. of Specimens	3	3	3	3	
Glass Transition Temp.					DMA ⁴
Dry [°F](°C)	[430](221)				
Wet [°F](°C)	[342](172)				
THERMOPHYSICAL PROPERTIES: +45°					
Thermal Expansion ¹					TMA ²
α_x [μ in/in-°F] (μ cm/cm-°C)	[-0.15](-0.27)	[-0.22](-0.40)	[-0.36](-0.64)	[-0.49](-0.89)	
No. of Specimens per direction	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.55] (0.94)	[0.56] (0.96)	[0.57] (0.99)	[0.59] (1.01)	
No. of Specimens	3	3	3	3	

NOTES: 1. On the unidirectionally reinforced specimens, the x-direction is along the fiber axis, the y-direction is across the fiber axis, and the z-direction is through the thickness (identical to the y-direction). On +45° bidirectionally reinforced specimens, the x and y directions are identical and oriented at 45° to either fiber direction, while the z-direction is through the thickness.

2. Thermo-mechanical analysis.

3. Differential scanning calorimetry.

4. Dynamic mechanical analysis.

TABLE 46
PRELIMINARY ACCUMULATED DATA FOR HyE 2034D¹

HyE 2034D (75 million modulus pitch) tested by various companies under different cure cycle and testing procedures. All mechanical test values, except shear, are normalized to 60% fiber volume. All testing was performed at room temperature.

	<u>Fiberite</u>	<u>TRW</u>	<u>Ryan</u>	<u>G.D. Convair²</u>	<u>G.D. Convair³</u>
F _{fu} - Ksi	99	95	84	91/--	85/--
E _f - Msi	37	39	34 ⁴	-----	33/--
F _{su} - Ksi	10	8	9	9/--	7/--
F _{tu} - Ksi	110	121	123	108/39	87/32
E _t - Msi	46	43	47	44/15	46/15
F _{cu} - Ksi			54 ⁵		
E _c - Msi			38 ⁵		

¹All information in this table provided by FIBERITE.

²Cure cycle 1, (0°)₁₂/(0, 45, 90, 135)_g
Apply vacuum at R.T., heat at 3°F/minute to 250 ± 5°F, hold 30 minutes, apply 100 psig, hold an additional 30 minutes, heat at 3°F/minute to 275 ± 5°F. Hold six hours, cool to below 150°F at a rate not to exceed 5°F/minute under vacuum and 100 psig, debag and free stand postcure for 20 hours at 275 ± 5°F.

³Cure cycle 2, (0°)₁₂/(0, 45, 90, 135)_g
Apply vacuum at R.T., heat at 3°F/minute to 250 ± 5°F, hold 45 minutes, apply 100 psig, hold an additional 45 minutes, heat at 3°F/minute to 350 ± 5°F, hold two hours. Cool to below 150°F at a rate not to exceed 5°F/minute under vacuum and 100 psig.

⁴May be in error due to deflectometer troubles.

⁵Celanese compression tests.

4.4 T300/V378A

This graphite/polyimide system is based on a resin matrix system developed by U.S. Polymeric.

Tables 47 through 59 present the data generated for this nominal 450°F (232°C) graphite/polyimide system. Figures 58 through 73 illustrate the stress-strain, fatigue, and creep behavior of the material as well as the effects of humidity aging upon selected composite properties.

Probably the most unusual characteristic of this system is the very noticeable odor of the prepreg. This arises from a volatile reactive constituent in the resin and not only is offensive to those working with the prepreg, but also results in an abbreviated out-life for the prepreg. When a sufficient amount of this volatile reactant has vaporized, good quality laminates can no longer be fabricated. The substantial differences between the HPLC analyses on new and old V378A prepreg presented in Appendix B (pages 279 and 280) illustrate the dramatic changes undergone by the resin system even in 0°F (-18°C) storage. The first five peaks in the HPLC are very significantly reduced on the old material, while the last three have disappeared completely.

TABLE 47
PROCESSING CONDITIONS FOR T300/V378A
COMPOSITE LAMINATES

Composite Processing Information	
Material System - V373A	Gr/PI
Fiber - T300 w/epoxy size Matrix - V378A	
Maximum Rated Temperature - 450°F (232°C)	Prepreg by -U.S. Polymeric
<p style="text-align: center;">Laminate Processing Schedule</p> <p>Layup Procedure: The prepreg was stored in a closed wrapper at 0°F (-18°C). Prepreg was warmed to room temperature before removal from wrapper to prevent moisture condensation on prepreg. Plies were cut to desired size with razor knife and stacked in desired sequence (release paper removed) from each ply). The stack was placed in the autoclave according to the layup system illustrated in Figure 58. The corprene edge dam serves to restrict fiber flow.</p> <p>Cure Schedule: Apply full vacuum and 85 psi above bladder at room temperature. Heat to 175°F (80°C) at a rate of 4°F/min. Vent vacuum at 175°F (80°C) and hold at temperature for 2 hours. Heat up to 355°F (180°C) at a rate of 4°F/min. and hold at 355°F (180°C) for 4 hours. Reduce pressure to 10 psi then cool to below 150°F (66°C). Remove panel from autoclave and start postcure.</p> <p>Postcure Schedule: Heat to 475°F (246°C) and hold for 4 hours. Increase temperature to 550°F (288°C) and hold for 1 hour. Cool panels to below 150°F (66°C) and remove.</p>	

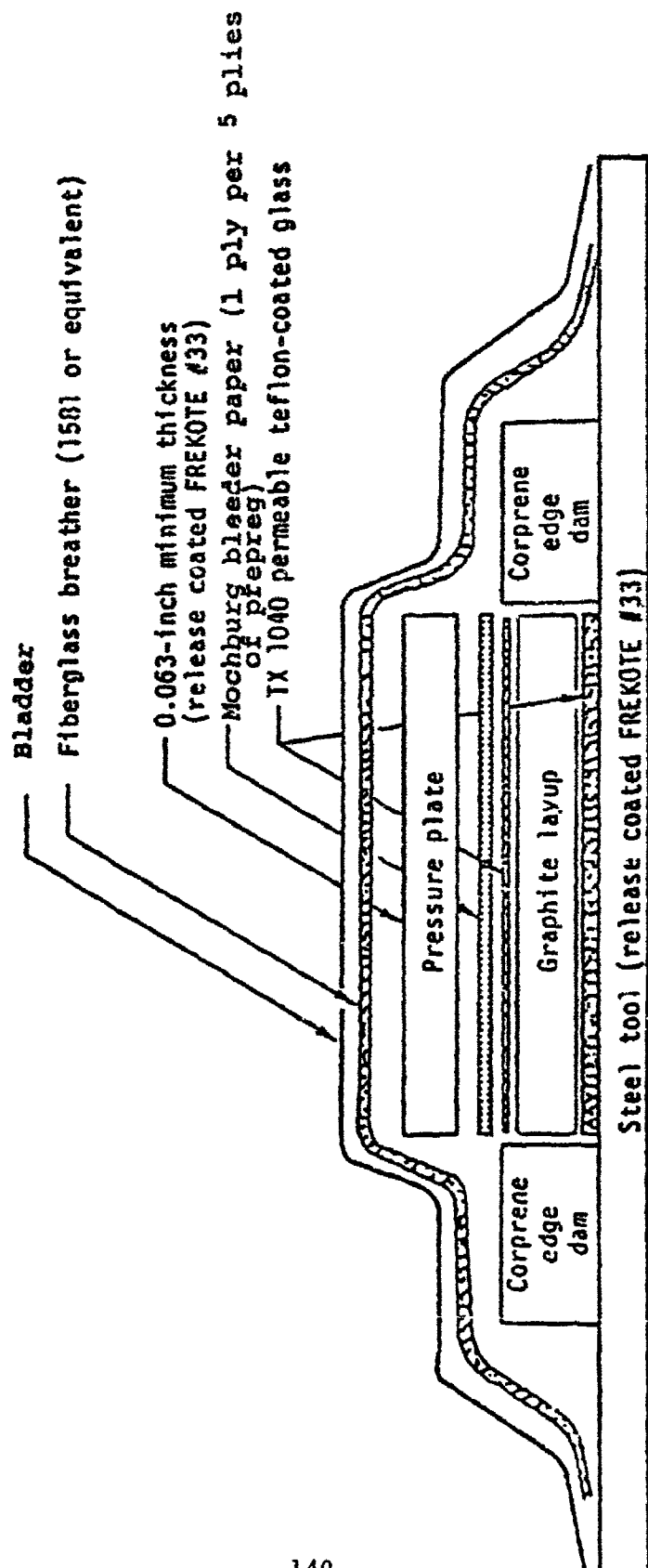


Figure 58. Layup System for V378A Laminates.

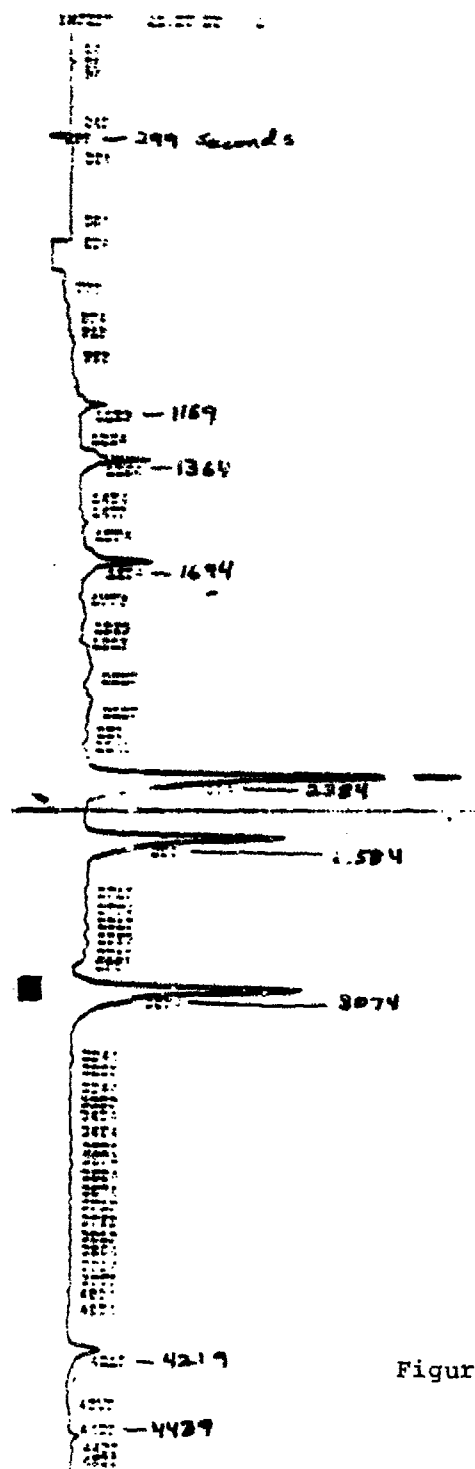
TABLE 48

PREPREG AND COMPOSITE PHYSICAL PROPERTIES

Composite Physical Property Information				
Material System - T300/V378A Fiber - T300 Matrix - V378A Maximum Rated Temperature - 450°F(232°C)			Gr/Polyimide Prepreg by -U.S. Polymeric	
Prepreg Physical Properties				
(Property)	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
Volatile Content-5.5% by wt.	0.8%	4.6-6.1	QCI-C-V-14	Fiberite
Resin Content- 30.6% by wt.	1.8%	29.0-32.6	R-15	Fiberite
Gel Time - 32.2 min@210°F	0.3 min	32.0-32.5	G-2	Fiberite
No. of Rolls Involved- 1				
No. of Batches Involved- 1				
Laminate Physical Properties ¹				
	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
No. of Panels- 36				
Fiber Content- 67.0% by wt.	2.2%	6.34-71.1%	see footnote 2	
Resin Content- 25.6% by wt.	2.2%	21.7-29.7%		
Void Content- 1.4 % by vol.	1.2%	0-4.3%	D 2734	ASTM
Laminate Sp. Gr.- 1.58	0.02	1.53-1.61	D792	ASTM
Fiber Sp. Gr.- 1.75	As reported by manufacturer.			
Matrix Sp. Gr.- 1.27	As reported by manufacturer.			
Thickness per ply- 0.0051 inch (0.13 mm)			---	---

¹The properties reported here represent averages for all panels of this material used throughout the program.

²An acid digestion method similar to that described in AFML-TR-67-243 was used with the following materials and temperatures. A mixture of concentrated sulfuric acid and hydrogen peroxide (30%) in the ratio of 80% to 20% by volume respectively was used as the digesting acid. The specimens were soaked in this solution at 375-400°F (190-204°C) until the acid turned dark. The acid was drained, the specimen rinsed, and fresh acid added. This sequence was repeated until the acid did not discolor and the residual fiber weight reached equilibrium.



HPLC ANALYSIS
 V378A - New*
 SAMPLE (CONC.) 0.19% SAMPLE SIZE 25 μ l
 MOBILE PHASE 1 H₂O MOBILE PHASE 2 Dioxane
 FLOW RATE 1.0 ml/min PROGRAM Meth C
 COLUMN(S) RP-8 (SP) DETECTOR Trans-UV
 ATTENUATION 16 WAVE LENGTH 254
 CHART SPEED 0.5 mm/min FULL SCALE (mV) 40
 DATE 10-2-80 OPERATOR A. Price

* 1 month storage at 0°F

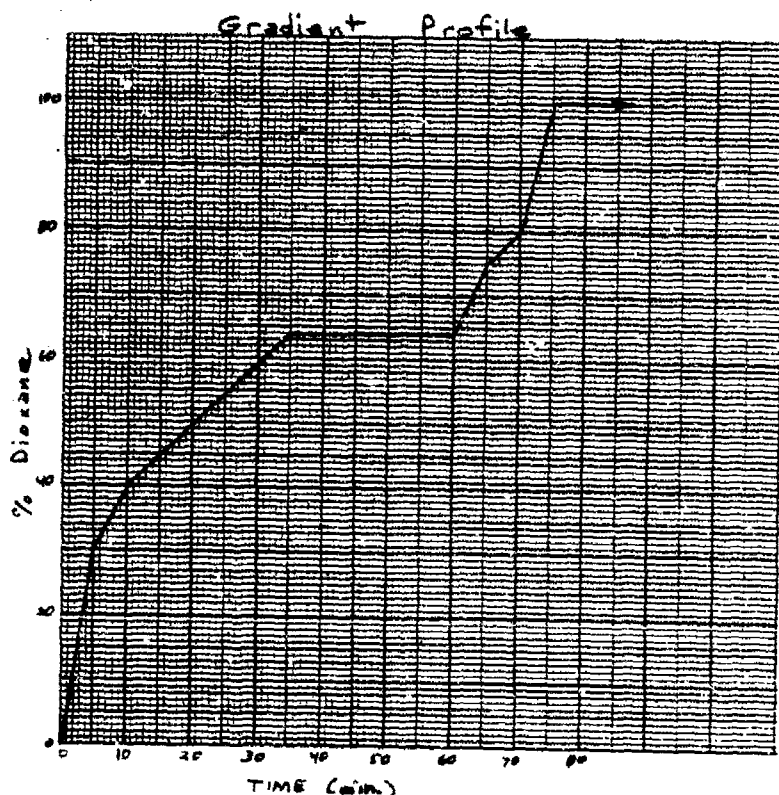


Figure 59. HPLC Analysis of V378A.

TABLE 49
TENSILE PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/V378A		Prepreg by - U.S. Polymeric		Gr/PI
Fiber - T300 Matrix - V378A		Laminate Sp. Gr. - 1.58		
Maximum Rated Temperature - 450°F (232°C)		Nominal Ply Thickness - 0.0052 inch (0.13 mm)		
Resin Content - 25.6% by wt.		No. of panels from which specimens were tested		
Fiber Content - 87.1% by vol.		in this table - 7		
Void Content - 1.1% by vol.				
Thickness of each type specimen: 0° - 6 ply		; 90° - 15 ply		
TENSION: 0°				
	-67°F (-55°C)	72°F (22°C)	150°F (177°C)	450°F (232°C)
F_x^{tu} (ksi) (MPa)	[222.3] (1532)	[230.2] (1586)	[210.1] (1448)	[217.3] (1497)
Stand. Dev. (ksi) (MPa)	[11.7] (218)	[25.0] (172)	[23.4] (161)	[15.3] (105)
Range (ksi) (MPa)	[172.4 - 250.0]	[189.7 - 250.6]	[103.9 - 239.4]	[200.8 - 240.3]
	(1188 - 1722)	(1307 - 1727)	(1267 - 1849)	(1384 - 1836)
No. of Specimens	5	5	5	5
F_y^{tpl} (ksi) (MPa)	[222.3] (1532)	[230.2] (1586)	[210.1] (1448)	[217.3] (1497)
Stand. Dev. (ksi) (MPa)	[11.7] (218)	[25.0] (172)	[23.4] (161)	[15.3] (105)
No. of Specimens	5	5	5	5
E_x^t (Msi) (GPa)	[20.0] (1.38)	[20.1] (1.38)	[22.1] (1.52)	[18.6] (1.30)
Stand. Dev. (Msi) (GPa)	[0.6] (4.3)	[0.4] (3.1)	[1.5] (10)	[1.1] (8)
No. of Specimens	5	5	5	5
ϵ_x^{tu} (in/in) (mm/mm)	10,130	10,510	9,770	11,180
Stand. Dev.	1,900	1,400	8,000	506
No. of Specimens	5	5	5	5
ν_{xy}^t	0.31	0.32	0.33	0.32
Stand. Dev.	0.02	0.03	0.03	0.04
No. of Specimens	5	5	5	5
Test Method	Straight-sided tension			
Reference	ASTM D3039			
TENSION: 90°				
F_{xy}^{tu} (ksi) (MPa)	[5.82] (40)	[5.37] (37)	[4.84] (33)	[4.21] (29)
Stand. Dev. (ksi) (MPa)	[0.91] (6.3)	[0.55] (3.8)	[0.38] (2.6)	[0.57] (3.9)
Range	[4.84 - 6.60]	[4.74 - 6.11]	[4.02 - 4.97]	[3.48 - 4.69]
	(32 - 46)	(33 - 42)	(27 - 34)	(24 - 32)
No. of Specimens	5	5	5	5
F_y^{tpl} (ksi) (MPa)	[5.82] (40)	[5.55] (24)	[3.62] (25)	[2.55] (18)
Stand. Dev. (ksi) (MPa)	[0.91] (6.3)	[0.94] (6.5)	[0.35] (2.4)	[0.64] (4.4)
No. of Specimens	5	5	5	5
E_y^t (Msi) (GPa)	[1.40] (9.6)	[1.31] (9.0)	[1.07] (7.4)	[1.00] (6.9)
Stand. Dev. (Msi) (GPa)	[0.01] (0.07)	[0.03] (0.2)	[0.03] (0.2)	[0.02] (0.1)
No. of Specimens	5	5	5	5
ϵ_y^{tu} (in/in) (mm/mm)	4,145	4,140	4,130	4,290
Stand. Dev.	600	410	390	630
No. of Specimens	5	5	5	5
ν_{yx}^t	0.022 ¹	0.020 ¹	0.016 ¹	0.017 ¹
Stand. Dev.	---	---	---	---
No. of Specimens	---	---	---	---
Test Method	Straight-sided tension			
Reference	ASTM D3039			

¹Computed using elastic moduli and longitudinal Poisson's ratio.

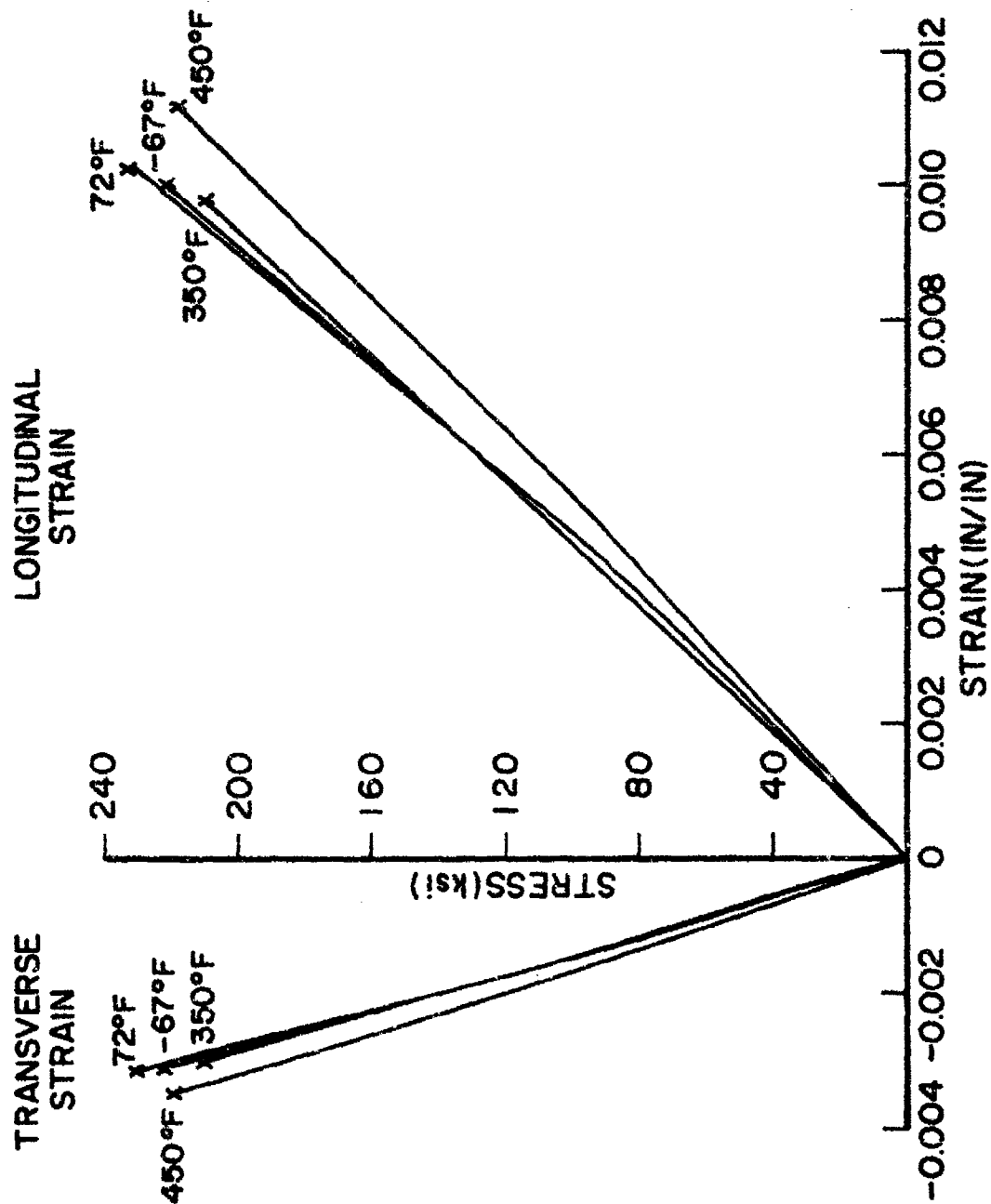


Figure 60. Tensile Stress-Strain Curve for Unidirectional T300/V378A Composite Laminates: 0° Fiber Orientation.

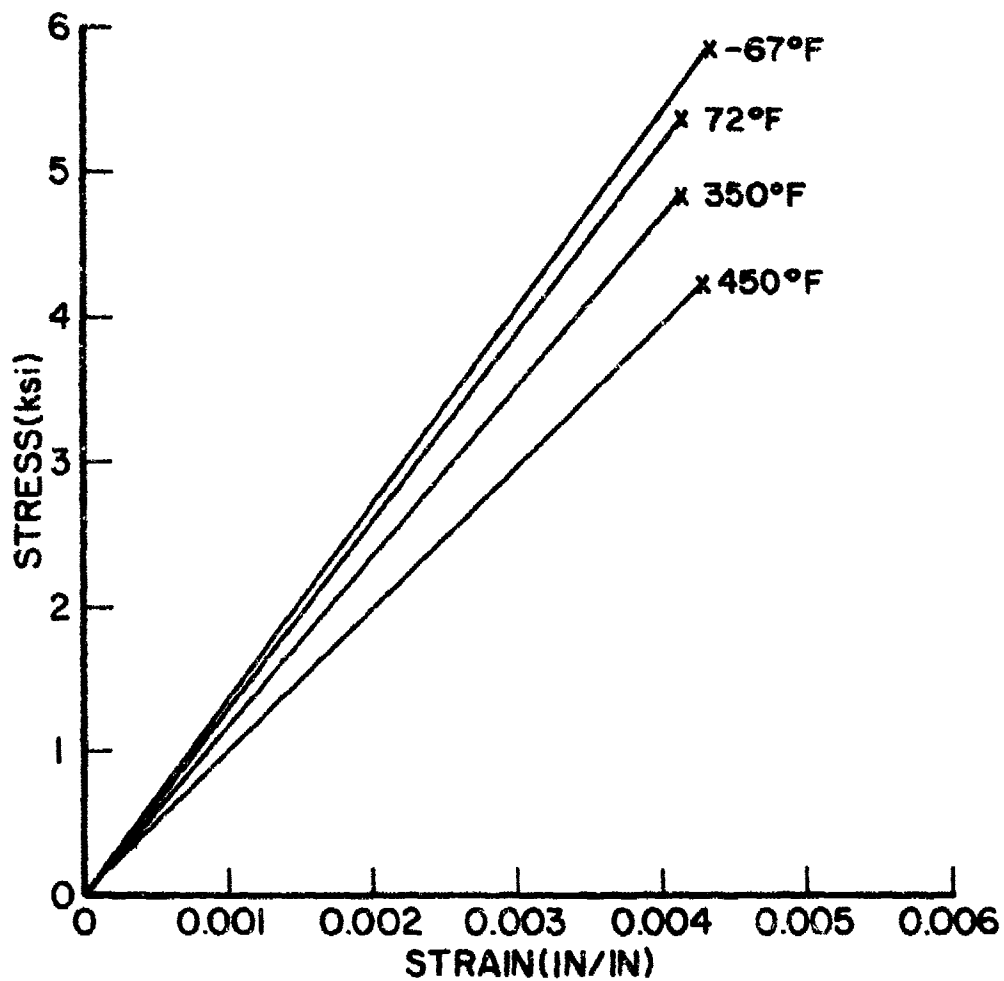


Figure 61. Tensile Stress-Strain Curves for Unidirectional T300/V378A Composite Laminates: 90° Fiber Orientation.

TABLE 50
TENSILE PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/V378A		Prepreg by - U.S. Polymeric		Gr/Polyimide
Fiber - T300 Matrix - V378A		Laminate Sp. Gr. - 1.59		
Maximum Rated Temperature - 450°F(232°C)		Nominal Ply Thickness - 0.0052 inch(0.13 mm)		
Resin Content - 26.9% by wt.		No. of panels from which specimens were tested		
Fiber Content - 66.1% by vol.		in this table - 8		
Void Content - 0.8% by vol.		Thickness of specimen - 8 ply		
TENSION: $\pm 45^\circ$				
	-67°F(-55°C)	72°F(22°C)	350°F(177°C)	450°F(232°C)
F_x^{tu} [ksi] (MPa)	[21.52] (148)	[21.29] (147)	[16.12] (111)	[14.94] (103)
Std.Dev. [ksi] (MPa)	[1.17] (8.1)	[1.29] (8.9)	[0.69] (4.8)	[0.34] (2.3)
Range [ksi] (MPa)	[20.33 - 23.12] (140 - 159)	[19.18-22.14] (132-153)	[14.96-16.77] (103-116)	[14.46 - 15.41] (100 - 106)
No. of Specimens	5	5	5	5
F_x^{tpl} [ksi] (MPa)	[8.32] (57)	[6.35] (44)	[4.49] (31)	[3.46] (24)
Std.Dev. [ksi] (MPa)	[0.83] (5.7)	[0.67] (4.6)	[0.59] (4.1)	[0.73] (5.0)
No. of Specimens	5	5	5	5
E_x^t [ksi] (GPa)	[3.13] (22)	[2.96] (20)	[2.54] (18)	[2.16] (15)
Std.Dev. [ksi] (GPa)	[0.16] (1.1)	[0.03] (0.2)	[0.13] (0.9)	[0.11] (0.8)
No. of Specimens	5	5	5	5
ϵ_x^{tu} [in/in] (µm/cm)	9,020	12,100	27,070	20,320
Std. Dev.	930	140	11,020	230
No. of Specimens	5	5	5	5
ν_{xy}^t	0.70	0.59	1.00	0.82
Std. Dev.	0.05	0.04	0.07	0.03
No. of Specimens	5	5	4	5
Test Method	Straight-sided tension			
Reference	ASTM D3039			

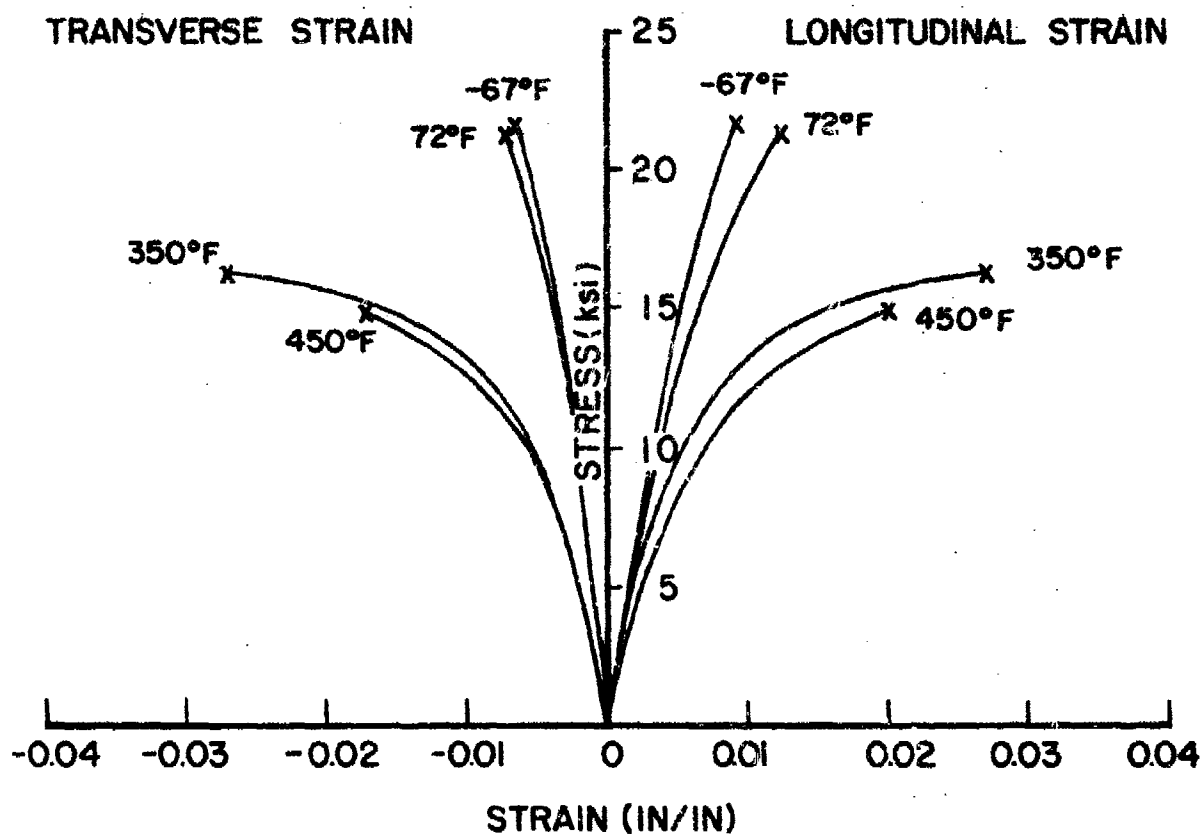


Figure 62. Tensile Stress-Strain Curves for Bidirectional T300/V378A Composite Laminates: $+45^\circ$ Fiber Orientation.

TABLE 51
TENSILE PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/V378A		Prepreg by - U.S. Polymeric		Gr/Polyimide
Fiber - T300 Matrix - V378A		Laminate Sp. Gr. - 1.57		
Maximum Rated Temperature - 450°F (232°C)		Nominal Ply Thickness - 0.0053 inch (0.13 mm)		
Resin Content - 25.7% by wt.		No. of panels from which specimens were tested		
Fiber Content - 54.6% by vol.		in this table - 13		
Void Content - 1.8% by vol.				
Thickness of each type specimen: 20 ply				
THICKNESS: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0)°				
	-67°F (-55°C)	72°F (22°C)	150°F (177°C)	450°F (232°C)
E_x^{tu} (ksi) (MPa)		[119.7] (825)	[106.1] (731)	[107.5] (741)
Stand. Dev. (ksi) (MPa)		[12.8] (88)	[11.4] (79)	[12.1] (83)
Range (ksi) (MPa)		[102.6-130.4]	[90.3 - 119.6]	[88.9 - 119.2]
No. of Specimens		5	5	5
E_x^{tp} (ksi) (MPa)		[119.7] (825)	[106.1] (731)	[107.5] (741)
Stand. Dev. (ksi) (MPa)		[12.8] (88)	[11.4] (79)	[12.1] (83)
No. of Specimens		5	5	5
E_x^c (ksi) (GPa)		[13.96] (96)	[13.41] (92)	[13.15] (91)
Stand. Dev. (ksi) (GPa)		[1.13] (7.8)	[2.43] (16.7)	[0.80] (5.5)
No. of Specimens		5	5	5
ϵ_x^{tu} (in/in) (mm/mm)		10,590	9,020	9,380
Stand. Dev.		170	910	1,463
No. of Specimens		5	5	5
ν_{xy}^t		0.59	0.62	0.52
Stand. Dev.		0.05	0.07	0.11
No. of Specimens		5	5	5
Test Method	ASTM D3039			
Reference				
THICKNESS: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0)°, with 0.1935 inch (0.491 cm) hole				
E_y^{tu} (ksi) (MPa)		[93.1] (641)		
Stand. Dev. (ksi) (MPa)		[14.2] (98)		
Range		[79.9-112.5]		
No. of Specimens		5		
E_y^{tp} (ksi) (MPa)				
Stand. Dev. (ksi) (MPa)				
No. of Specimens				
E_y^c (ksi) (GPa)				
Stand. Dev. (ksi) (GPa)				
No. of Specimens				
ϵ_y^{tu} (in/in) (mm/mm)				
Stand. Dev.				
No. of Specimens				
ν_{yx}^t				
Stand. Dev.				
No. of Specimens				
Test Method				
Reference				

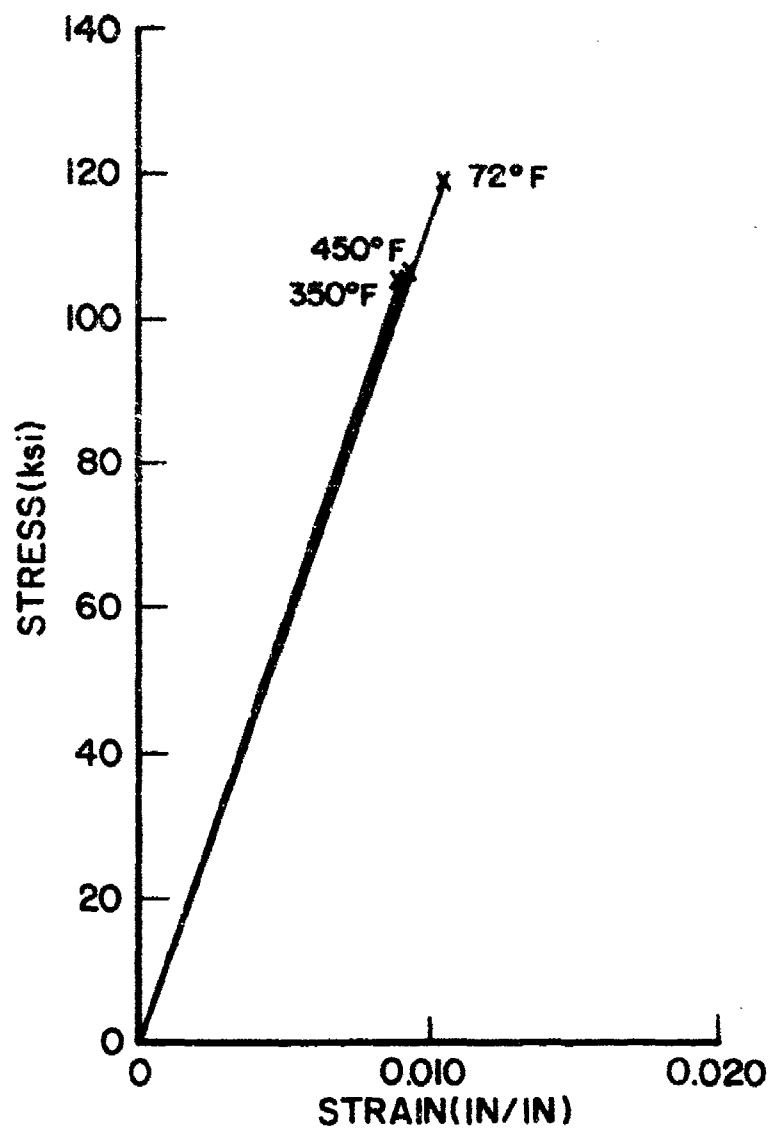


Figure 63 . Tensile Stress-Strain Curves for Multidirectional T300/V378A Composite Laminates: (0,45,-45,0,0,-45,45,0,90,0)_s Fiber Orientation.

TABLE 52
COMPRESSIVE PROPERTIES OF T300/V378A
COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/V378A		Prepreg by - U.S. Polymeric		Gr/Polyimide
Fiber - T300 Matrix - V378A				
Maximum Rated Temperature - 450°F (232°C)		Laminate Sp. Gr. - 1.60		
Resin Content - 24.2% by wt.		Nominal Ply Thickness - 0.0050 inch (0.13 mm)		
Fiber Content - 69.1% by vol.		No. of panels from which specimens were tested		
Void Content - 0.8% by vol.		in this table - 2		
Thickness of each type specimen: 0° - 20 ply ; 90° - 20 ply				
COMPRESSION: 0°				
	-67°F (-55°C)	72°F (22°C)	350°F (177°C)	450°F (232°C)
F_x^{cu} [ksi] (MPa)	[213.4] (1470)	[192.6] (1327)	[162.1] (1117)	[100.6] (693)
Std. Dev. [ksi] (MPa)	[17.9] (123)	[16.0] (110)	[22.4] (154)	[26.4] (182)
Range [ksi] (MPa)	[189.7-238.1] (1307-1640)	[168.5-212.8] (1161-1466)	[136.8-195.0] (943-1344)	[79.4 - 145.9] (547 - 1003)
No. of Specimens	5	5	5	5
F_y^{cpl} [ksi] (MPa)	[45.3] (312)	[140.0] (965)	[123.3] (850)	[85.5] (589)
Std. Dev. [ksi] (MPa)	[15.0] (103)	[83.3] (574)	[50.5] (348)	[44.6] (307)
No. of Specimens	5	5	5	5
E_x^c [Msi] (GPa)	[19.6] (135)	[19.8] (136)	[23.4] (161)	[20.8] (143)
Std. Dev. [Msi] (GPa)	[1.7] (12)	[0.6] (4)	[1.4] (10)	[2.3] (16)
No. of Specimens	5	5	5	5
ϵ_x^{cu} [in/in] ($\mu\text{cm/cm}$)	12,940 ^{+1,2}	16,120 ^{+1,3}	8,120	5,140
Std. Dev.	5,490	3,170	2,760	1,530
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3410			
COMPRESSION: 90°				
F_y^{cu} [ksi] (MPa)	[37.9] (261)	[26.8] (185)	[19.0] (131)	[20.2] (139)
Std. Dev. [ksi] (MPa)	[11.6] (80)	[2.1] (14)	[2.1] (14)	[3.2] (22)
Range	[28.2-54.7] (194-377)	[24.4-28.5] (168-196)	[16.2-21.8] (112-150)	[17.6 - 25.5] (121 - 155)
No. of Specimens	5	5	5	5
F_y^{cpl} [ksi] (MPa)	[16.1] (111)	[5.9] (41)	[5.2] (36)	[6.8] (47)
Std. Dev. [ksi] (MPa)	[13.2] (91)	[2.3] (16)	[1.5] (10)	[6.5] (45)
No. of Specimens	5	5	5	5
E_y^c [Msi] (GPa)	[2.5] (17)	[2.5] (17)	[1.6] (11)	[1.2] (8)
Std. Dev. [Msi] (GPa)	[1.0] (7)	[0.9] (6)	[0.3] (2)	[0.1] (1)
No. of Specimens	5	5	5	5
ϵ_y^{cu} [in/in] ($\mu\text{cm/cm}$)	23,360 ^{+1,3}	23,820 ^{+1,4}	13,820 ^{+1,2}	18,880 ^{+1,5}
Std. Dev.	7,170	7,820	4,260	16,870
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3410			

¹Ultimate strain values represent maximum observed strain rather than ultimate values.

²Three of five specimens exhibited evidence of buckling.

³One of five specimens exhibited evidence of buckling.

⁴All five specimens exhibited evidence of buckling.

⁵Two of five specimens exhibited evidence of buckling.

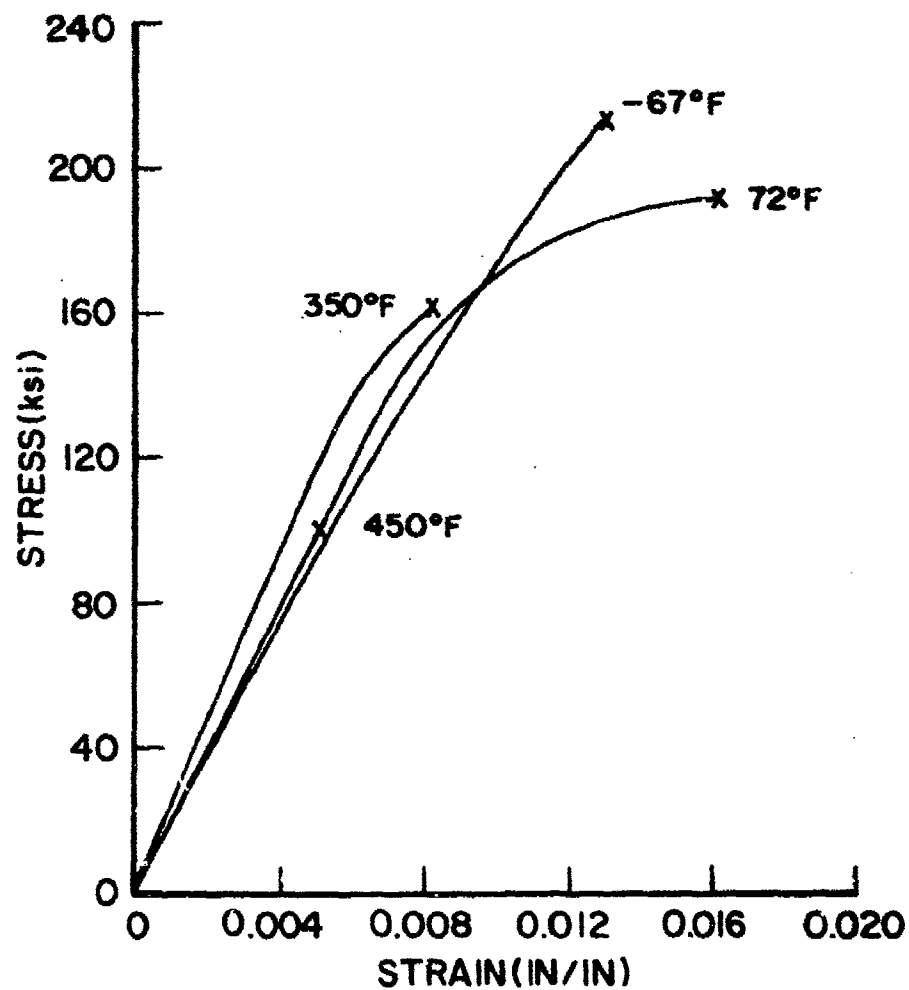


Figure 64. Compressive Stress-Strain Curves for Unidirectional T300/V378A Composite Laminates: 0° Fiber Orientation.

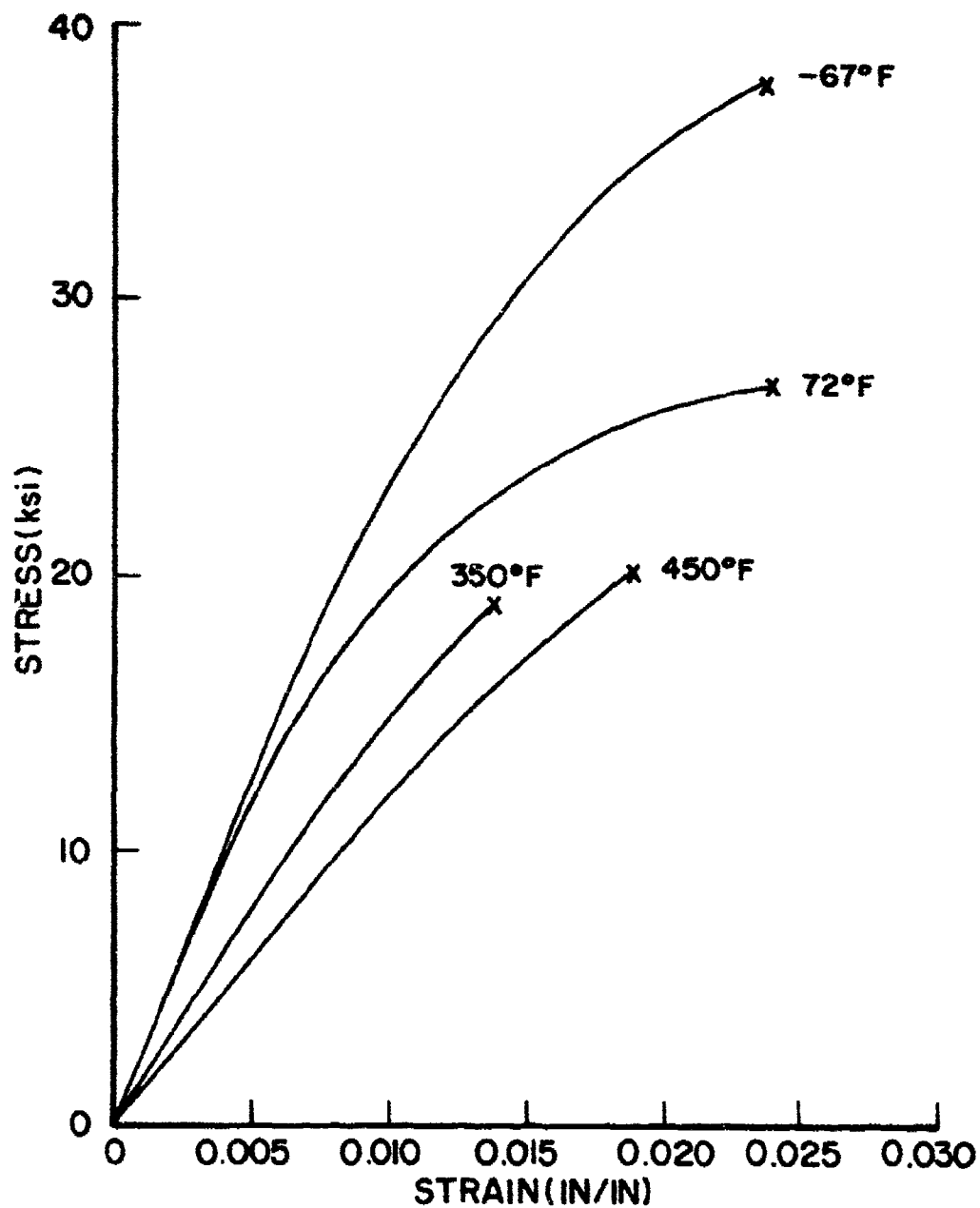


Figure 65. Compressive Stress-Strain Curves for Unidirectional T300/V378A Composite Laminates: 90° Fiber Orientation.

TABLE 53
FLEXURAL PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/V378A		Prepared by - U.S. Polymeric		Gr/Polyimide
Fiber - T300 Matrix - V378A		Laminate Sp. Gr. - 1.57		
Maximum Rated Temperature - 450°F (232°C)		Nominal Ply Thickness - 0.0054 inch (0.14 mm)		
Resin Content - 23.2% by wt.		No. of panels from which specimens were tested		
Fiber Content - 69.0% by vol.		in this table - 2		
Void Content - 2.6% by vol.				
Thickness of each type specimen: 0° - 14 ply ; 90° - 14 ply				
FLEXURE: 0°				
	-57°F (-55°C)	72°F (22°C)	350°F (177°C)	450°F (232°C)
F_x^u [ksi] (MPa)	[270.7] (1865) ¹	[224.6] (1547) ²	[170.5] (1175) ³	[164.1] (1131) ⁴
Std.Dev. [ksi] (MPa)	[15.8] (109)	[5.2] (36)	[6.3] (43)	[9.5] (65)
Range [ksi] (MPa)	[348.4-289.4] (1711-1994)	[219.5-232.3] (1512-1601)	[163.4-175.4] (1126-1209)	[156.5-176.1] (1078-1213)
No. of Specimens	5	5	3	5
E_x^f [ksi] (GPa)	[16.0] (110)	[17.2] (119)	[15.6] (107)	[16.1] (111)
Std.Dev. [ksi] (GPa)	[0.7] (5)	[1.2] (8)	[0.6] (4)	[0.6] (4)
No. of Specimens	5	5	3	5
Test Method Reference	3 pt. flexure 4 pt. flexure 3 pt. flexure 3 pt. flexure Advanced Composite Design Guide; Jan., 1971 ⁵			
FLEXURE: 90°				
F_y^u [ksi] (MPa)	[11.18] (77.0)	[11.58] (79.8)	[8.39] (57.8)	[7.84] (54.0)
Std.Dev. [ksi] (MPa)	[2.12] (14.6)	[0.91] (6.3)	[1.19] (8.2)	[0.54] (3.7)
Range [ksi] (MPa)	[9.40 - 14.38] (64.8 - 99.1)	[10.33 - 12.35] (71.2 - 85.1)	[6.92 - 9.80] (47.7 - 67.5)	[7.07 - 8.52] (48.7 - 58.7)
No. of Specimens	5	5	5	5
E_y^f [ksi] (GPa)	[1.82] (12.5)	[1.74] (12.0)	[1.47] (10.1)	[1.29] (8.9)
Std.Dev. [ksi] (GPa)	[0.11] (0.8)	[0.05] (0.3)	[0.06] (0.4)	[0.09] (0.6)
No. of Specimens	5	5	5	5
Test Method Reference	4 pt. flexure Advanced Composite Design Guide; Jan., 1971 ⁵			

- NOTES:
1. All failures were in tension on lowest ply.
 2. Mixed failure mode. Some delamination, some tension on bottom ply, some compressive under upper loading nose.
 3. Mixed failure mode. Some tensile failure on bottom ply and some compressive failure on top ply. Two other specimens were tested in 4-point flexure but exhibited shear failures at a flexural stress level of 161.5 ksi (1113 MPa).
 4. Two specimens exhibited same mixed failure mode as those tested at 350°F (177°C). Three specimens exhibited only compressive failures on top ply.
 5. This procedure corresponds to ASTM D790 except for loading speed and, in the case of the 4-point test, the position of the two upper loading points.

TABLE 54
SHEAR PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/V378A		Prepreg by - U.S. Polymeric		Graphite/Polyimide
Fiber - T300 Matrix - V378A		Laminate Sp. Gr. - 1.59		
Maximum Rated Temperature - 450°F (232°F)		Nominal Ply Thickness - 0.0052 inch (0.13 mm)		
Resin Content - 25.7% by wt.		No. of panels from which specimens were tested in this table - 9		
Fiber Content - 66.3% by vol.				
Void Content - 0.8% by vol.				
Thickness of each type specimen - Inplane - 8 ply ; Interlaminar - 15 ply				
INPLANE SHEAR				
	-67°F (-55°C)	72°F (22°C)	350°F (177°C)	450°F (232°C)
τ_{xy}^{su} [ksi] (MPa)	[10.76] (74.1)	[10.64] (73.3)	[8.06] (55.5)	[7.47] (51.5)
Std.Dev. [ksi] (MPa)	[0.59] (4.1)	[0.61] (4.2)	[0.34] (2.3)	[0.17] (1.2)
Range [ksi] (MPa)	[10.17 - 11.56] (70.1 - 79.6)	[9.59 - 11.07] (66.1 - 76.3)	[7.48 - 8.39] (51.5 - 57.8)	[7.23 - 7.70] (49.8 - 53.1)
No. of Specimens	5	5	5	5
G_{xy}^s [ksi] (GPa)	[1.86] (12.8)	[1.62] (11.2)	[1.34] (9.2)	[1.15] (7.9)
Std.Dev. [ksi] (GPa)	[0.06] (0.4)	[0.05] (0.3)	[0.12] (0.8)	[0.11] (0.8)
No. of Specimens	5	5	5	5
Test Method	+45° Straight-sided tension			
Reference	J. Comp. Mtls. [Vol. 6, p. 252 & Vol. 7, p. 124]			
INTERLAMINAR SHEAR				
τ_{lu}^{su} [ksi] (MPa)	[18.14] (125)	[15.02] (103)	[10.02] (69)	[9.24] (64)
Std.Dev. [ksi] (MPa)	[0.63] (4.3)	[0.49] (3.4)	[0.62] (4.3)	[0.17] (1.2)
Range	[17.30-18.88] (119-130)	[14.23-15.56] (98-107)	[9.03-10.75] (62-74)	[8.96-9.43] (62-65)
No. of Specimens	5	10	5	5
Test Method	ASTM D2344			
Reference				

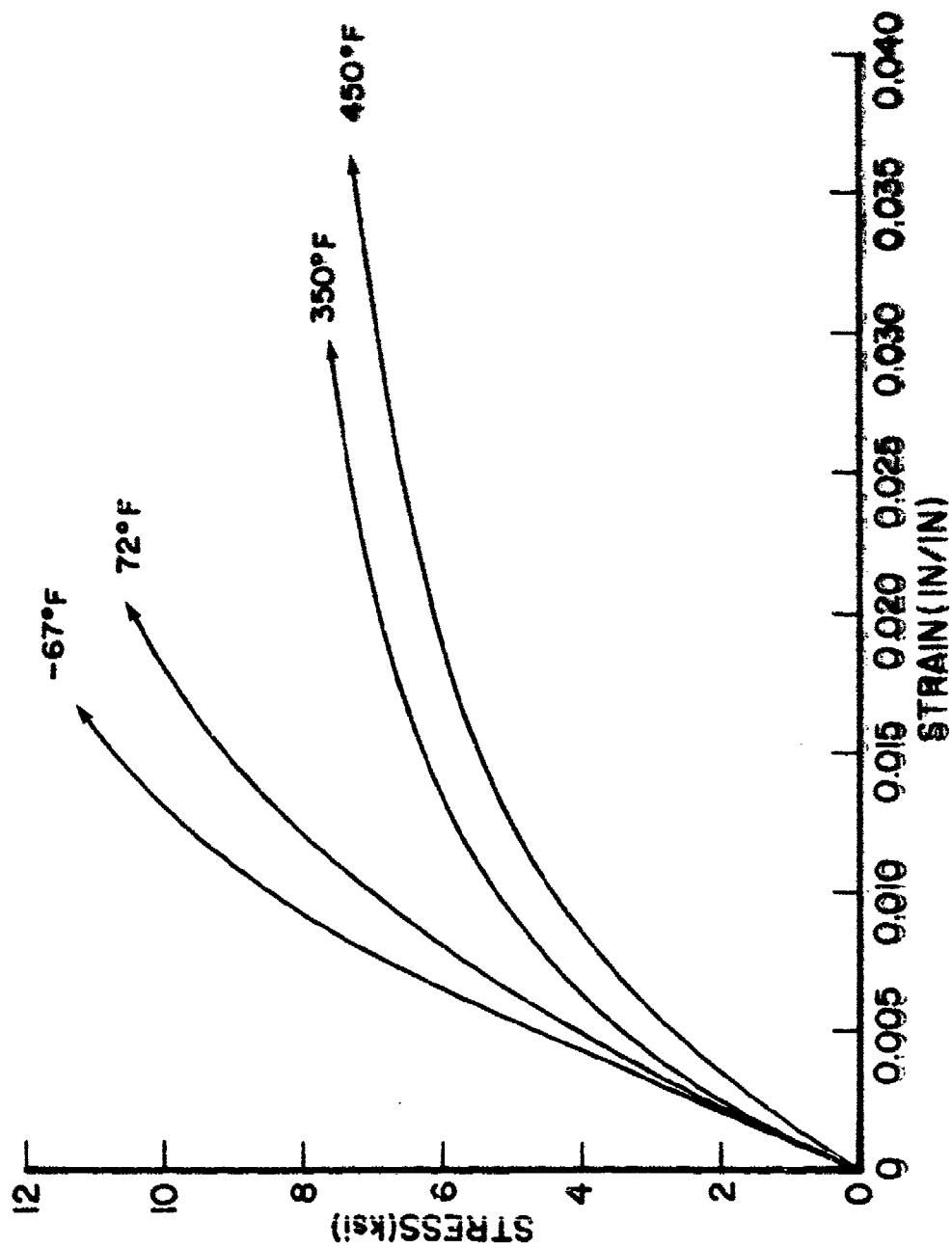


Figure 66. Inplane Shear Stress-Strain Curves for T300/V378A Composite Laminates.

TABLE 55

Specimens gained weight so rapidly that they were already saturated at first weighing (48 hrs). They were dried in a desiccator at 72° F and 0.5 R.H. for 116 hrs to reach the weight gain indicated.

Specimens had reached saturation long before this but were kept in humidity cabinet until test schedule permitted testing.

Three specimens tested after five minutes in 350°F oven, giving average strength of 20.95 ksi (144 MPa). Two

Three of the five specimens exhibited evidence of buckling.

Two of the five specimens exhibited evidence of buckling.

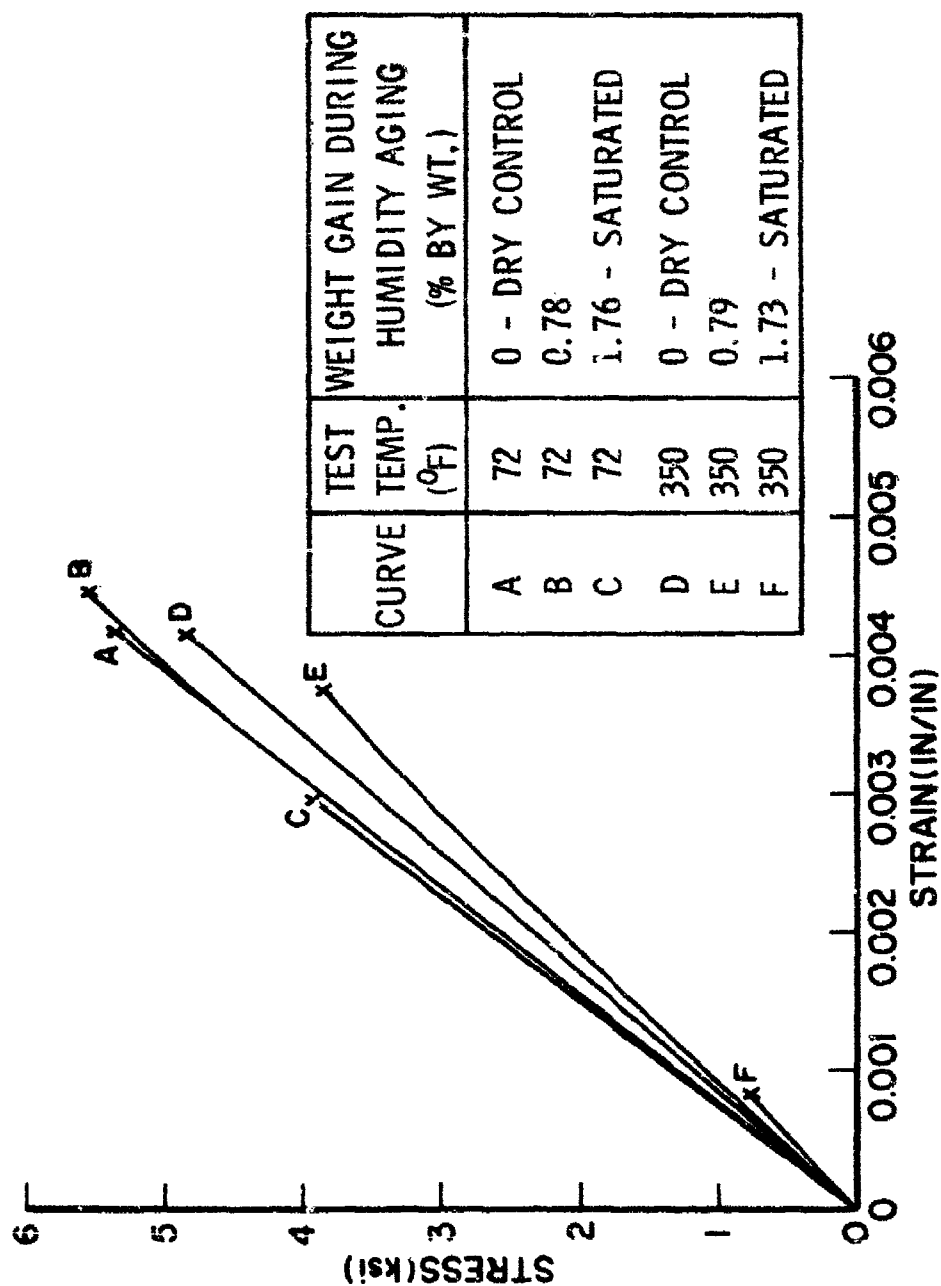


Figure 67. Tensile Stress-Strain Curves for Unidirectional T300/V378A Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

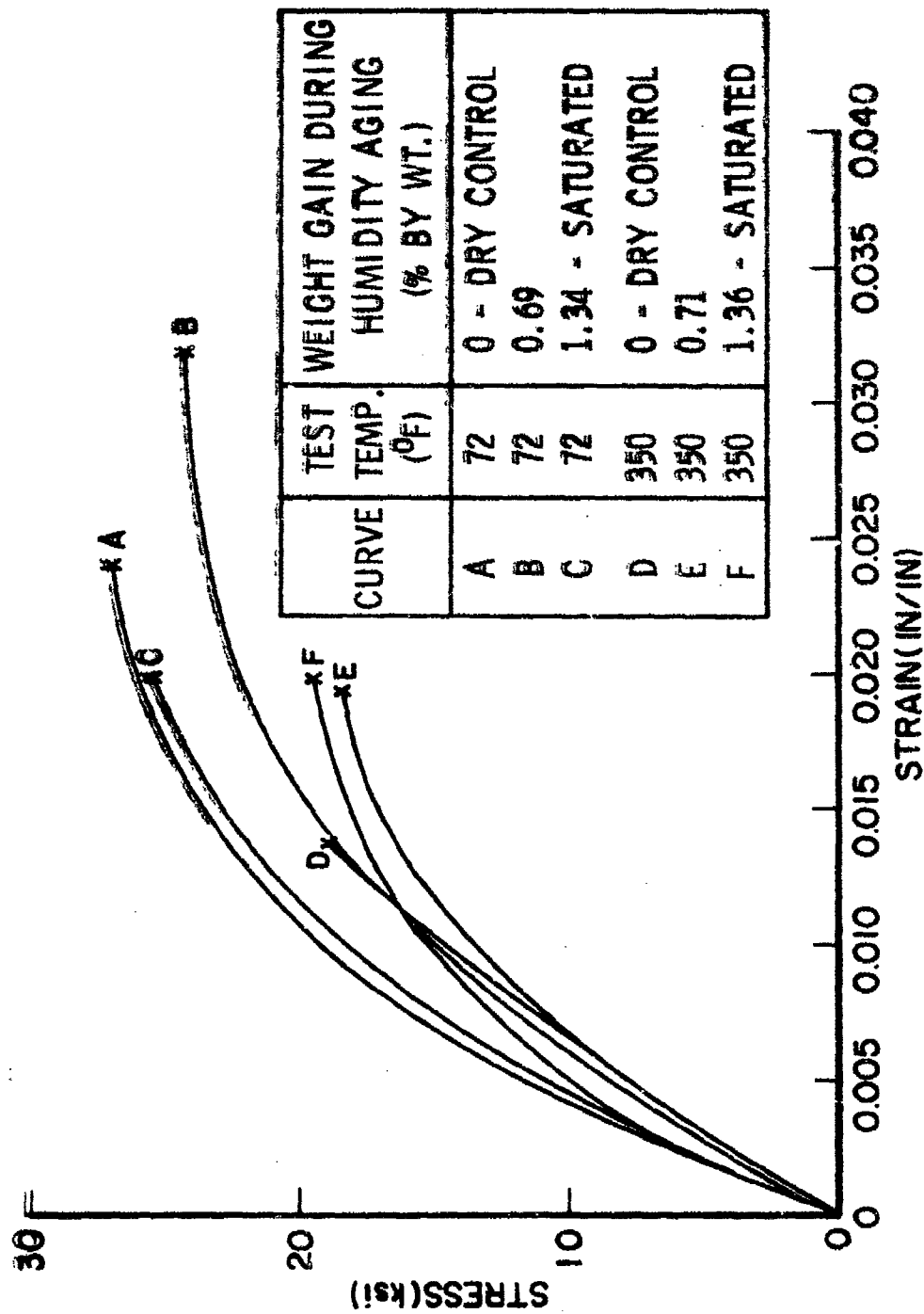


Figure 68. Compressive Stress-Strain Curves for Unidirectional T300/V378A Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

TABLE 56

CREEP PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties			
Material System - T300/V378		Prepared by - U.S. Polymeric	Gs/Polyviside
Fiber - T300		Matrix - V378	
Maximum Temperature Arming - 450°F (232°C)		Laminates Sp. Hr. - 1.58	
Resin Content - 26.0% by wt.		Nominal Ply Thickness - 0.0052 inch (0.13 mm)	
Fiber Content - 66.7% by vol.		No. of panels from which specimens were	
Void Content - 1.2% by vol.		tested in this table - 18	
Test Method - Straight-sided tension		Thickness of each type specimen:	
Reference - ASTM D2290 and D3039		0/45/90 - 20 ply	
		+45° - 8 ply	
CREEP			
Temperature		(0,+45,-45,0,0,-45,+45,0,90,0)°	+45°
72°F (22°C)	Stress Level [ksi] (MPa)	[101.8] (701)	[16.93] (117)
	Creep Strain, 500 hr(%)	0.0149	0.3575 @ 24 hrs ¹
	No. of Specimens	1	3
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	1 ⁴	2
	Stress Level [ksi] (MPa)	[95.2] (656)	[14.90] (103)
	Creep Strain, 500 hr(%)	0.0197	0.6011
	No. of Specimens	3	3
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	3	3
150°F (177°C)	Stress Level [ksi] (MPa)	[81.1] (559)	[12.77] (88)
	Creep Strain, 500 hr(%)	0.0149	0.3748
	No. of Specimens	3	3
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	3	2
	Stress Level [ksi] (MPa)	[84.9] (588)	[12.89] (89)
	Creep Strain, 500 hr(%)	0.0266	1.8756 ²
	No. of Specimens	2	2
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	2	3
250°F (232°C)	Stress Level [ksi] (MPa)	[76.1] (512)	[11.28] (78)
	Creep Strain, 500 hr(%)	0.0149	0.9708 ³
	No. of Specimens	3	2
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	3	3
	Stress Level [ksi] (MPa)	—	[9.67] (67)
	Creep Strain, 500 hr(%)	—	0.7073 ²
	No. of Specimens	—	2
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	—	3
450°F (232°C)	Stress Level [ksi] (MPa)	—	[11.95] (82)
	Creep Strain, 500 hr(%)	—	—
	No. of Specimens	—	—
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	—	—
	Stress Level [ksi] (MPa)	—	[10.45] (72)
	Creep Strain, 500 hr(%)	—	0.6713 ⁵
	No. of Specimens	—	1
	Residual Strength [ksi] (MPa)	—	—
	No. of Specimens	—	3

¹Strain gage failed on one specimen after 24 hrs., on another after 144 hrs. One specimen failed during test.

²Strain gage failed on one specimen during test.

³Strain gage failed on three specimens during test.

⁴Two specimens failed on loading.

⁵Strain gage failed on two specimens during test.

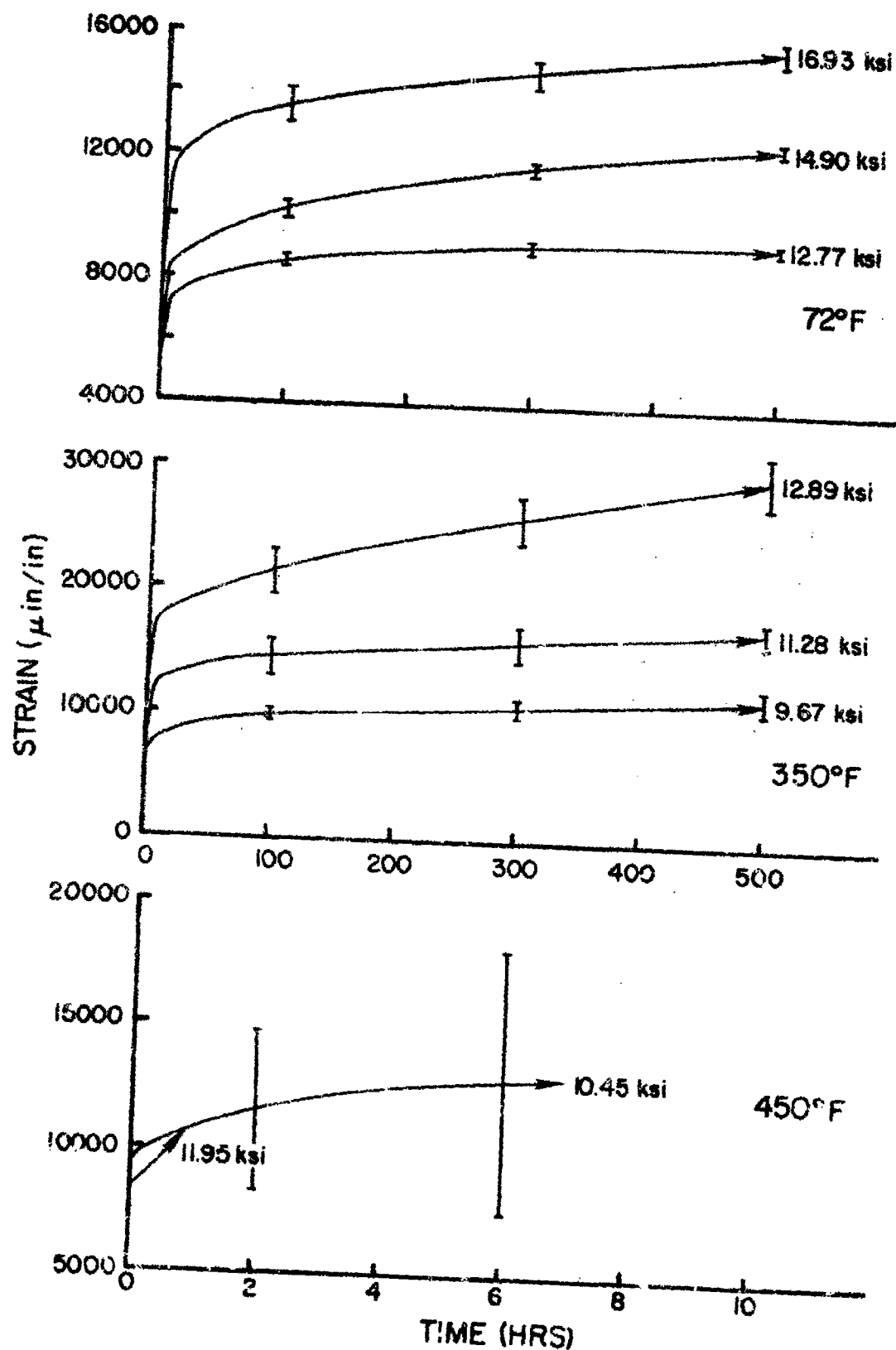


Figure 69. Tensile-Creep Behavior of Bidirectional T300/V378A Composite Laminates: $\pm 45^\circ$ Fiber Orientation.

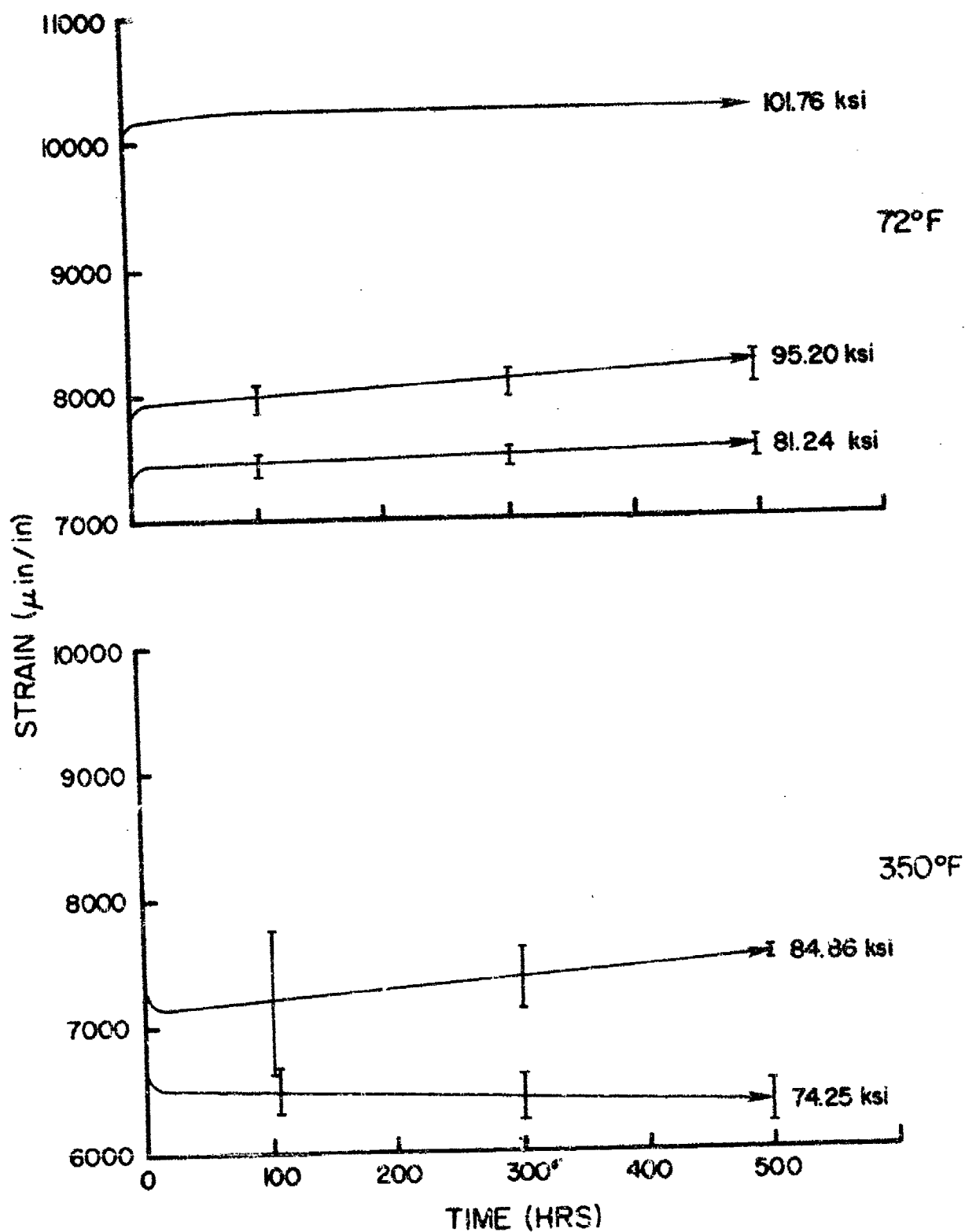


Figure 70. Tensile-Creep Behavior of T300/V378A Composite Laminates: $(0,+45,-45,0,0,-45,+45,0,90,0)_S$ Fiber Orientation.

TABLE 57
STRESS RUPTURE PROPERTIES OF T300/V378A
COMPOSITE LAMINATES

Composite Material Properties			
Material System - T300/V378A Fiber - T300 Matrix - V378A Maximum Temperature Rating - 450°F Resin Content - 26.0% by wt. Fiber Content - 66.8% by vol. Void Content - 1.2% by vol. Test Method - Straight-sided tension Reference - ASTM D2290 and D3039			Gr/Polyimide
Prepreg by - U.S. Polymeric Laminate Sp. Gr. - 1.58 Nominal Ply Thickness - 0.0052 inch (0.13 mm) No. of panels from which specimens were tested in this table - 16 Thickness of each type specimen: (0/+45/90) - 20 ply +45 - 8 ply			
STRESS RUPTURE			
Temperature	Fiber Orientation	(0,+45,-45,0,0,-45,+45,0,90,0) ₂	+45°
72°F (22°C)	Stress Level(ksi)(MPa)	[101.8] (701)	[16.93] (117)
	Time to Failure(hrs)	176 ¹	363 ²
	No. of Specimens	3	3
	Residual Strength(ksi)(MPa)	—	—
	No. of Specimens	1	2
	Stress Level(ksi)(MPa)	[95.2] (656)	[14.90] (103)
	Time to Failure(hrs)	503 ²	581 ^{2,3}
	No. of Specimens	3	3
	Residual Strength(ksi)(MPa)	—	—
	No. of Specimens	3	3
260°F (127°C)	Stress Level(ksi)(MPa)	[34.9] (585)	[12.89] (89)
	Time to Failure(hrs)	532 ²	502 ^{2,3}
	No. of Specimens	2	3
	Residual Strength(ksi)(MPa)	—	—
	No. of Specimens	2	3
	Stress Level(ksi)(MPa)	[74.3] (512)	[11.28] (78)
	Time to Failure(hrs)	507 ^{2,3}	527 ^{2,3}
	No. of Specimens	3	3
	Residual Strength(ksi)(MPa)	—	—
	No. of Specimens	3	3
350°F (177°C)	Stress Level(ksi)(MPa)		[11.95] (82)
	Time to Failure(hrs)		230
	No. of Specimens		3 ²
	Residual Strength(ksi)(MPa)		—
	No. of Specimens		1
	Stress Level(ksi)(MPa)		[10.45] (72)
	Time to Failure(hrs)		503 ^{2,3}
	No. of Specimens		3
	Residual Strength(ksi)(MPa)		—
	No. of Specimens		3

¹One specimen survived for 500 hours without failure.

²Two specimens survived for 500 hours without failure.

³Three specimens survived for 500 hours without failure.

TABLE 58
FATIGUE PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties				
Material System - T300/V378A		Prepreg by - U.S. Polymeric		Gr/Polyimide
Fiber - T300 Matrix - V378A		Laminata Sp. Gr. - 1.57		
Maximum Temperature Rating - 450°F(232°C)		Nominal Ply Thickness - 0.0052 inch(0.13 mm)		
Resin Content - 25.8% by wt.		No. of panels from which specimens were tested in this table - 15		
Fiber Content - 66.7% by vol.		Thickness of each type specimen:		
Void Content - 1.5% by vol.		+45 - 8 ply		
Test Method - Straight-sided tension		0/+45/90 - 20 ply		
Reference - ASTM D3039				
TENSILE FATIGUE, R=0.1 ⁽³⁾				
Temperature	Fiber Orientation	+45°	0/+45/90 ⁽¹⁾	0/+45/90 ^(1,2)
72°F(22°C)	Max. Stress[ksi](MPa)	[15.97] (110)	[95.8] (660)	
	Lifetime (cycles)	16,742	15,534	
	No. of Specimens	5	5	
	Residual Strength[ksi](MPa)	—	—	
	No. of Specimens	0	0	
	Max. Stress[ksi](MPa)	[14.90] (103)	[92.8] (639)	[83.8] (577)
	Lifetime (cycles)	68,856	255,077 ^(4,5)	61,300
	No. of Specimens	4	4	1
	Residual Strength[ksi](MPa)	—	—	—
	No. of Specimens	0	1	0
	Max. Stress[ksi](MPa)	[13.84] (95)	[89.8] (619)	[79.1] (545)
	Lifetime (cycles)	429,359	1,579,910 ⁽⁴⁾	467,807
	No. of Specimens	5	4	4
	Residual Strength[ksi](MPa)	—	—	—
	No. of Specimens	0	1	0
350°F (177°C)	Max. Stress[ksi](MPa)	[13.70] (94)	[90.1] (621)	
	Lifetime (cycles)	4,727	96,587	
	No. of Specimens	5	5	
	Residual Strength[ksi](MPa)	—	—	
	No. of Specimens	0	0	
	Max. Stress[ksi](MPa)	[12.90] (89)	[87.5] (603)	
	Lifetime (cycles)	52,012	323,176 ⁽⁶⁾	
	No. of Specimens	4	3	
	Residual Strength[ksi](MPa)	—	—	
	No. of Specimens	0	0	
	Max. Stress[ksi](MPa)	[12.09] (83)	[84.8] (584)	
	Lifetime (cycles)	347,393	531,563	
	No. of Specimens	5	5	
	Residual Strength[ksi](MPa)	—	—	
	No. of Specimens	0	0	

1. Stacking sequence (0,+45,-45,0,0,-45,+45,0,90,0).
2. These specimens had a 0.1935 inch (0.491 cm) hole in the center of the test section. Stresses calculated using net cross-sectional area.
3. Fatigue lifetimes are log mean values. All residual strengths determined by tensile test at 72°F (22°C).
4. One specimen ran out to 10⁷ cycles without failure.
5. One specimen broke at 3,169,500 cycles due to power outage.
6. One specimen failed at 2,128,300 cycles due to oven overheating.

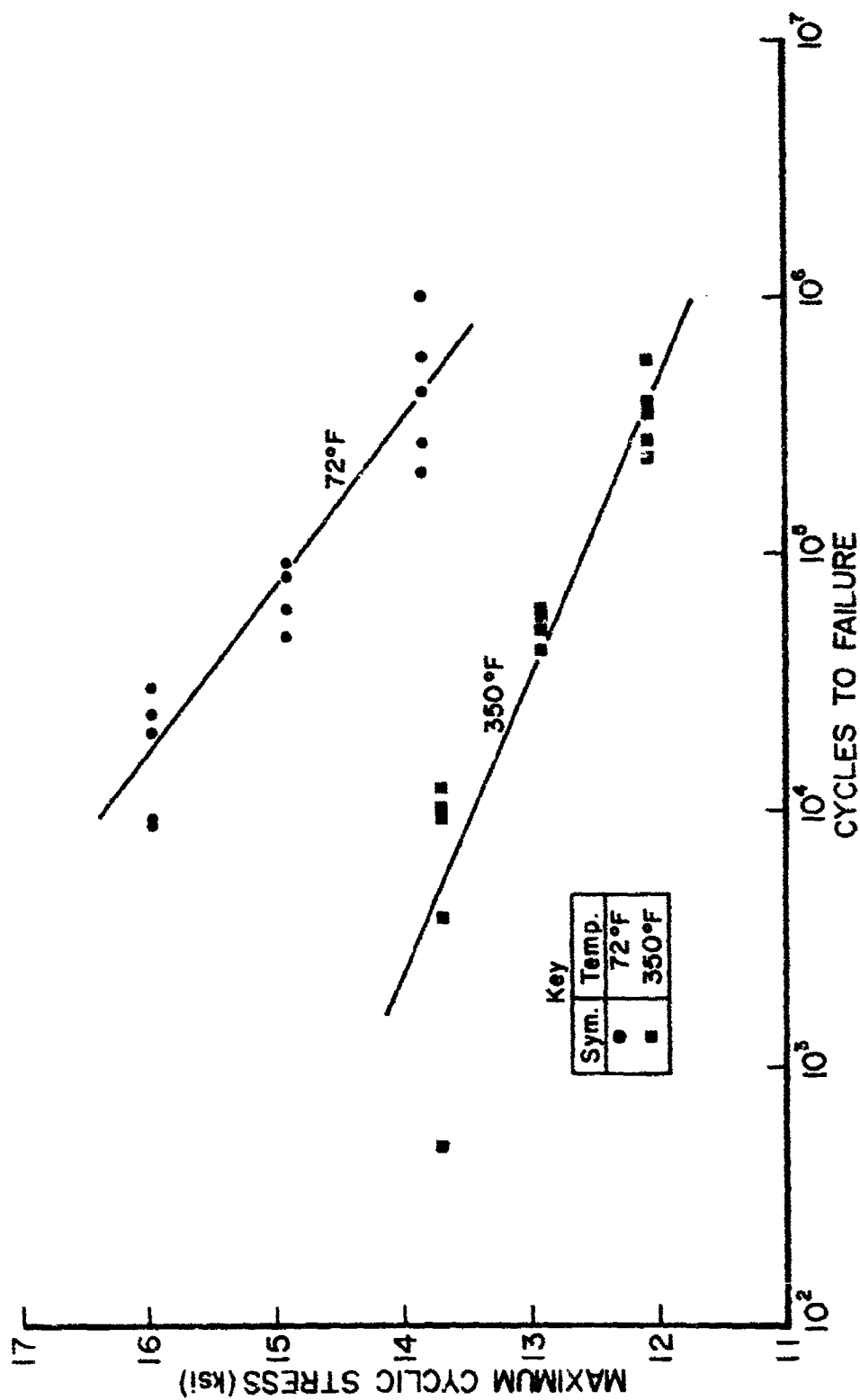


Figure 71. Tensile-Tensile Fatigue Behavior of T300/V378A Composite Laminates: +45° Fiber Orientation, $R = 0.10$, 10 Hz.

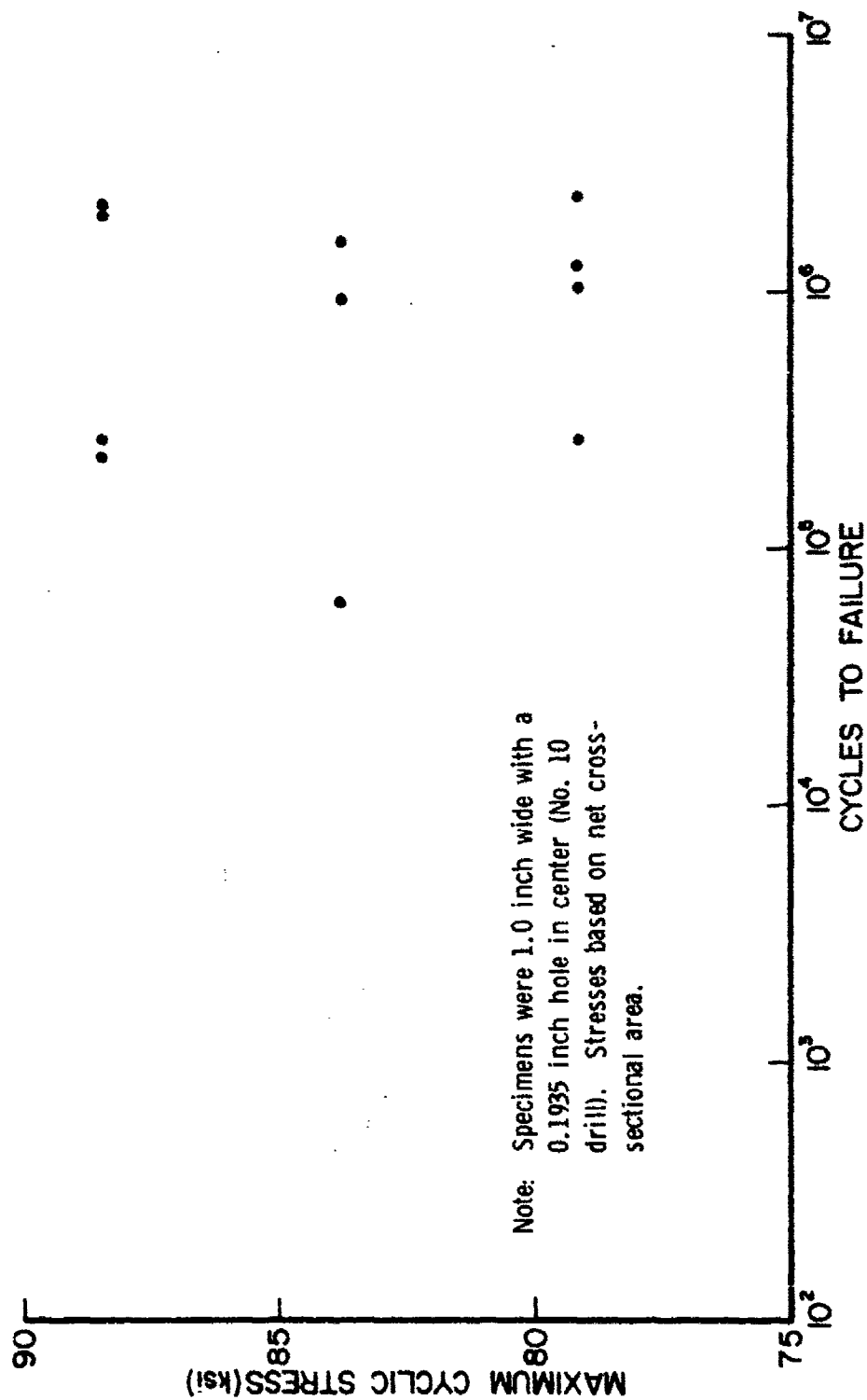


Figure 73. Tensile-Tensile Fatigue Behavior of T300/V378A Composite Laminates: (0,45,-45,0,0,-45,45,0,90,0)_s Fiber Orientation, R = 0.10, 10 Hz.

TABLE 59
THERMOPHYSICAL PROPERTIES OF T300/V378A COMPOSITE LAMINATES

Composite Material Properties					
Material System - T300/V378A		Prepreg by - U.S. Poly.		Gr/PI	
Fiber - T300	Matrix - V378A	Laminate Sp. Gr. - 1.57			
Maximum Temperature Rating - 450°F(232°C)		Average Ply Thickness - 0.0051 inch(0.13 mm)			
Resin Content - 24.6% by wt.		No. of panels from which specimens were tested in this table - 2			
Fiber Content - 67.2% by vol.					
Void Content - 2.0% by vol.					
Thickness of each type specimen: Therm. Exp. - 40 ply		Spec. Ht. - 1 ply			
Therm. Cond. - 40 ply		Glass Trans. - 8 ply			
THERMOPHYSICAL PROPERTIES: 0°					
	-67°F(-55°C)	72°F(22°C)	150°F(177°C)	450°F(232°C)	Test Method
Thermal Expansion ¹ α_x [in/in-°F] (μcm/cm-°C)	[0.12] (0.22)	[-0.15] (-0.27)	[-0.11] (-0.20)	[-0.14] (-0.25)	TMA ²
α_y [in/in-°F] (μcm/cm-°C)	[15.8] (28.4)	[17.3] (31.2)	[22.8] (41.1)	[23.7] (42.7)	
No. of Specimens per direction	3	3	3	3	
Specific Heat C_p [btu/lb.-°F] (J/kg-°C)	[0.123] (515)	[0.206] (862)	[0.748] (3132)	[0.761] (3186)	DSC ³
No. of Specimens	3	3	3	3	
Thermal Conductivity ¹ k_x [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.28] (0.50)	[0.34] (0.59)	[0.44] (0.77)	[0.47] (0.83)	
No. of Specimens	3	3	3	3	DMA ⁴
Glass Transition Temp. Dry [°F] (°C)	[702] (372)	[372]			
Wet [°F] (°C)	[702] (372) ⁵	[372]			
THERMOPHYSICAL PROPERTIES: +45°					
Thermal Expansion ¹ α_x [in/in-°F] (μcm/cm-°C)	[2.21] (3.98)	[1.65] (2.97)	[2.11] (3.79)	[2.06] (3.71)	TMA ²
No. of Specimens per direction	3	3	3	3	
Thermal Conductivity ¹ k_x [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.25] (0.44)	[0.29] (0.51)	[0.39] (0.67)	[0.42] (0.72)	Comparative
No. of Specimens	3	3	3	3	

NOTES: 1. On the unidirectionally reinforced specimens, the x-direction is along the fiber axis, the y-direction is across the fiber axis, and the z-direction is through the thickness (identical to the y-direction). On +45° bidirectionally reinforced specimens, the x and y directions are identical and oriented at 45° to either fiber direction, while the z-direction is through the thickness.

2. Thermo-Mechanical Analysis

3. Differential Scanning Calorimetry

4. Dynamic Mechanical Analysis

5. Gained wt. very rapidly. May have dried very rapidly also, so actual value was for dry material by end of test.

4.5 HyE 1076J

This system consists of 15,000 filament tow Thornel 300 from Union Carbide in Fiberite's 976 epoxy resin matrix.

Tables 60 through 74 present the data generated for this 350°F (177°C) graphite/epoxy composite material. Figures 74 through 89 illustrate the stress-strain, fatigue, and creep behavior of this material as well as the effects of humidity aging upon selected composite materials.

The 976 resin system was developed to retain higher property levels after humidity aging than earlier 350°F (177°C) epoxy systems. Two tables released by Fiberite are included at the end of this section which provides comparisons of the 934 and 976 systems.

TABLE 60
PROCESSING CONDITIONS FOR HyE 1076J
COMPOSITE LAMINATES

Composite Processing Information	
Material System - HyE 1076J	Gr/Ep
Fiber - T300/15K Matrix - 976	
Maximum Rated Temperature - 350°F (177°C)	Prepreg by - Fiberite
<p style="text-align: center;">Laminate Processing Schedule</p> <p><u>Layup Procedure:</u> The prepreg was stored in a closed wrapper at 0°F (-18°C). Prepreg was warmed to room temperature before removal from wrapper to prevent moisture condensation on prepreg. Plies were cut to desired size with razor knife and stacked in desired sequence (release paper removed from each ply). The stack was placed in the autoclave according to the layup system illustrated in Figure 74. The corprene edge dam serves to restrict fiber flow.</p> <p><u>Cure Schedule:</u> Apply full vacuum and hold for 1/2 hour at room temperature. Heat to 250°F (121°C) at a rate of 2-5°F/min. When temperature has reached 250°F (121°C) apply 100 psi above bladder (while retaining vacuum). Hold at 250°F (121°C) for 45 minutes then heat to 350°F (177°C) at a rate of 2-5°F/min. Hold at 350°F (177°C) for 2 hours then cool to 150°F (66°C) at 2-5°F/min. Release pressure when temperature has reached 150°F (66°C), then release vacuum and remove panel from autoclave.</p> <p><u>Postcure Schedule:</u> None.</p>	

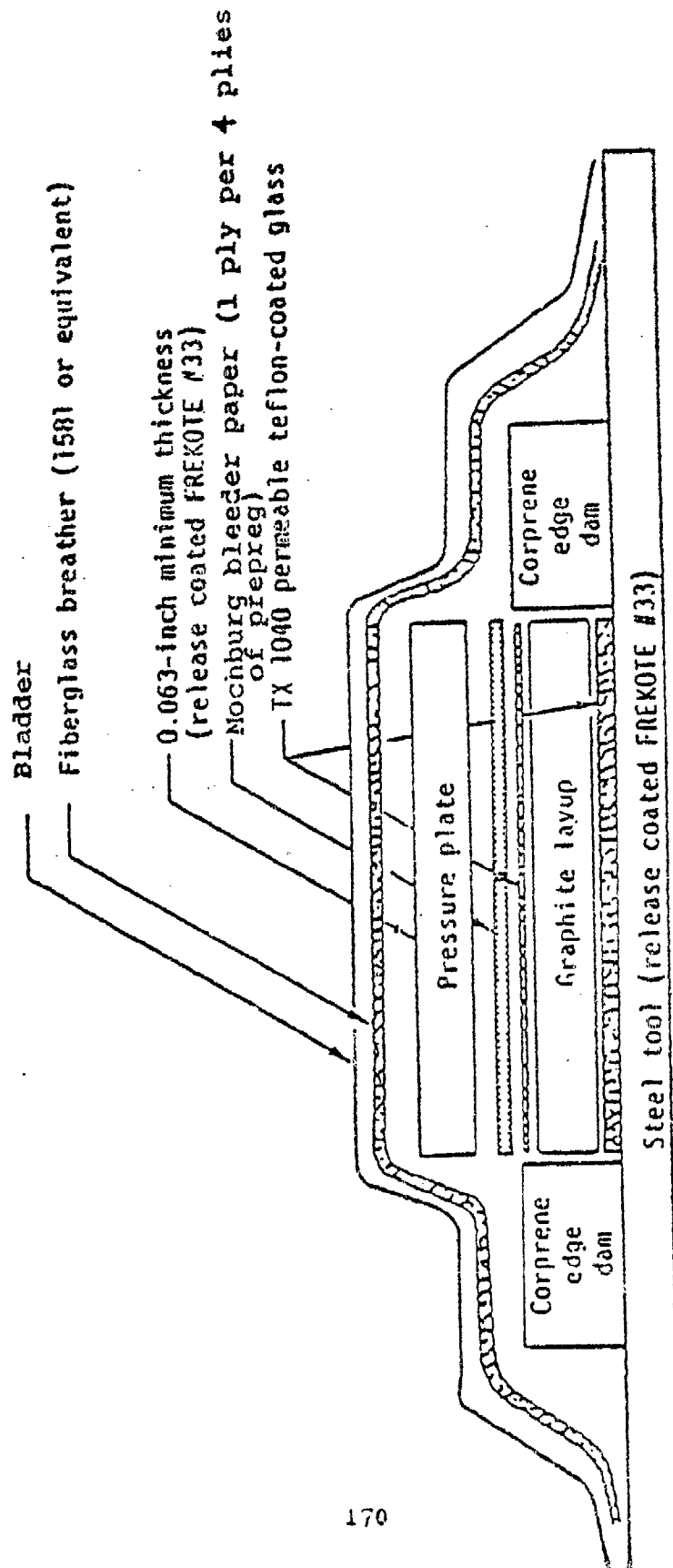


Figure 74. Layup System for HyE 1076J Laminates.

TABLE 61

PREPREG AND COMPOSITE PHYSICAL PROPERTIES

Composite Physical Property Information				
Material System - HyE 1076J Fiber - T300/15K Matrix - 976 Maximum Rated Temperature - 350°F(177°C)			Gr/Ep Prepreg by - Fiberite	
Prepreg Physical Properties				
(Property)	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
Volatile Content- 0.44% by wt.		0.23-0.57	QCI-C-V-14	Fiberite
Resin Content- 37.7% by wt.		37.5-37.8	R-15	Fiberite
Gel Time - 21.3 minutes		20.1-22.3	G2	Fiberite
No. of Rolls Involved- 1				
No. of Batches Involved- 1				
Laminate Physical Properties ¹				
	(Std.Dev.)	(Range)	(Test Method)	(Ref.)
No. of Panels- 34				
Fiber Content- 68.0% by vol.	1.5%	62.3-69.9%	Acid Digestion	
Resin Content- 25.6% by wt.	2.6%	23.8-37.7%	AFML-TR-67-243	
Void Content- ± 0% by vol.			D2734	ASTM
Laminate Sp. Gr.- 1.62			D792	ASTM
Fiber Sp. Gr.- 1.78		As reported by manufacturer.		
Matrix Sp. Gr.- 1.28		As reported by manufacturer.		
Thickness per ply-			---	---

¹ The properties reported here represent averages for all panels of this material used throughout the program.

512

928
182

HPLC ANALYSIS

SAMPLE (CONC.) HyE 1076J (0.1%) SAMPLE SIZE 25 μ l
 MOBILE PHASE 1 Water MOBILE PHASE 2 Dioxane
 FLOW RATE 1.0 ml/min PROGRAM Method 9
 COLUMNS Zorbax 905 DETECTOR Trace UV
 ATTENUATION 54 WAVE LENGTH 254
 CHART SPEED 0.5 in/min FULL SCALE (mV) 40
 DATE 5-1-81 OPERATOR B. Price

1235

1372

1442

1527

1575

1615

1775

1827

1865

1912

1965

2005

2038

2092

2102

2237

2305

2435

2488

2525

2567

2607

2637

2698

2735

2782

2822

2867

2912

2955

3000

3042

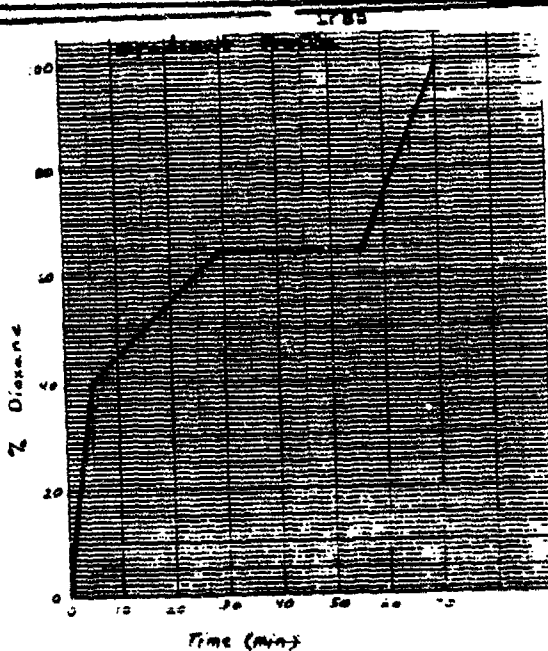


Figure 75. HPLC Analysis of HyE 1076J.

TABLE 62
TENSILE PROPERTIES OF Hye 1076J
COMPOSITE LAMINATES

Composite Material Properties				
Material System - Hye 1076J		Prepreg by - Fiberite		Gr/Ep
Fiber - T300/15K Matrix - 976		Laminate Sp. Gr. - 1.60/0; 1.64/90		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness-0.0053 in./0;0.0049 in./90		
Resin Content - 35.3%/0; 24.5%/90 by wt.		No. of panels from which specimens were tested		
Fiber Content - 58.6%/0; 69.4%/90 by vol.		in this table - 7		
Void Content - ± 0				
Thickness of each type specimen: 0° - 6 ply ; 90° - 15 ply				
TENSION: 0°				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F_x^{tu} [ksi] (MPa)	[196.8] (1356)	[207.1] (1427)	[232.3] (1601)	[228.4] (1573)
Std.Dev. [ksi] (MPa)	[15.1] (104)	[13.4] (92)	[15.9] (110)	[8.6] (59)
Range [ksi] (MPa)	[172.5 - 213.5] (1189 - 1471)	[190.8 - 219.4] (1315 - 1512)	[211.5 - 254.7] (1457 - 1755)	[218.7 - 242.2] (1507 - 1669)
No. of Specimens	5	5	5	5
F_x^{tpl} [ksi] (MPa)	[196.8] (1356)	[207.1] (1427)	[232.3] (1601)	[228.4] (1573)
Std.Dev. [ksi] (MPa)	[15.1] (104)	[13.4] (92)	[15.9] (110)	[8.6] (59)
No. of Specimens	5	5	5	5
E_x^t [Msi] (GPa)	[20.4] (141)	[19.3] (133)	[22.4] (154)	[22.1] (152)
Std.Dev. [Msi] (GPa)	[0.5] (3)	[1.0] (7)	[0.5] (3)	[1.4] (10)
No. of Specimens	5	5	5	5
ϵ_x^{tu} [μ in/in] (μ cm/cm)	8,600	10,420	9,900	9,930
Std.Dev.	450	360	440	530
No. of Specimens	3	5	5	4
ν_{xy}^t	0.32	0.32	0.31	0.35
Std. Dev.	0.02	0.02	0.03	0.03
No. of Specimens	5	5	5	5
Test Method	Straight-sided tension			
Reference	ASTM D3039			
TENSION: 90°				
F_y^{tu} [ksi] (MPa)	[4.73] (33)	[5.66] (39)	[3.81] (26)	[3.47] (24)
Std.Dev. [ksi] (MPa)	[1.19] (8)	[0.87] (6)	[0.66] (5)	[0.46] (3)
Range	[3.23 - 6.29] (22 - 43)	[4.53 - 6.52] (31 - 45)	[2.87 - 4.68] (20 - 32)	[2.67 - 3.83] (18 - 26)
No. of Specimens	5	5	5	5
F_y^{tpl} [ksi] (MPa)	[4.73] (154)	[5.66] (39)	[3.81] (26)	[3.47] (24)
Std.Dev. [ksi] (MPa)	[1.19] (8)	[0.87] (6)	[0.66] (5)	[0.46] (3)
No. of Specimens	5	5	5	5
E_y^t [Msi] (GPa)	[1.69] (12)	[1.34] (9)	[1.37] (9)	[1.30] (9)
Std.Dev. [Msi] (GPa)	[0.2] (1)	[0.04] (0.3)	[0.1] (1)	[0.08] (0.6)
No. of Specimens	5	5	5	5
ϵ_y^{tu} [μ in/in] (μ cm/cm)	2,760	3,900	2,640	2,620
Std. Dev.	560	570	500	350
No. of Specimens	5	5	5	5
ν_{yx}^t	0.026 ¹	0.022 ¹	0.019 ¹	0.020 ¹
Std. Dev.	---	---	---	---
No. of Specimens	---	---	---	---
Test Method	Straight-sided tension			
Reference	ASTM D3039			

¹Computed using elastic moduli and longitudinal Poisson's ratio.

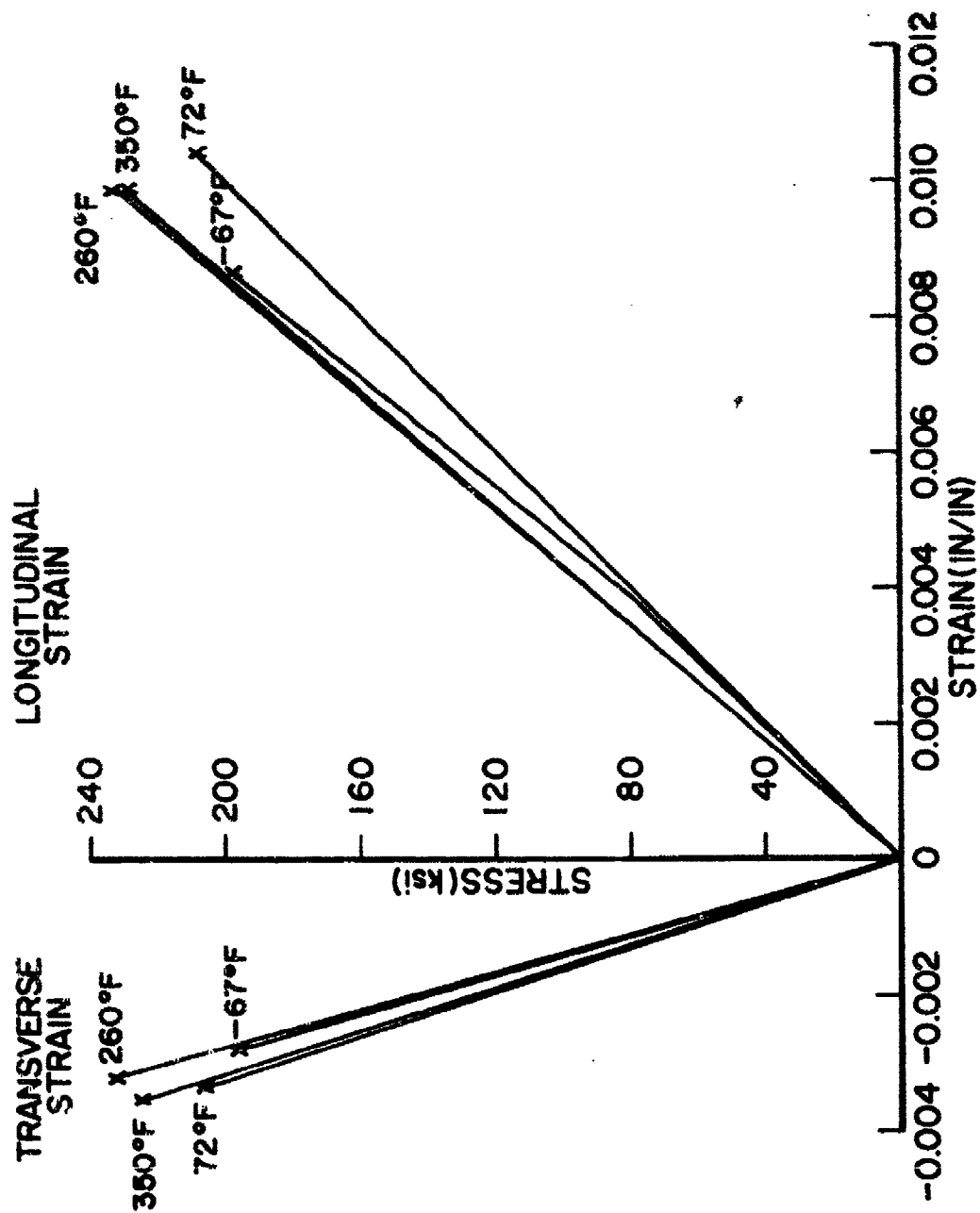


Figure 76. Tensile Stress-Strain Curves for Unidirectional HyE 1076J Composite
Laminates: 0° Fiber Orientation.

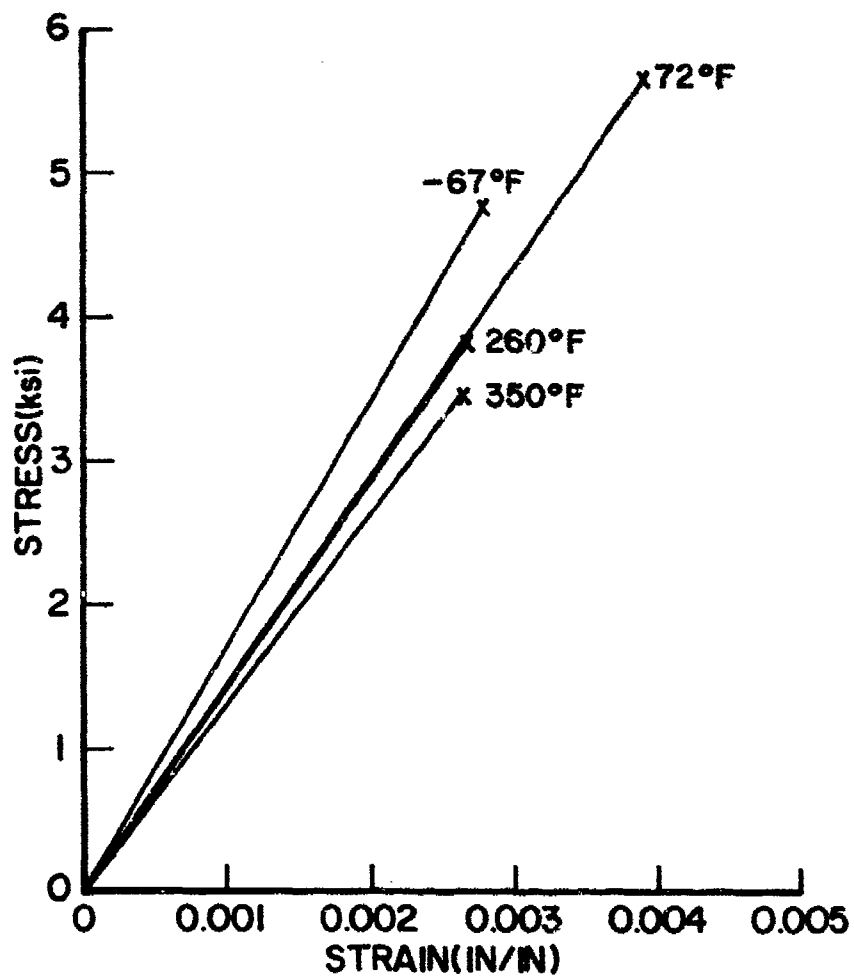


Figure 77. Tensile Stress-Strain Curves for Unidirectional HyE 1076J Composite Laminates: 90° Fiber Orientation.

TABLE 63
TENSILE PROPERTIES OF HyE 1076J
COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyZ 1076J		Prepreg by - Fiberite		Gr/Ep
Fiber - T300/15K Matrix - 976		Laminate Sp. Gr. - 1.62		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0053 inch(0.13 mm)		
Resin Content - 25.3% by wt.		No. of panels from which specimens were tested		
Fiber Content - 67.9% by vol.		in this table - 10		
Void Content - 0.2% by vol.		Thickness of specimen - 8 ply		
TENSION: +45°				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F_x^{TU} [ksi] (MPa)	[27.49] (189)	[22.28] (154)	[16.49] (114)	[16.60] (114)
Std.Dev. [ksi] (MPa)	[1.92] (13)	[0.28] (2)	[0.79] (5)	[1.29] (9)
Range [ksi] (MPa)	[26.40 - 30.92] (182 - 213)	[22.0 - 22.73] (152 - 157)	[15.55 - 17.44] (107 - 120)	[15.33 - 18.71] (106 - 129)
No. of Specimens	5	5	5	5
F_x^{TF} [ksi] (MPa)	[13.61] (94)	[6.42] (44)	[4.36] (30)	[4.21] (29)
Std.Dev. [ksi] (MPa)	[3.62] (25)	[1.85] (13)	[0.51] (4)	[0.57] (4)
No. of Specimens	5	5	5	5
E_x^T [ksi] (GPa)	[3.16] (22)	[3.08] (21)	[3.09] (21)	[2.68] (18)
Std.Dev. [ksi] (GPa)	[0.14] (1)	[0.10] (1)	[0.2] (1)	[0.17] (1)
No. of Specimens	5	5	5	5
ϵ_x^{TU} (in/in) (mm/cm)	11,120	11,670	18,880	34,400
Std. Dev.	2,380	1,270	8,820	1,390
No. of Specimens	5	3 ¹	5	2 ²
ν_{xy}^T	0.67	0.67	0.72	0.71
Std. Dev.	0.05	0.03	0.05	0.04
No. of Specimens	5	5	5	5
Test Method	ASTM D3039			
Reference				

¹Strain gages failed on two specimens prior to fracture.

²Strain gages failed on three specimens prior to fracture.

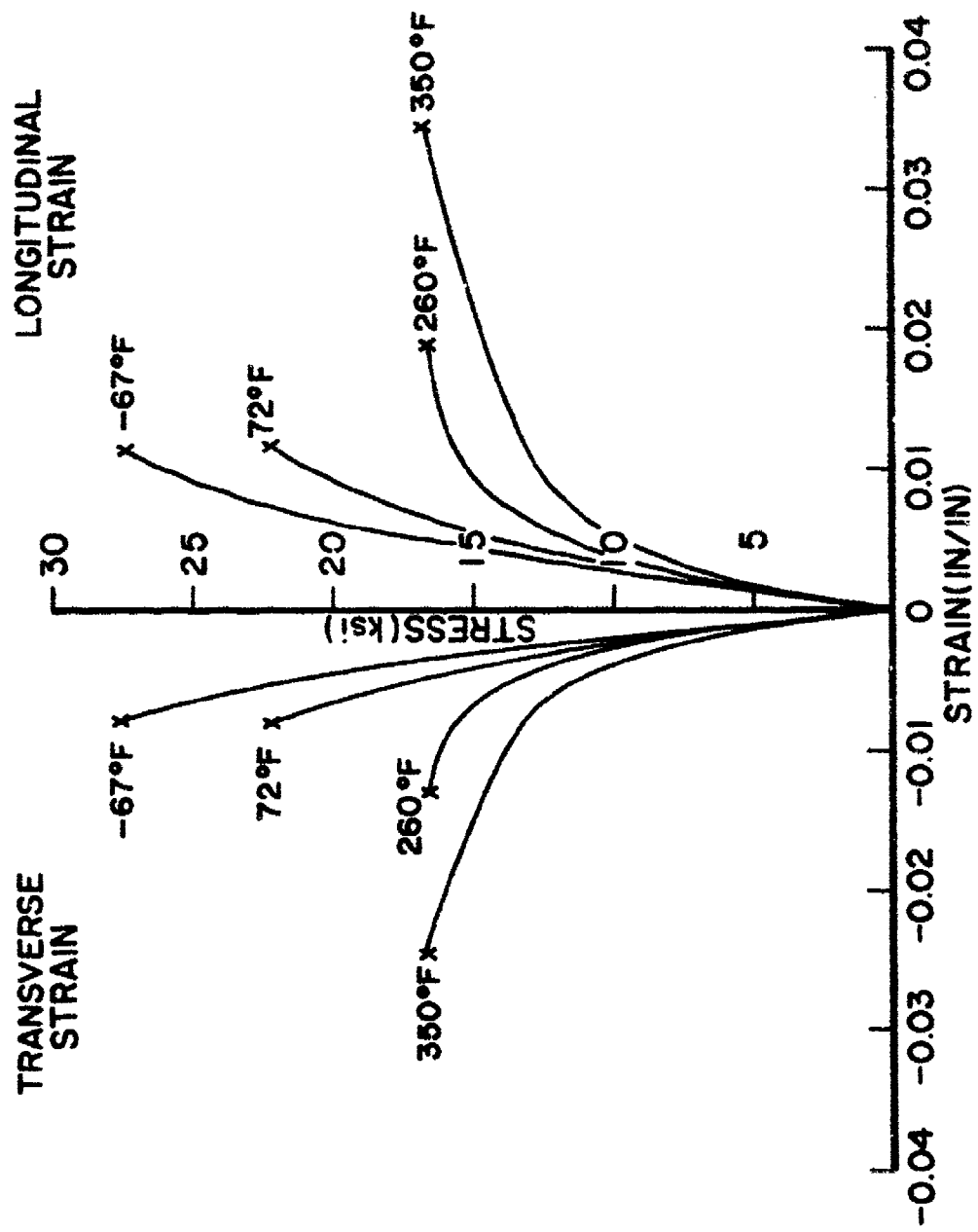


Figure 78. Tensile Stress-Strain Curves for Bidirectional HyE 1076J Composite
 Laminates: +45° Fiber Orientation.

TABLE 64
TENSILE PROPERTIES OF HyE 1076J
COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 1076J		Prepreg by - Fiberite	Gr/Ep	
Fiber - T300/15K Matrix - 976		Laminata Sp. Gr. - 1.62		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0050 inch (0.13 mm)		
Resin Content - 25.4% by wt.		No. of panels from which specimens were tested in this table - 11		
Fiber Content - 68.4% by vol.				
Void Content - 0.3% by vol.				
Thickness of each type specimen: 20 ply				
TENSION: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0)°				
	-67°F(-55°C)	72°F(22°C)	280°F(127°C)	350°F(177°C)
E_x^{cu} [ksi](MPa)		[116.8] (805)	[120.1] (827)	[118.1] (814)
Stand.Dev. [ksi](MPa)		(7.9) (54)	(5.9) (41)	(6.6) (45)
Range [ksi](MPa)		[108.9 - 128.1] (750 - 883)	[116.2 - 127.0] (801 - 875)	[109.3 - 126.3] (753 - 870)
No. of Specimens		5	5	5
E_x^{tpl} [ksi](MPa)		[116.8] (805)	[120.1] (827)	[118.1] (814)
Stand.Dev. [ksi](MPa)		(7.9) (54)	(5.9) (41)	(6.6) (45)
No. of Specimens		5	5	5
E_x^c [ksi](GPa)		[11.2] (77)	[12.2] (84)	[11.9] (82)
Stand.Dev. [ksi](GPa)		(0.5) (3)	(0.7) (5)	(0.8) (6)
No. of Specimens		5	5	5
ν_x^{cu} [in/in](mm/mm)		10.620	9.780	9.900
Stand.Dev.		550	630	430
No. of Specimens		5	5	4 ¹
ν_{xy}^c		0.37	0.40	0.36
Stand. Dev.		0.01	0.03	0.04
No. of Specimens		5	5	5
Test Method	ASTM D3039			
Reference				
TENSION: (0, +45, -45, 0, 0, -45, +45, 0, 90, 0)°, with 0.1935 inch (0.491 cm) hole				
E_y^{cu} [ksi](MPa)		[88.5] (610)		
Stand.Dev. [ksi](MPa)		(8.0) (55)		
Range		[78.6 - 99.1] (542 - 683)		
No. of Specimens		5		
E_y^{tpl} [ksi](MPa)				
Stand.Dev. [ksi](MPa)				
No. of Specimens				
E_y^c [ksi](GPa)				
Stand.Dev. [ksi](GPa)				
No. of Specimens				
ν_y^{cu} [in/in](mm/mm)				
Stand. Dev.				
No. of Specimens				
ν_{yx}^c				
Stand. Dev.				
No. of Specimens				
Test Method	ASTM D3039			
Reference				

¹Case failed on one specimen prior to end of test.

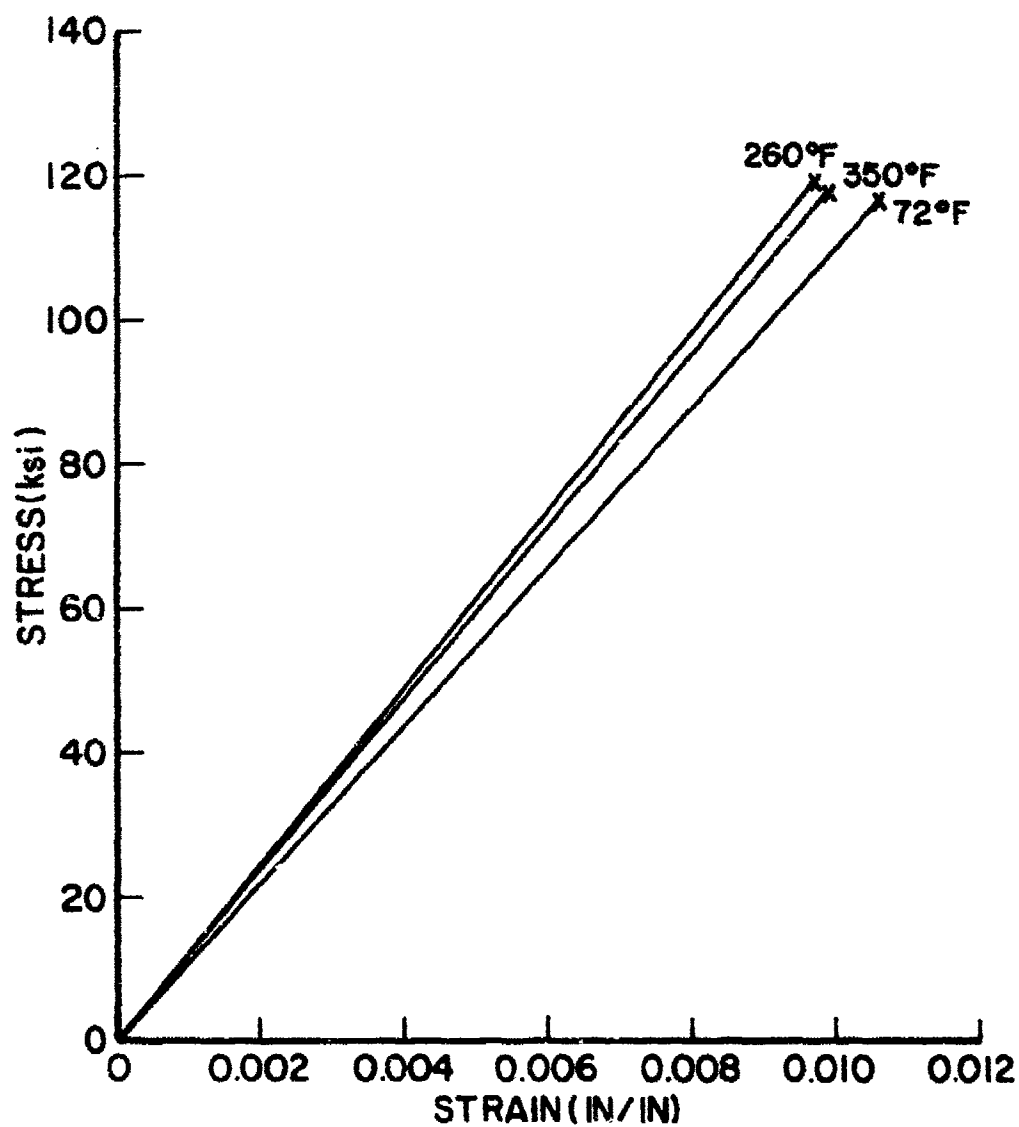


Figure 79. Tensile Stress-Strain Curves for Multidirectional HyE 1076J Composite Laminates: (0,45-45,0,0,-45,45,0,90,0)_s Fiber Orientation.

TABLE 65
COMPRESSIVE PROPERTIES OF Hye 1076J
COMPOSITE LAMINATES

Composite Material Properties

Material System - HyE 1076J

Fiber - T300/15K Matrix - 976

Maximum Rated Temperature - 350°F(177°C)

Resin Content - 24.3% by wt.

Fiber Content - 69.5% by vol.

Void Content - ~ 0% by vol.

Thickness of each type specimen: 0° - 20 ply ; 90° - 20 ply

Prepreg by - Fiberite

Gr/Epoxy

Laminate Sp. Gr. - 1.63

Nominal Ply Thickness - 0.0050 inch(0.13 mm)

No. of panels from which specimens were tested in this table - 2

COMPRESSION: 0°

	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
σ_x^{cu} [ksi](MPa)	[223.4] (1539)	[218.2] (1503)	[170.9] (1178)	[158.5] (1092)
Std.Dev.[ksi](MPa)	[21.8] (150)	[34.7] (239)	[37.1] (256)	[29.3] (202)
Range [ksi](MPa)	[195.7 - 253.5] (1348 - 1747)	[161.9 - 248.1] (1115 - 1709)	[111.1 - 205.1] (765 - 1413)	[124.2 - 185.6] (856 - 1279)
No. of Specimens	5	5	5	5
σ_x^{cpl} [ksi](MPa)	[63.8] (440)	[116.7] (804)	[62.9] (433)	[86.4] (595)
Std.Dev.[ksi](MPa)	[20.0] (138)	[88.9] (613)	[30.0] (207)	[34.6] (238)
No. of Specimens	5	5	5	5
E_x^c [ksi](GPa)	[21.9] (151)	[21.8] (150)	[21.4] (147)	[22.9] (158)
Std.Dev.[ksi](GPa)	[4.4] (30)	[2.9] (20)	[5.7] (39)	[3.0] (21)
No. of Specimens	5	5	5	5
ϵ_x^{cu} [in/in]($\mu\text{cm/cm}$)	14,500 ^{+1,2}	12,500 ^{+1,3}	8,900 ^{+1,3}	9,400
Std. Dev.	4,600	4,000	2,700	3,700
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3410			

COMPRESSION: 90°

σ_y^{cu} [ksi](MPa)	[35.1] (242)	[30.8] (212)	[22.6] (156)	[19.1] (132)
Std.Dev.[ksi](MPa)	[6.6] (45)	[1.3] (9)	[2.4] (17)	[2.2] (15)
Range	[26.7-44.9] (184 - 309)	[26.7-31.9] (184 - 220)	[19.4-25.7] (134 - 177)	[17.3-22.8] (119 - 157)
No. of Specimens	5	5	5	5
σ_y^{cpl} [ksi](MPa)	[9.9] (68)	[11.0] (76)	[4.5] (31)	[7.1] (49)
Std.Dev.[ksi](MPa)	[3.9] (27)	[1.9] (13)	[1.0] (7)	[3.7] (25)
No. of Specimens	5	5	5	5
E_y^c [ksi](GPa)	[1.84] (13)	[1.46] (10)	[1.84] (13)	[2.64] (11)
Std.Dev.[ksi](GPa)	[0.31] (2)	[0.19] (1)	[0.68] (4)	[0.32] (2)
No. of Specimens	5	5	5	5
ϵ_y^{cu} [in/in]($\mu\text{cm/cm}$)	22,100 ^{+1,4}	32,300 ^{+1,4}	17,600	14,200 ^{+1,2}
Std. Dev.	6,400	14,400	---	6,700
No. of Specimens	5	5	2	5
Test Method Reference	ASTM D3410			

¹ Ultimate strain value represents maximum observed strain rather than ultimate values.

² Three of five specimens exhibited evidence of buckling.

³ Two of five specimens exhibited evidence of buckling.

⁴ One of five specimens exhibited evidence of buckling.

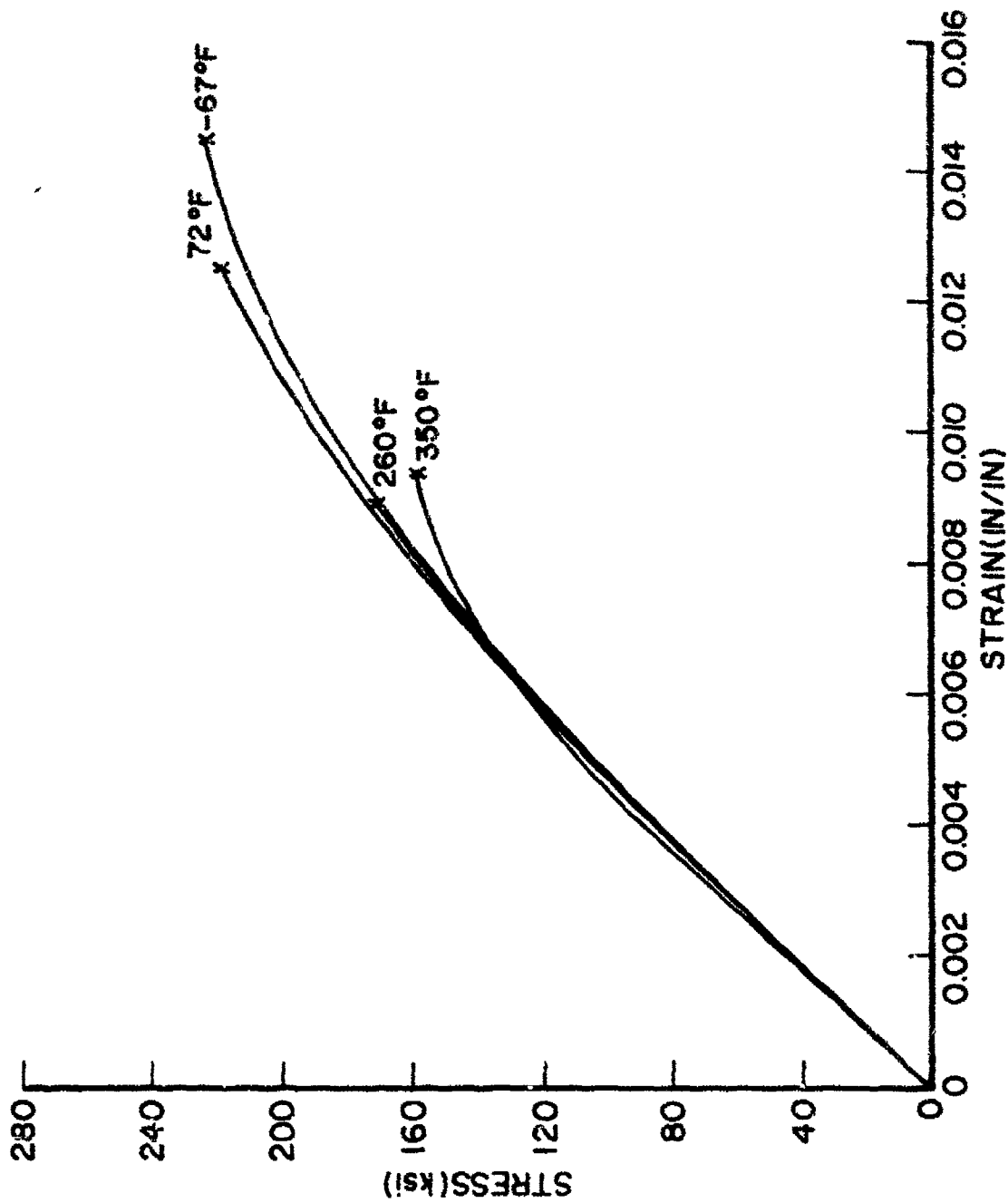


Figure 80. Compressive Stress-Strain Curves for Unidirectional HyE 1076J Composite
Laminates: 0° Fiber Orientation.

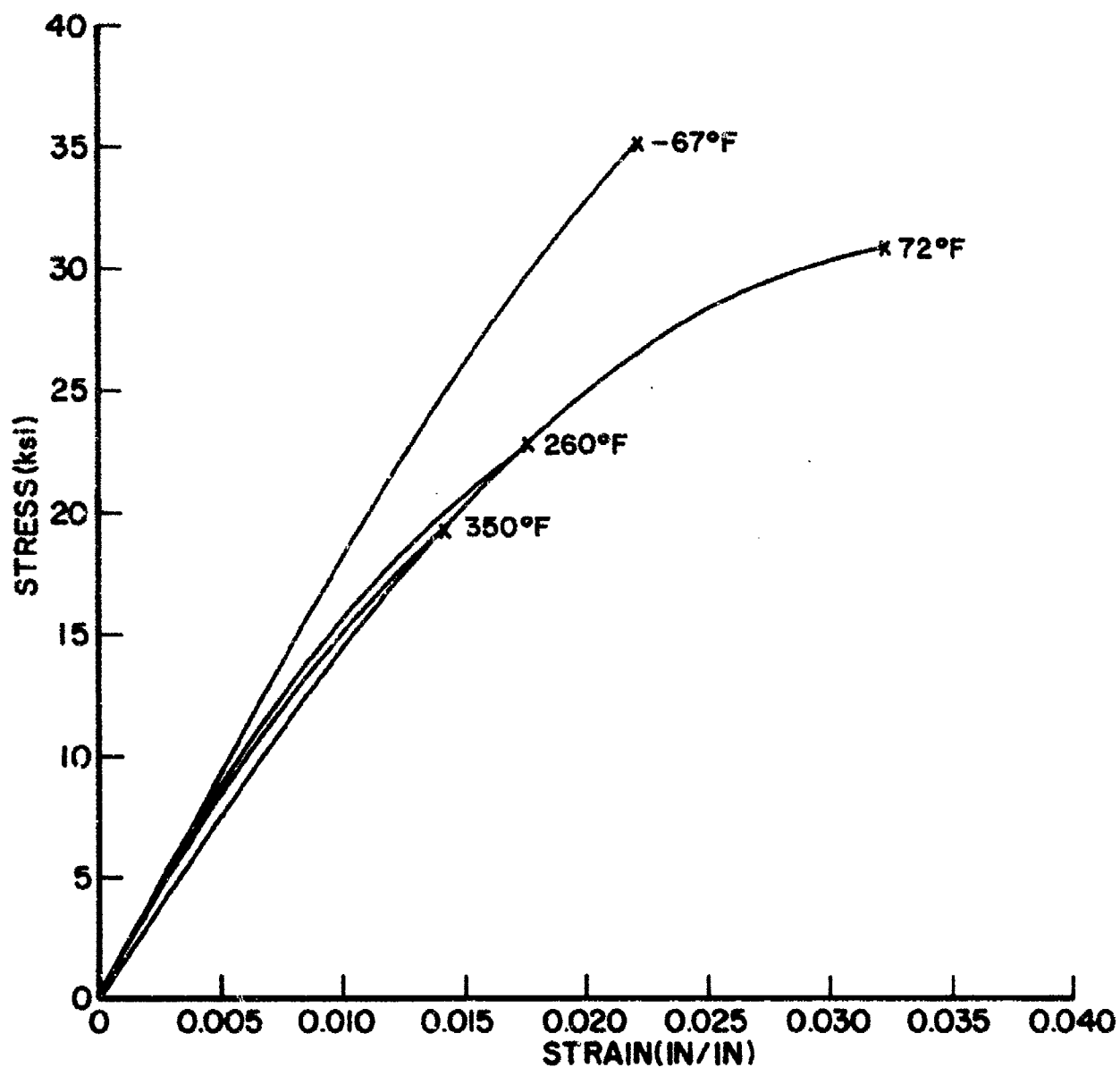


Figure 31. Compressive Stress-Strain Curves for Unidirectional HyE 1076J Composite Laminates: 90° Fiber Orientation.

TABLE 66
FLEXURAL PROPERTIES OF HYE 1076J
COMPOSITE LAMINATES

Composite Material Properties				
Material System - RYE 1076J		Prepreg by - Fibarite		Gr/Ep
Fiber - T300/15K		Matrix - 976		
Maximum Rated Temperature - 350°F(177°C)		Laminate Sp. Gr. - 1.62		
Resin Content - 25.1% by wt.		Nominal Ply Thickness - 0.0050 inch (0.13 mm)		
Fiber Content - 58.0% by vol.		No. of panels from which specimens were tested		
Void Content - 0.6% by vol.		in this table - 2		
Thickness of each type specimen: 0° - 14 ply ; 90° - 14 ply				
FLEXURE: 0°				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F_x^{fu} [ksi](MPa)	[261.9] (1804)	[190.1] (1310) ¹	[156.8] (1080) ²	[135.9] (1281) ³
Std.Dev. [ksi](MPa)	[13.9] (96)	[3.6] (25)	[11.5] (79)	[8.2] (56)
Range [ksi](MPa)	[239.3 - 276.3] (1649 - 1904)	[186.3 - 195.8] (1284 - 1349)	[148.1 - 176.2] (1020 - 1214)	[176.0 - 197.4] (1226 - 1360)
No. of Specimens	5	5	5	4
E_x^f [Msi](GPa)	[18.6] (1.28)	[14.9] (103)	[13.1] (90)	[18.3] (126)
Std.Dev. [Msi](GPa)	[0.7] (5)	[0.7] (5)	[0.8] (6)	[1.1] (8)
No. of Specimens	5	5	5	4
Test Method	3 pt. flex.	4 pt. flex.	4 pt. flex.	3 pt. flex.
Reference	Advanced Composite Design Guide; Jan. 1971 ⁴			
FLEXURE: 90°				
F_y^{fu} [ksi](MPa)	[10.31] (71)	[8.79] (60)	[7.42] (51)	[7.03] (48)
Std.Dev. [ksi](MPa)	[1.52] (10)	[2.19] (8)	[1.37] (9)	[1.16] (8)
Range [ksi](MPa)	[8.34 - 11.78] (57 - 81)	[7.38 - 10.66] (51 - 73)	[5.85 - 9.06] (40 - 62)	[5.86 - 8.66] (40 - 60)
No. of Specimens	5	5	5	5
E_y^f [Msi](GPa)	[1.84] (13)	[1.71] (81)	[1.62] (11)	[1.45] (10)
Std.Dev. [Msi](GPa)	[0.21] (1)	[0.16] (1)	[0.10] (1)	[0.17] (1)
No. of Specimens	5	5	5	5
Test Method	4 pt. flexure			
Reference	Advanced Composite Design Guide; Jan. 1971 ⁴			

¹All failures in tension on lower surface.

²All specimens exhibit compressive failure on upper surface.

³All specimens exhibit compressive failure on upper surface. One specimen tested in 4 pt. flexure failed in shear at a load corresponding to a flexural stress of 145.7 ksi (1004 MPa).

⁴This procedure corresponds to ASTM D790 except for loading speed and, in the case of the 4 pt. test, the position of the upper loading points.

TABLE 67
SHEAR PROPERTIES OF HyE 1076J
COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 1076J		Prepared by - Fiberite		Gr/Ep
Fiber - T300/15K Matrix - 976		Laminate Sp. Gr. - 1.63		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0052 inch (0.13 mm)		
Resin Content - 24.7% by wt.		No. of panels from which specimens were tested in this table - 11		
Fiber Content - 68.8% by vol.				
Void Content - ±0.1% by vol.				
Thickness of each type specimen - Inplane - 8 ply ; Interlaminar - 15 ply				
INPLANE SHEAR				
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)
τ_{xy} [ksi] (MPa)	[13.75] (95)	[11.14] (77)	[8.25] (57)	[8.30] (57)
Std.Dev. [ksi] (MPa)	[0.96] (7)	[0.14] (1)	[0.39] (3)	[0.65] (4)
Range [ksi] (MPa)	[13.20 - 15.46] (91 - 107)	[11.08-11.36] (76-78)	[7.78 - 8.72] (54 - 60)	[7.67 - 9.36] (53-64)
No. of Specimens	5	5	5	5
G_{xy}^s [ksi] (GPa)	[1.00] (7)	[0.92] (6)	[0.89] (6)	[0.77] (5)
Std.Dev. [ksi] (GPa)	[0.07] (1)	[0.05] (1)	[0.05] (1)	[0.06] (1)
No. of Specimens	5	5	5	5
Test Method	+45° straight-sided tension			
Reference	J. Comp. Mtls. (Vol. 6, p. 252 & Vol. 7, p. 124)			
INTERLAMINAR SHEAR				
τ_{ls} [ksi] (MPa)	[16.62] (115)	[12.87] (89)	[9.36] (64)	[8.60] (59)
Std.Dev. [ksi] (MPa)	[2.12] (15)	[2.36] (16)	[0.95] (6)	[0.69] (5)
Range	[14.24 - 19.64] (98 - 135)	[9.42 - 17.11] (65 - 118)	[8.59 - 10.79] (59 - 74)	[7.72 - 9.56] (53 - 66)
No. of Specimens	5	10	5	5
Test Method	ASTM D2344			
Reference				

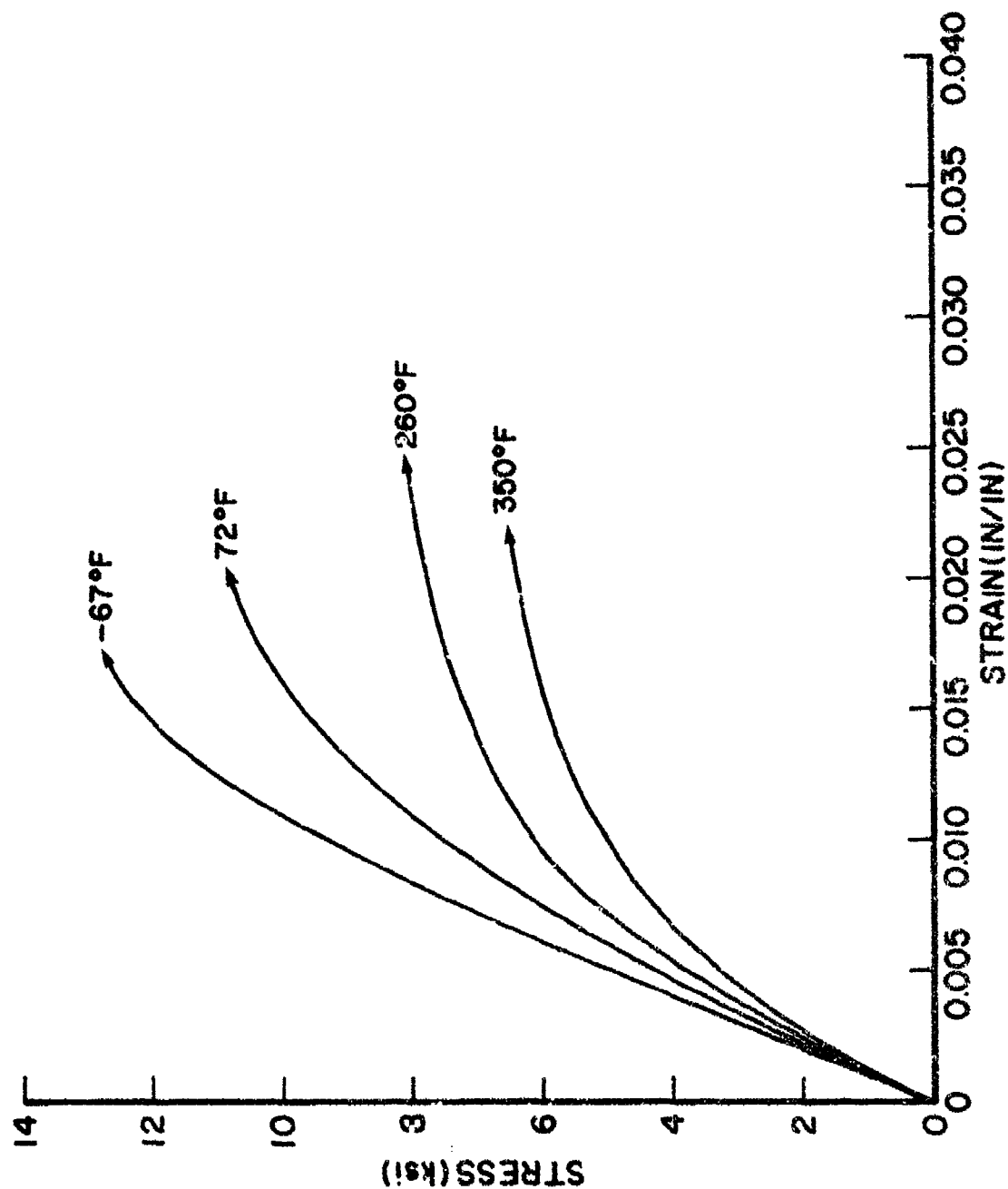


Figure 82. Inplane Shear Stress-Strain Curves for HyE 1076 Composite Laminates.

TABLE 68

TENSILE, COMPRESSIVE, AND SHEAR PROPERTIES OF HYE 1076J COMPOSITE LAMINATES AFTER HUMIDITY AGING

Composite Material Properties

Material System - HVS 1076J		Gr/Ep		COMPRESSION: 90°									
Fiber - 1900/15K Matrix - 97%		Prepreg by - Fibreite		72°F (22°C)									
Maximum Rated Temperature - 350°F		Laminate Sp. Gr. - 1.63		161									
Resin Content - 24.4% by wt. (177°C)		Nominal Ply Thickness - 0.0050 in. (0.13mm)		161									
Fiber Content - 69.5% by wt.		No. of panels from which specimens were tested in this table - 6		0.73									
Void Content - ± 0% by vol.		Aging Conditions - 160°F (71°C) ± 100% R.H.		0.05									
Thickness of each type specimen: Tension - 15 ply/ Comp. - 20 ply/ Shear - 15 ply				5									
TENSION: 90°													
Exposure Time (hrs)	72°F (22°C)	160°F (71°C)	72°F (22°C)	160°F (71°C)	72°F (22°C)	160°F (71°C)	72°F (22°C)	160°F (71°C)	72°F (22°C)	160°F (71°C)	72°F (22°C)	160°F (71°C)	240°F (127°C)
Wt. Gain(% of orig. dry wt.)	0.77	0.76	1.17 ¹	1.77 ²	1.17 ¹	1.77 ²	1.17 ¹	1.77 ²	1.17 ¹	1.77 ²	1.17 ¹	1.77 ²	1.05 ³
Std. Dev. (%)	0.04	0.03	0.02	5	0.01	5	0.01	5	0.01	5	0.01	5	0.05
No. of Specimens	5	5	5	5	5	5	5	5	5	5	5	5	5
$P_{t/y}$ [ksi] (MPa)	(4.80) (33)	(2.90) (20)	(4.03) (28)	(1.49) (10)	(1.49) (10)	(1.49) (10)	(1.49) (10)	(1.49) (10)	(1.49) (10)	(1.49) (10)	(1.49) (10)	(1.49) (10)	(1.49) (10)
Std. Dev. [ksi] (MPa)	(0.73) (5)	(0.47) (3)	(0.18) (1)	(0.42) (3)	(0.42) (3)	(0.42) (3)	(0.42) (3)	(0.42) (3)	(0.42) (3)	(0.42) (3)	(0.42) (3)	(0.42) (3)	(0.42) (3)
Range	(4.14-5.98)	(2.47-3.63)	(3.80-4.26)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)	(1.09-1.99)
No. of Specimens	5	5	5	5	5	5	5	5	5	5	5	5	5
$P_{c/y}$ [ksi] (MPa)	(3.49) (24)	(1.31) (9)	(3.83) (26)	(1.05) (7)	(1.05) (7)	(1.05) (7)	(1.05) (7)	(1.05) (7)	(1.05) (7)	(1.05) (7)	(1.05) (7)	(1.05) (7)	(1.05) (7)
Std. Dev. [ksi] (MPa)	(1.63) (11)	(0.64) (4)	(0.59) (4)	(0.24) (2)	(0.24) (2)	(0.24) (2)	(0.24) (2)	(0.24) (2)	(0.24) (2)	(0.24) (2)	(0.24) (2)	(0.24) (2)	(0.24) (2)
No. of Specimens	5	5	5	5	5	5	5	5	5	5	5	5	5
E_y [ksi] (GPa)	(1.41) (10)	(1.20) (8)	(1.41) (10)	(1.03) (7)	(1.03) (7)	(1.03) (7)	(1.03) (7)	(1.03) (7)	(1.03) (7)	(1.03) (7)	(1.03) (7)	(1.03) (7)	(1.03) (7)
Std. Dev. [ksi] (GPa)	(0.09) (1)	(0.09) (1)	(0.10) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)	(0.16) (1)
No. of Specimens	5	5	5	5	5	5	5	5	5	5	5	5	5
ϵ_y [in/in] (µm/cm)	3.500	2.700	2.800	1.480	1.480	1.480	1.480	1.480	1.480	1.480	1.480	1.480	1.480
Std. Dev.	540	370	200	300	300	300	300	300	300	300	300	300	300
No. of Specimens	5	5	5	5	5	5	5	5	5	5	5	5	5
Test Method Reference	Straight-sided tension ASTM D3039												
INTERLAMINAR SHEAR													
Exposure Time (hrs)	168	168	168	168	168	168	168	168	168	168	168	168	168
Wt. Gain(% of orig. dry wt.)	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Std. Dev. (%)	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
No. of Specimens	10	10	10	10	10	10	10	10	10	10	10	10	10
$P_{i/y}$ [ksi] (MPa)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)	(11.88) (81.9)
Std. Dev. [ksi] (MPa)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)	(1.68) (11.6)
Range	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)	(9.62-15.17)
No. of Specimens	10	10	10	10	10	10	10	10	10	10	10	10	10
Test Method Reference	ASTM D2344												

¹ Represents 100% saturation at aging conditions.² One of five specimens exhibited evidence of buckling.³ Two of five specimens exhibited evidence of buckling.

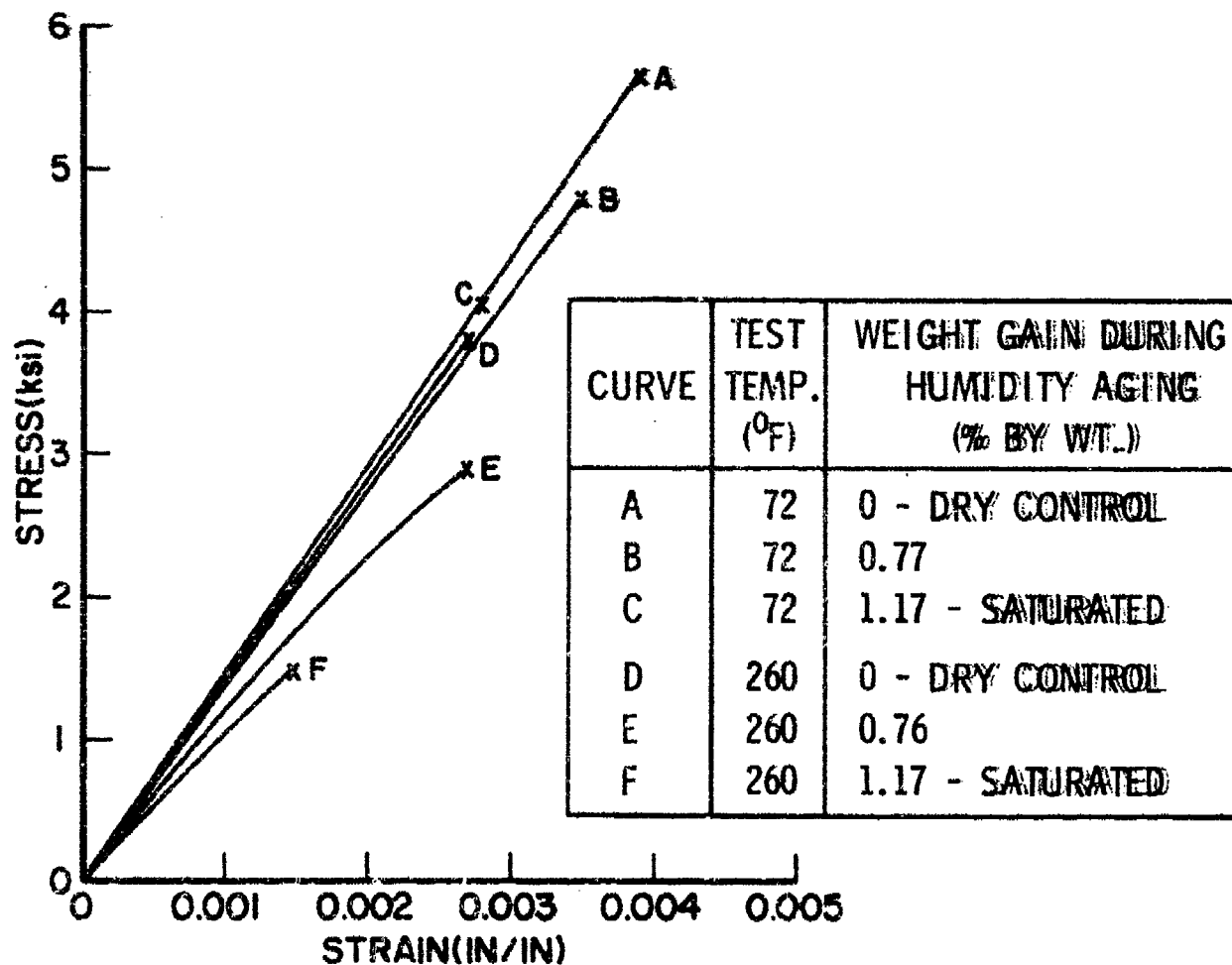


Figure 83 . Tensile Stress-Strain Curves for Unidirectional HyE 1076J Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

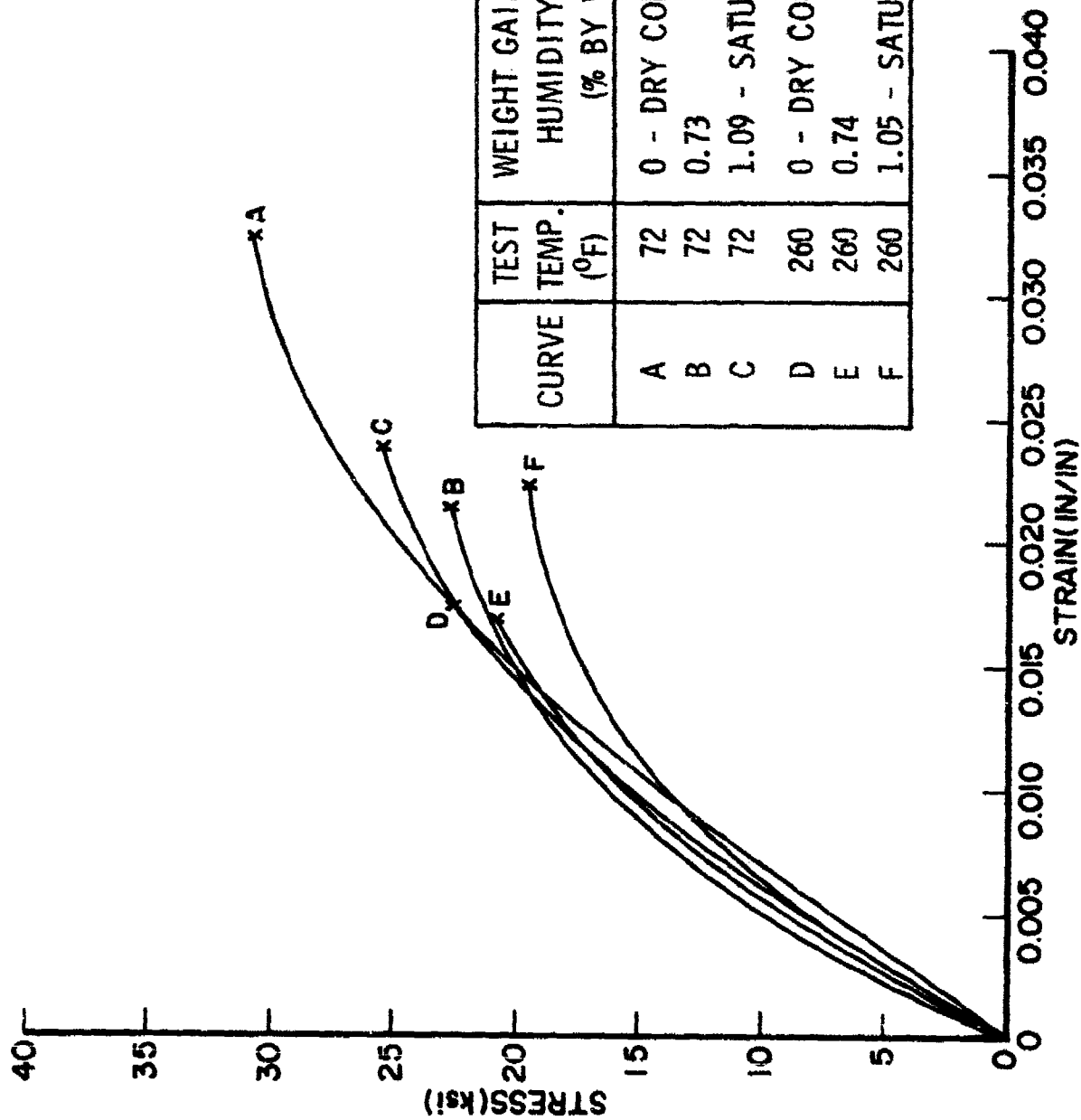


Figure 84. Compressive Stress-Strain Curves for Unidirectional HyE 1076J Composite Laminates After Humidity Aging at 160°F (71°C) and 100% R.H.: 90° Fiber Orientation.

TABLE 69
CREEP PROPERTIES OF HYE 1076J
COMPOSITE LAMINATES

Composite Material Properties			
Material System - HYE 1076J		Prepared by - Fiberite	Gr/Ep
Fiber - T300/L5K Matrix - 976		Laminate Sp. Gr. - 1.62	
Maximum Temperature Rating - 350°F (177°C)		Nominal Ply Thickness - 0.0053 inch (0.13 mm)	
Resin Content - 25.2% by wt.		No. of panels from which specimens were tested in this table - 16	
Fiber Content - 68.0% by vol.		Thickness of each type specimen:	
Void Content - 4.0.3% by vol.		0/45/90 - 20 ply	
Test Method - Straight-sided tension		+45 - 8 ply	
Reference - ASTM D2290 and D3039			
CREEP			
Temperature	Fiber Orientation	(0,+45,-45,0,0,-45,+45,0,90,0)°	+45°
72°F (22°C)	Stress Level [ksi] (MPa)	(93.5) (644)	(20.05) (138)
	Creep Strain, 500 hr (%)	0.0239	0.01
	No. of Specimens	1 ¹	3
	Residual Strength [ksi] (MPa)	(130.9) (902)	
	No. of Specimens	1	0
	Stress Level [ksi] (MPa)	(81.8) (564)	(17.83) (123)
	Creep Strain, 500 hr (%)	0.0121	0.3005
	No. of Specimens	3	3
	Residual Strength [ksi] (MPa)	(115.6) (796)	(24.40) (168)
	No. of Specimens	3	3
240°F (127°C)	Stress Level [ksi] (MPa)	(70.1) (483)	(15.60) (107)
	Creep Strain, 500 hr (%)	0.0254	0.2074
	No. of Specimens	1	3
	Residual Strength [ksi] (MPa)	(104.3) (719)	(23.35) (161)
	No. of Specimens	1	3
	Stress Level [ksi] (MPa)	(96.1) (662)	(13.19) (91)
	Creep Strain, 500 hr (%)	0.0003 ²	0.0003 ²
	No. of Specimens	1	3
	Residual Strength [ksi] (MPa)	(134.3) (925)	(22.45) (155)
	No. of Specimens	1	3
350°F (177°C)	Stress Level [ksi] (MPa)	(84.1) (579)	(11.55) (80)
	Creep Strain, 500 hr (%)	0.0002	0.3870 ³
	No. of Specimens	3	2
	Residual Strength [ksi] (MPa)	(111.4) (768)	(22.72) (157)
	No. of Specimens	3	2
	Stress Level [ksi] (MPa)	(72.0) (496)	(9.90) (68)
	Creep Strain, 500 hr (%)	0.0109	0.4191
	No. of Specimens	3	3
	Residual Strength [ksi] (MPa)	(111.6) (769)	(20.88) (144)
	No. of Specimens	3	3
350°F (177°C)	Stress Level [ksi] (MPa)	(94.5) (651)	(13.28) (91)
	Creep Strain, 500 hr (%)	0.0183	0.0183
	No. of Specimens	2	3
	Residual Strength [ksi] (MPa)	(119.2) (821)	(21.64) (149)
	No. of Specimens	-2 ⁴	3
	Stress Level [ksi] (MPa)	(82.7) (570)	(11.62) (80)
	Creep Strain, 500 hr (%)	0.0607	0.8734 ⁵
	No. of Specimens	3	1
	Residual Strength [ksi] (MPa)	(112.0) (772)	(20.93) (144)
	No. of Specimens	3	3
350°F (177°C)	Stress Level [ksi] (MPa)	(70.9) (489)	(9.96) (69)
	Creep Strain, 500 hr (%)	0.0754	0.0754
	No. of Specimens	3	3
	Residual Strength [ksi] (MPa)	(115.8) (798)	(19.52) (134)
	No. of Specimens	3	3

¹Three specimens failed on loading or during test.

²Strain exceeded limits of gage capabilities prior to end of test.

³Two specimens broke on loading.

⁴One specimen failed during test.

⁵Strain gages failed on two specimens during test.

⁶Two specimens failed during test.

⁷One specimen failed on loading.

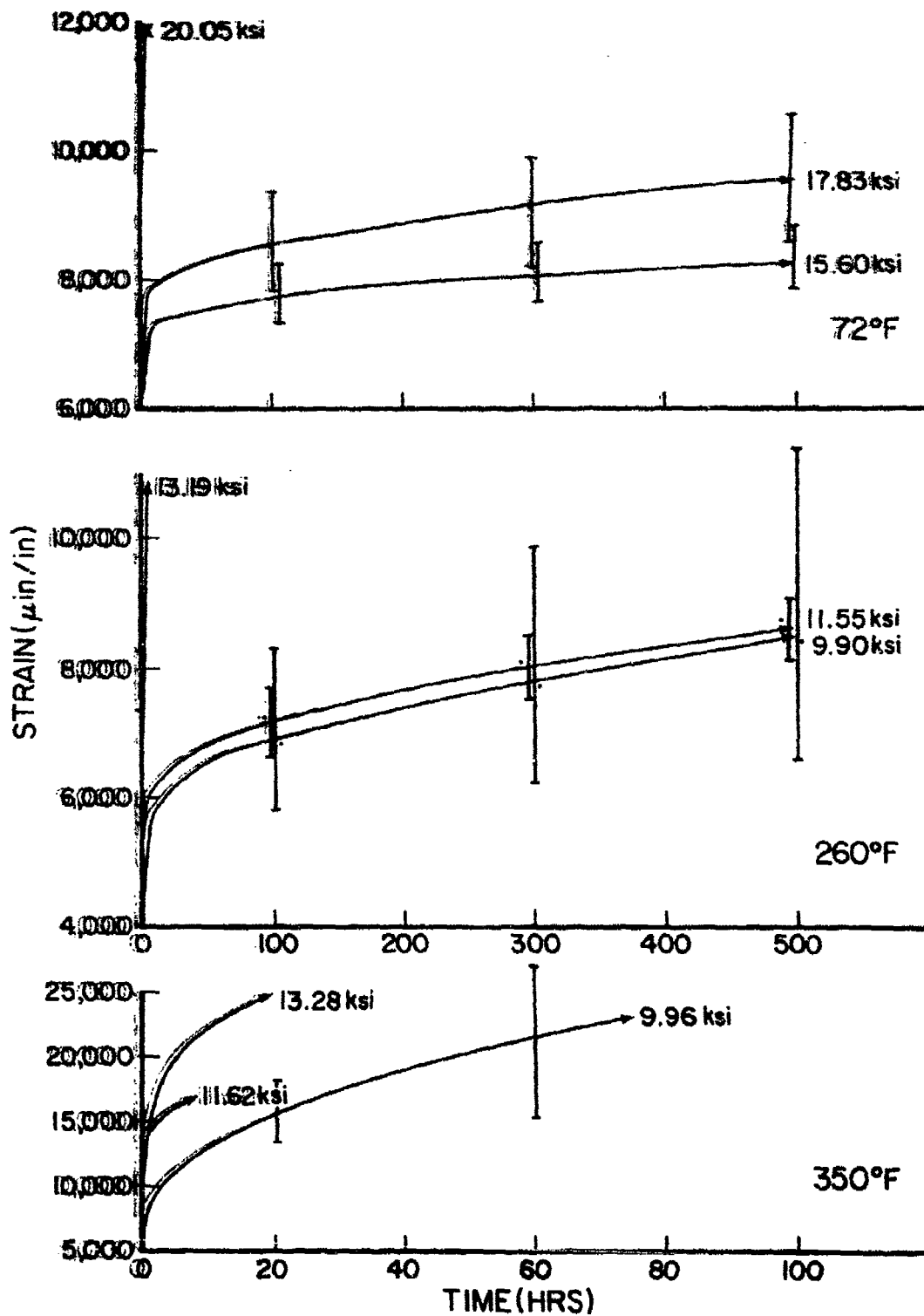


Figure 85. Tensile Creep Behavior of Bidirectional HyE 1076J Composite Laminates: $\pm 45^\circ$ Fiber Orientation.

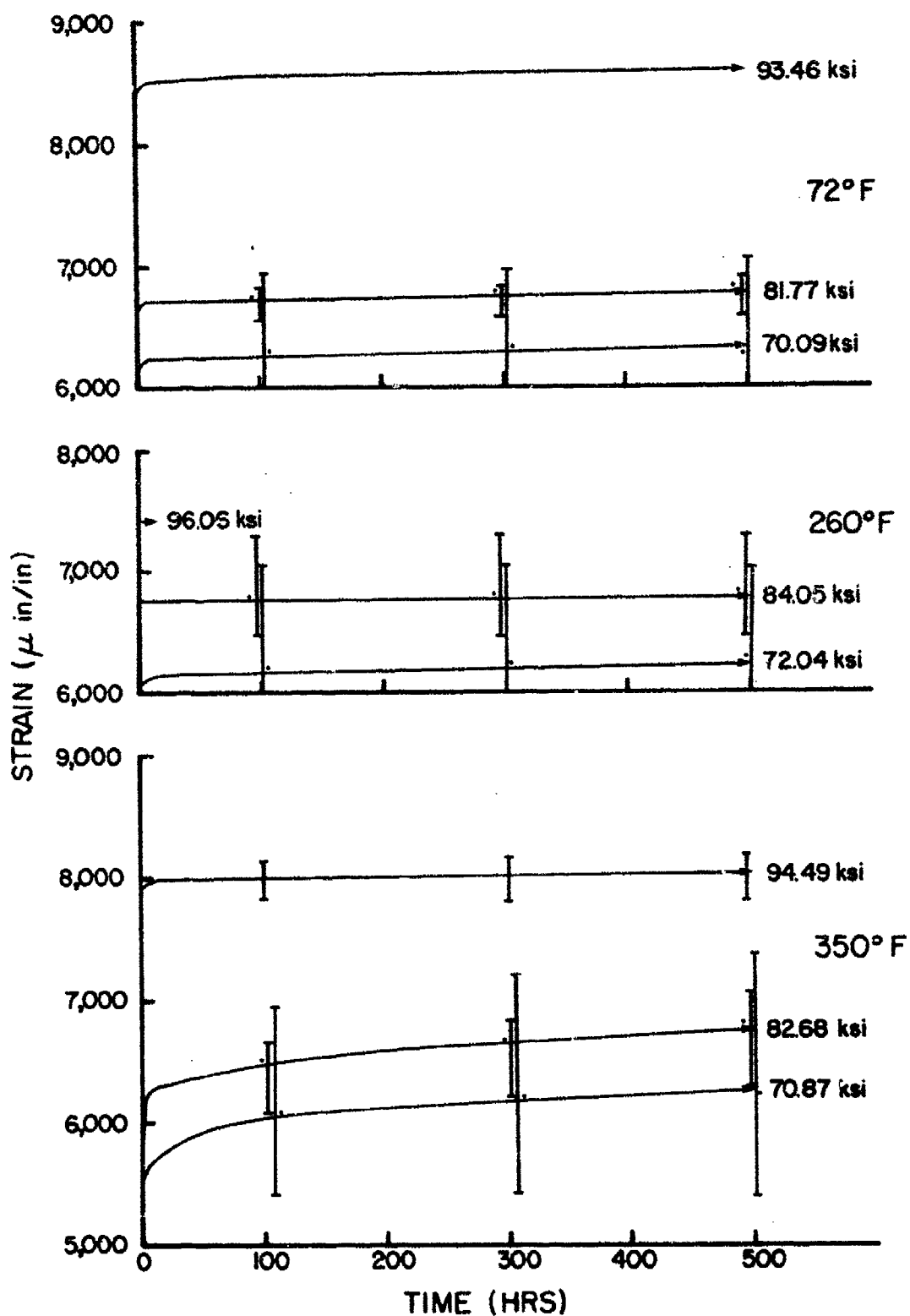


Figure 86. Tensile Creep Behavior of HyE 1076J Composite Laminates: (0,+45,-45,0,0,-45,+45,0,90,0)_s Fiber Orientation.

TABLE 70
STRESS-RUPTURE BEHAVIOR OF HyE 1076J
COMPOSITE LAMINATES

Composite Material Properties			
Material system - HyE 1076J Fiber - T300/15K Matrix - 976 Maximum Temperature Rating - 350°F(177°C) Resin Content - 25.2% by wt. Fiber Content - 68.0% by vol. Void Content - ±0.3% by vol. Test Method - Straight-sided tension Reference - ASTM D2290 and D3039			Gr/Epoxy
Prepreg by - Fiberite Lamina Sp. Gr. - 1.62 Nominal Ply Thickness - 0.0053 inch (0.13 mm) No. of panels from which specimens were tested in this table - 16 Thickness of each type specimen: (0/+45/90) - 20 ply +45 - 8 ply			
STRESS RUPTURE			
Temperature	Fiber Orientation	(0,+45,-45,0,0,-45,+45,0,90,0) _g	+45°
72°F (22°C)	Stress Level[ksi](MPa)	[93.5] (644)	[17.83] (123)
	Time to Failure(hrs)	167+ ¹	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[130.9] (902)	[24.40] (168)
	No. of Specimens	1	3
	Stress Level[ksi](MPa)	[81.8] (564)	[15.60] (107)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[115.6] (796)	[23.15] (161)
	No. of Specimens	3	3
260°F(127°C)	Stress Level[ksi](MPa)	[95.1] (662)	[13.19] (91)
	Time to Failure(hrs)	256+ ²	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[134.3] (925)	[22.45] (155)
	No. of Specimens	1	3
	Stress Level[ksi](MPa)	[84.1] (579)	[9.90] (68)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[111.4] (768)	[20.88] (144)
	No. of Specimens	3	3
350°F(177°C)	Stress Level[ksi](MPa)	[94.5] (651)	[13.28] (91)
	Time to Failure(hrs)	334+ ³	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[119.2] (821)	[21.64] (149)
	No. of Specimens	2	3
	Stress Level[ksi](MPa)	[82.7] (570)	[11.62] (80)
	Time to Failure(hrs)	500+	500+
	No. of Specimens	3	3
	Residual Strength[ksi](MPa)	[112.0] (772)	[20.93] (144)
	No. of Specimens	3	3

¹Two specimens broke on loading.

²Two specimens broke during test.

³One specimen broke on loading.

TABLE 71

TENSILE-TENSILE FATIGUE PROPERTIES OF
HyE 1076J COMPOSITE LAMINATES

Composite Material Properties				
Material System - HyE 1076J		Prepreg by - Fiberite		GK/Ep
Fiber - T300/15K Matrix - 976		Laminate Sp. Gr. - 1.62		
Maximum Temperature Rating - 350°F(177°C)		Nominal Ply Thickness - 0.0052 inch (0.13 mm)		
Resin Content - 25.2% by wt.		No. of panels from which specimens were tested		
Fiber Content - 68.1% by vol.		in this table - 20		
Void Content - 0.2% by vol.		Thickness of each type specimen:		
Test Method - Straight-sided tension		+45 - 8 ply		
Reference - ASTM D3039		0/+45/90 - 20 ply		
TENSILE FATIGUE ¹ , R=0.1				
Temperature	Fiber Orientation	+45°	0/+45/90 ¹	0/+45/90 ^{1,2}
72°F(22°C)	Max. Stress[ksi](MPa)	[17.82] (123)	[105.1] (724)	[97.4] (671)
	Lifetime (cycles)	5,701	19,153	735
	No. of Specimens	5	5	2
	Residual Strength[ksi](MPa)	—	—	—
	No. of Specimens	0	0	0
	Max. Stress[ksi](MPa)	[15.60] (107)	[102.2] (704)	[92.9] (640)
	Lifetime (cycles)	136,004	182,507	6421
	No. of Specimens	5	3	4
	Residual Strength[ksi](MPa)	—	—	—
	No. of Specimens	0	0	0
	Max. Stress[ksi](MPa)	[14.48] (100)	[99.3] (684)	[88.5] (610)
	Lifetime (cycles)	1,120,500	598,592	94,313
	No. of Specimens	4	5	5
	Residual Strength[ksi](MPa)	—	—	[119.3] (815)
	No. of Specimens	0	0	1
260°F(127°C)	Max. Stress[ksi](MPa)	[14.02] (97)	[108.1] (745)	
	Lifetime (cycles)	23,206	4,850	
	No. of Specimens	5	4	
	Residual Strength[ksi](MPa)	—	—	
	No. of Specimens	0	0	
	Max. Stress[ksi](MPa)	[13.19] (91)	[96.1] (662)	
	Lifetime (cycles)	71,048	84,188	
	No. of Specimens	5	5	
	Residual Strength[ksi](MPa)	—	—	
	No. of Specimens	0	0	
	Max. Stress[ksi](MPa)	[12.37] (85)	[90.1] (621)	
	Lifetime (cycles)	488,973	1,438,881	
	No. of Specimens	5	5	
	Residual Strength[ksi](MPa)	—	—	
	No. of Specimens	0	0	

¹Stacking sequence (0,+45,-45,0,0,-45,+45,0,90,0)₂.²These specimens had a 0.1935 inch (0.491 cm) hole in the center of the test section. Stresses calculated using net cross-sectional area.³Fatigue lifetimes are log-mean values.

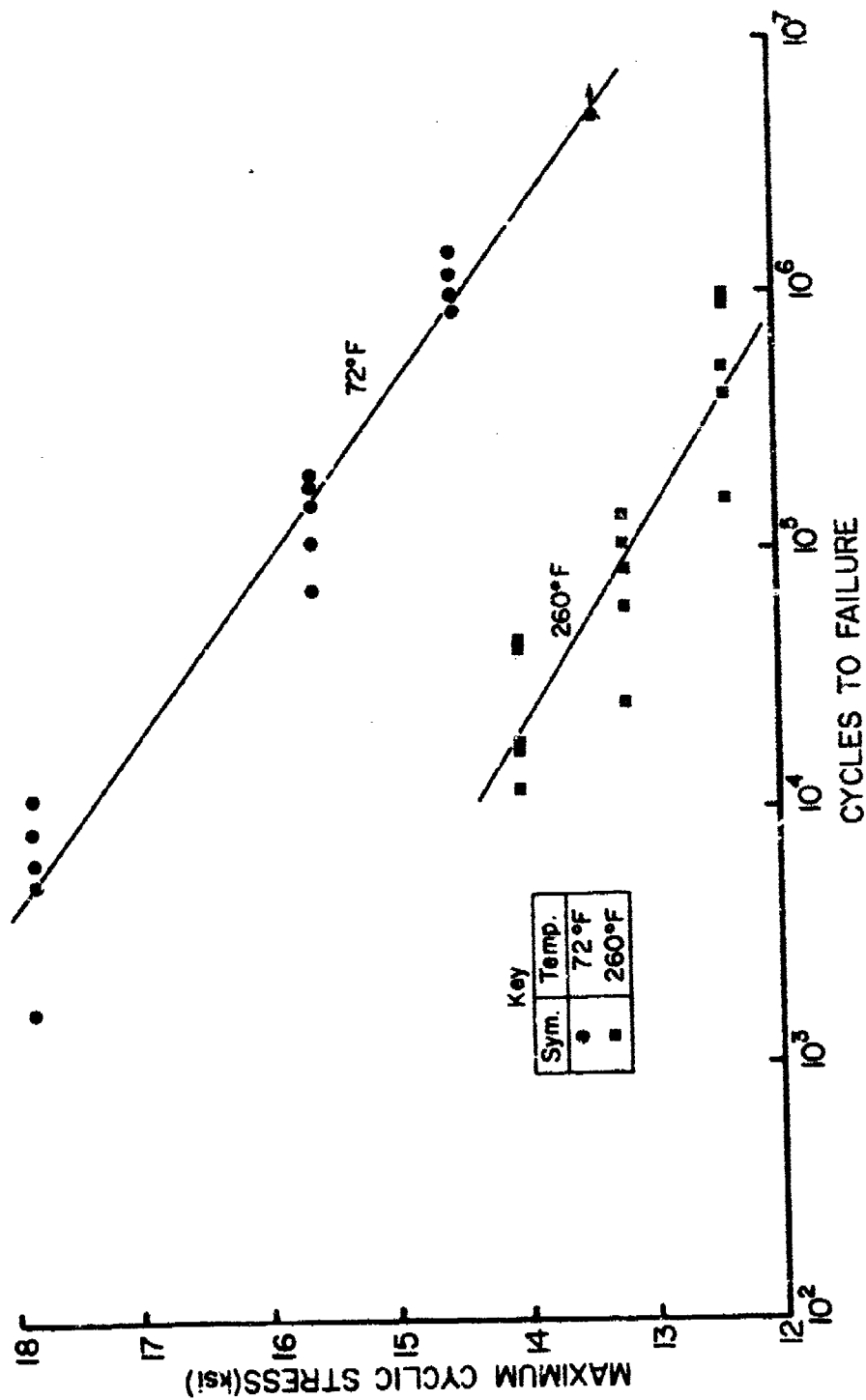


Figure 87. Tensile-Tensile Fatigue Behavior of Bidirectional HyE 1076J Composite
Laminates: +45° Fiber Orientation, R = 0.10, 10 Hz.

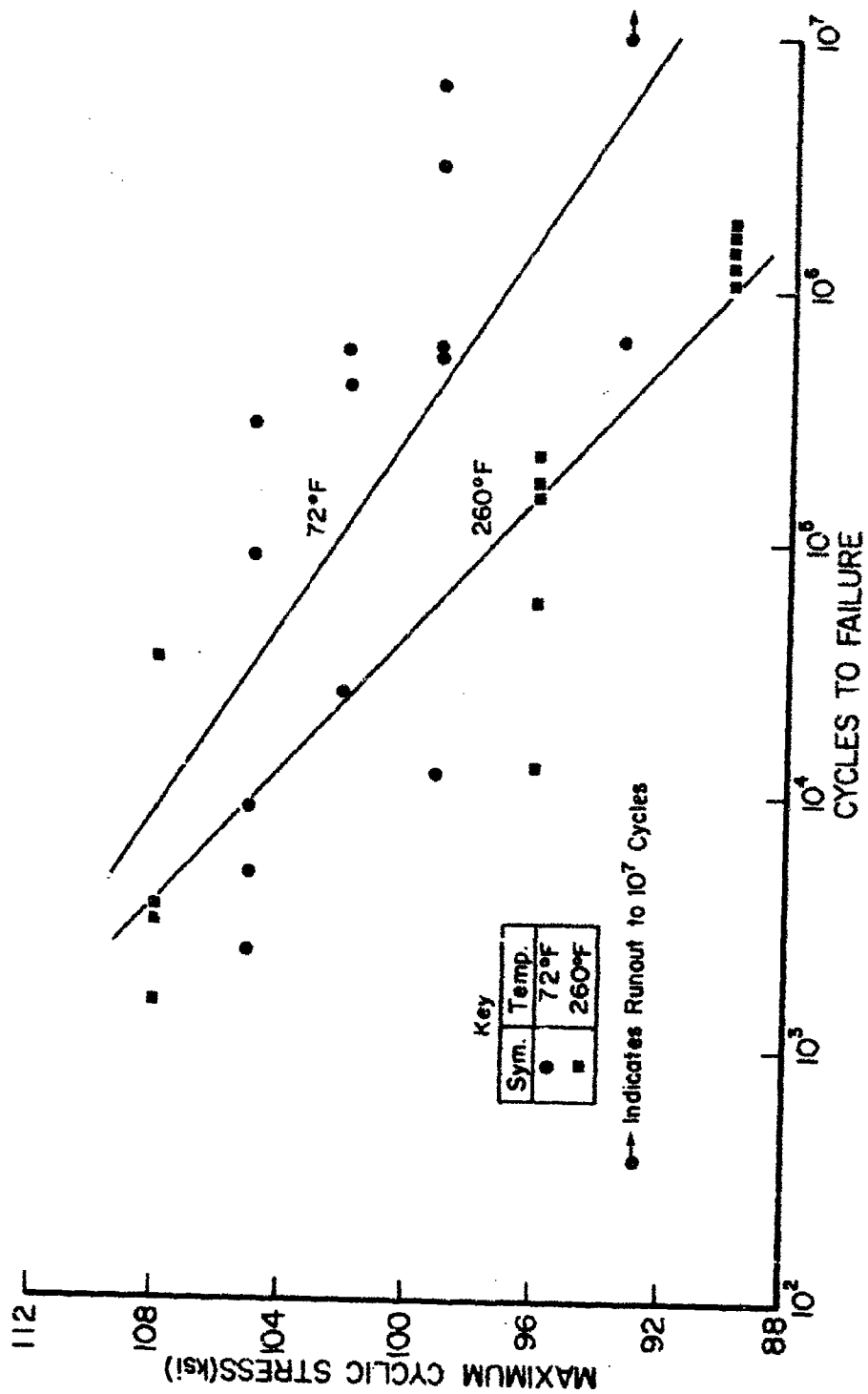


Figure 88. Tensile-Tensile Fatigue Behavior of Multidirectional HyE 1076J Composite
Laminates: (0,45,-45,0,0,-45,45,0,90,0)°s Fiber Orientation, $R = 0.10$,
10 Hz.

TABLE 72
THERMOPHYSICAL PROPERTIES OF HYE 1076J
COMPOSITE LAMINATES

Composite Material Properties					
Material System - HyE 1076J		Prepreg by - Fiberite		Gz/Epoxy	
Fiber - T300/15K Matrix - 976		Laminate Sp. Gr. - 1.62		Average Ply Thickness - 0.00050 inch(0.13 mm)	
Maximum Temperature Rating - 350°F(177°C)		No. of panels from which specimens were tested in this table - 2			
Resin Content - 25.6% by wt.					
Fiber Content - 67.7% by vol.					
Void Content - ± 0% by vol.					
Thickness of each type specimen:		Therm. Exp. - 40 ply		Spec. Ht. - 1 ply	
		Therm. Cond. - 40 ply		Glass Trans. - 8 ply	
THERMOPHYSICAL PROPERTIES: 0°					
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)	Test Method
Thermal Expansion ¹					TMA ²
α_x (in/in-°F) (μm/cm-°C)	[0.08] (0.15)	[-0.30] (-0.54)	[-0.24] (-0.44)	[-0.18] (-0.32)	
α_y (in/in-°F) (μm/cm-°C)	[12.5] (22.5)	[13.6] (24.4)	[17.4] (31.4)	[19.2] (34.6)	
No. of Specimens per direction	3	3	3	3	
Specific Heat					DSC ³
C_p (btu/lb.-°F) (J/kg-°C)	[0.153] (640)	[0.205] (860)	[0.274] (1150)	[0.330] (1380)	
No. of Specimens	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z (btu-ft/ft ² -hr-°F) (W/m-°C)	[0.37] (0.64)	[0.42] (0.72)	[0.48] (0.84)	[0.51] (0.89)	
No. of Specimens	3	3	3	3	
Glass Transition Temp.					DMA ⁴
Dry (°F) (°C)	[518] (270)				
Wet (°F) (°C)	[493] (256)				
THERMOPHYSICAL PROPERTIES: +45°					
Thermal Expansion ¹					TMA ²
α_x (in/in-°F) (μm/cm-°C)	[1.7] (3.1)	[1.4] (2.6)	[1.4] (2.5)	[1.5] (2.7)	
No. of Specimens per direction	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z (btu-ft/ft ² -hr-°F) (W/m-°C)	[0.28] (0.48)	[0.39] (0.67)	[0.53] (0.92)	[0.61] (1.05)	
No. of Specimens	3	3	3	3	

NOTES: 1. On the unidirectionally reinforced specimens, the x-direction is along the fiber axis, the y-direction is across the fiber axis, and the z-direction is through the thickness (identical to the y-direction). On +45° bidirectionally reinforced specimens, the x and y directions are identical and oriented at 45° to either fiber direction, while the z-direction is through the thickness.

2. Thermo-Mechanical Analysis.

3. Differential Scanning Calorimetry.

4. Dynamic Mechanical Analysis.

TABLE 73
COMPARISON OF 934 AND 976 RESIN PROPERTIES¹

<u>RESIN</u>	<u>934</u>	<u>976</u>
<u>VISCOSITY, cps</u>	6,000-12,000	6,000-12,000
*At 75 + 0.5°C *Brookfield Model HBT Viscometer *Fiberite FTM-V-9 Test Method		
<u>GEL TIME, MINUTES</u>	8-16	15-30
*At 170 + 10°C (934), 177 + 1°C (976) *Fisher-Johns Melting Point Apparatus *Fiberite FTM-G-3 Test Method		
<u>SPECIFIC GRAVITY OF CURED RESIN</u>	1.30	1.28
*At 23 + 2°C *Analytical Balance *ASTM-D-792 Test Method		
<u>% WEIGHT LOSS</u>	.450	.255
*RT to 200°C *T.G.A. *Heat-Up rate - - 5°C/Min		
<u>CAST RESIN PROPERTIES</u>		
*Tensile Strength, ksi	8,000-10,000	8,000-10,000
*Tensile Modulus, ksi	.3 - .5	.3 - .5
*Tensile Elongation, %	3	5
*Mean Glass Transition Temperature, °C	214	250

¹All data in this table provided by FIBERITE.

TABLE 74
COMPARISON OF DAY/WET MECHANICAL PROPERTIES¹

	<u>hy-E 1034C</u>	<u>hy-E 1076C</u>
<u>CURED LAMINATE</u>		
Resin Content, %	24.0	25.7
Fiber Volume, %	70.0	68.6
Void Content, %	0	0
Specific Gravity	1.62	1.63
Nominal Cured Ply Thickness, In.	.005	.005
<u>0° FLEXURAL STRENGTH, KSI (Normalized to 65% fiber volume)</u>		
RT, Dry	273	282
RT, Wet	NT	281
250°F, Dry	NT	266
250°F, Wet	177	226
350°F, Dry	197	215
350°F, Wet	63	140
<u>0° FLEXURAL MODULUS, MSI (Normalized to 65% fiber volume)</u>		
RT, Dry	20.4	20.5
RT, Wet	NT	20.1
250°F, Dry	NT	19.5
250°F, Wet	19.5	20.4
350°F, Dry	20.2	19.4
350°F, Wet	10.0	18.8
<u>SHORT BEAM SHEAR, KSI</u>		
RT, Dry	17.7	17.1
RT, Wet	NT	14.2
250°F, Dry	12.8	12.3
250°F, Wet	6.8	8.2
350°F, Dry	7.9	10.4
350°F, Wet	4.1	5.5

¹All data in this table provided by FIBERITE.

4.6 G-160/6535-1

This graphite/epoxy system was developed by AVCO and consists of a 160,000 filament graphite fiber tow (G-160) in a 350°F (177°C) epoxy matrix resin. Both the fiber and resin are manufactured by AVCO. The advantage of such a large filament tow is that prepreg costs can be considerably reduced.

Tables 75 through 87 present the data generated for this graphite/epoxy system. Figures 90 through 105 illustrate the stress-strain, fatigue, and creep behavior of this material as well as the effects of humidity aging upon selected composite properties.

The resin in this prepreg proved to be a very high flow material and it was difficult to avoid laminates with fiber content levels lower than 65-70% by volume, even with greatly reduced bleeder material and sealed layup bags. Although the acid digestion technique for determining fiber and resin content produced consistent fiber content levels of 65-73% by volume for the panels fabricated by several different layup schemes and cure schedules, photomicrographs of the laminate cross-sections seemed to indicate lower fiber contents for the tested laminates.

Figure 92 presents photomicrographs of two G-160/6535-1 laminates fabricated according to different layup/curing schemes and also of a T300/V378A laminate. Pertinent laminate physical property measurements are presented for each laminate along with comments based on inspection of the photomicrographs. It would appear that the fiber packings for panels K-2 and I-19 are comparable (disregarding the voids in K-2) while that for panel K-31 is slightly less (more average space between fibers). This would infer an approximately equivalent fiber content for panels K-2 and I-19 and a lower fiber content for panel K-31. As can be observed from the data accompanying the photomicrographs, this result was not obtained experimentally. Since the fiber packing obtained for panel K-31 did not appear unreasonably dense and was

comparable to that obtained for previous materials which exhibited fiber content levels of around 65%, it was decided to proceed with the cure schedule and layup scheme used for K-31 and described in Table 75 and illustrated in Figure 90 and simply report the measured fiber contents with this commentary.

TABLE 75
PROCESSING CONDITIONS FOR G-160/6535-1 COMPOSITE LAMINATES

Composite Processing Information	
Material System - G-160/6535-1 Fiber - G-160 Matrix - 6535-1 Maximum Rated Temperature - 350°F(177°C) Prepreg by - AVCO	Gr/Ep
<p style="text-align: center;">Laminate Processing Schedule</p> <p>Layup Procedure: The prepreg was stored in a closed wrapper at room temperature. Prepreg was removed from wrapper and plies cut to desired size using a razor knife. Plies were stacked in the desired sequence (release paper removed from each ply). The stack was placed in the autoclave according to the layup system illustrated in Figure 90. The corprene edge dam serves to restrict fiber flow.</p> <p>Cure Schedule: Apply full vacuum and heat to 265°F in 45 + 5 mins. under full vacuum. Hold at 265°F for 30 mins., then apply 100 psi. Heat to 350°F in 20 +5 mins. Hold at 350°F for two hours. Cool under pressure, and vacuum, to 120°F.</p> <p>Postcure Schedule: The panels were placed, unrestrained, in an oven at room temperature. The oven was brought to 375°F at rate of about 5°F/min. After a four-hour hold at 375°F, the oven was turned off. When the oven was cooled to near room temperature, the panels were removed.</p>	

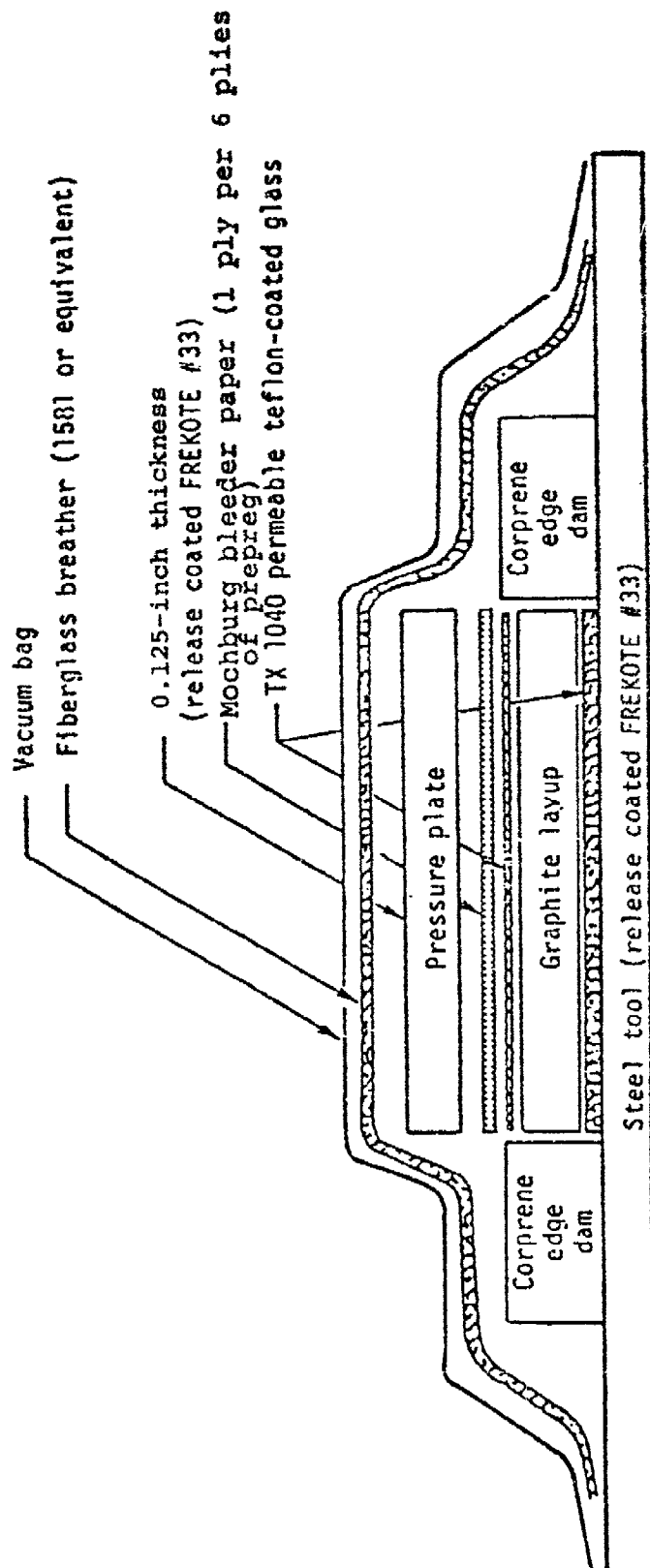


Figure 90. Layup System for AVCO 6535-1 Laminates.

TABLE 76
PREPREG AND COMPOSITE PHYSICAL PROPERTIES

Composite Physical Property Information					
Material System - G-160/6535-1				Gr/Ep	
Fiber - G-160 Matrix - 6535-1					
Maximum Rated Temperature - 350°F(177°C)				Prepreg by - AVCO	
Prepreg Physical Properties					
(Property)	(Std.Dev.)	(Range)	(Test Method)	(Ref.)	
Volatile Content- 0.20% by wt.	0.06	0.13-0.28	QCI-C-V-14	Fiberite	
Resin Content- 41.5% by wt.	1.7	39.3-44.1	R-15	Fiberite	
Gel Time @ 327°F(164°C)-38.2 min.	0.6	37.2-38.7	G-2	Fiberite	
No. of Rolls Involved- 2					
No. of Batches Involved- 1					
Laminate Physical Properties ¹					
	(Std.Dev.)	(Range)	(Test Method)	(Ref.)	
No. of Panels- 34					
Fiber Content- 68.4% by vol.	1.2	66.1-71.5	Acid Digestion	AFML-TR-67-243	
Resin Content- 25.7% by wt.	1.0	22.9-27.3			
Void Content- ± 0% by vol.			D2734	ASTM	
Laminate Sp. Gr.- 1.61	0.01	1.59-1.63	D792	ASTM	
Fiber Sp. Gr.- 1.75	As reported by manufacturer.				
Matrix Sp. Gr.- 1.26	As reported by manufacturer.				
Thickness per ply-					

¹The properties reported here represent averages for all panels of this material used throughout the program.

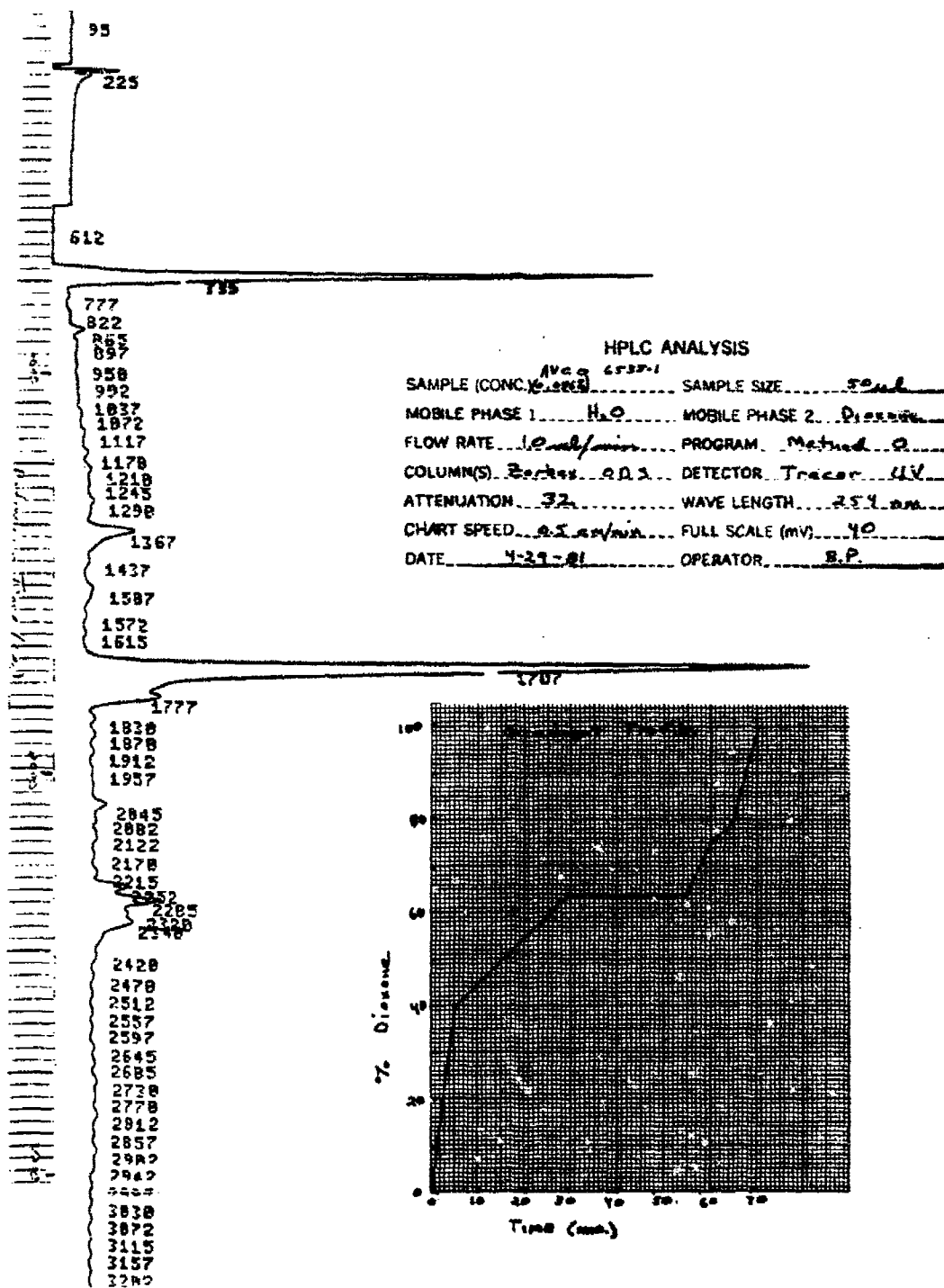
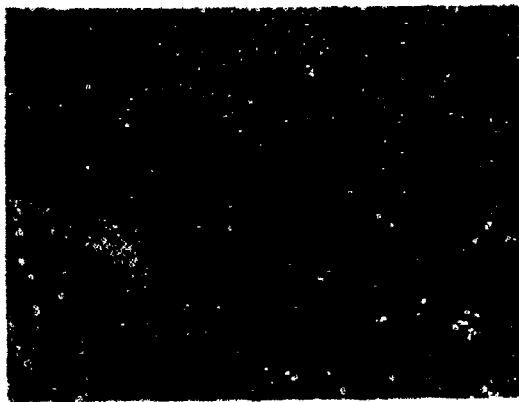
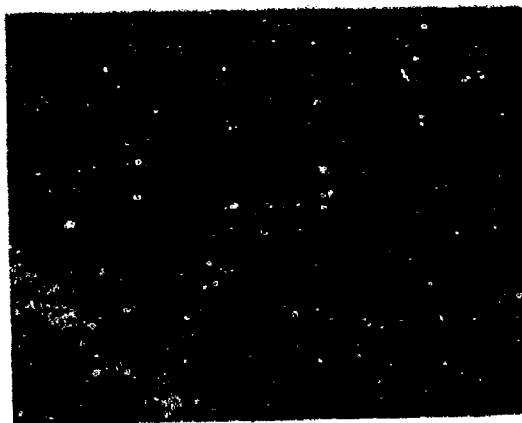


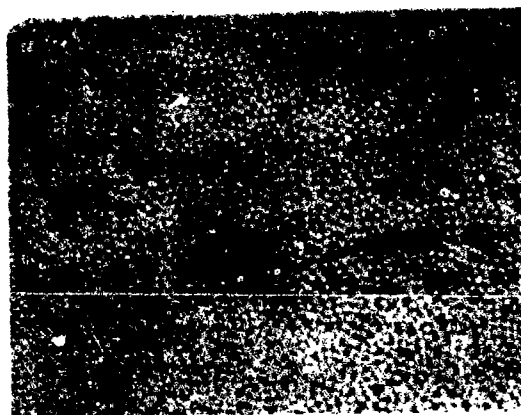
Figure 91. HPLC Analysis of AVCO 6535-1 Epoxy Resin.



- (a) G-160/6535-1
 PANEL K-2
 EARLY CURE SCHEDULE/LAYUP SCHEME
 FIBER CONTENT - 69.0% BY VOL.
 SPECIFIC GRAVITY - 1.58
 RESIN CONTENT - 23.8% BY WT.
 VOID CONTENT - 1.2% BY VOL.
 VISIBLE VOIDS



- (b) G-160/6535-1
 PANEL K-31
 FINAL CURE SCHEDULE/LAYUP SCHEME
 FIBER CONTENT - 68.5% BY VOL.
 SPECIFIC GRAVITY - 1.61
 RESIN CONTENT - 25.7% BY WT.
 VOID CONTENT - 0
 FIBER PACKING LESS DENSE THAN
 FOR PANEL K 2



- (c) T300/V378A
 PANEL I-19
 FIBER CONTENT - 65.2% BY VOL.
 SPECIFIC GRAVITY - 1.59
 RESIN CONTENT - 28.2% BY WT.
 VOID CONTENT - 0
 FIBER PACKING COMPARABLE TO
 PANEL K 2

Figure 92. Photomicrographs of Composite Laminates.

TABLE 77
TENSILE PROPERTIES OF G-160/6535-1 COMPOSITE LAMINATES

Composite Material Properties					
Material System - G160/6535-1		Prepreg by - AWC		Gr/Epoxy	
Fiber - G-160 Matrix - 6535-1		Laminate Sp. Gr. - 1.61			
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0048 inch (0.12 mm)			
Resin Content - 25.7% by wt.		No. of panels from which specimens were tested			
Fiber Content - 68.5% by vol.		in this table - 8			
Void Content - ± 0% by vol.					
Thickness of each type specimen: 0° - 6 ply		; 90° - 15 ply			
TENSION: 0°					
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)	
F_{tX}^u [ksi] (MPa)	[172.4] (1188)	[167.5] (1154)	[162.6] (1120)	[171.3] (1180)	
Std.Dev. [ksi] (MPa)	[25.7] (177)	[12.1] (83)	[7.5] (52)	[22.5] (155)	
Range [ksi] (MPa)	[148.3 - 213.8] (1022 - 1473)	[148.4 - 180.0] (1022 - 1240)	[150.0 - 168.6] (1033 - 1162)	[143.9 - 194.2] (991 - 1338)	
No. of Specimens	5	5	5	5	
F_{tX}^{tpl} [ksi] (MPa)	[172.4] (1188)	[167.5] (1154)	[162.6] (1120)	[166.7] (1149)	
Std.Dev. [ksi] (MPa)	[25.7] (177)	[12.1] (83)	[7.5] (52)	[20.7] (143)	
No. of Specimens	5	5	5	5	
E_x^t [ksi] (GPa)	[18.49] (127)	[18.54] (128)	[21.11] (145)	[19.89] (137)	
Std.Dev. [ksi] (GPa)	[0.52] (4)	[0.64] (4.4)	[0.68] (5)	[0.82] (6)	
No. of Specimens	5	5	5	5	
ϵ_x^u [in/in] (µm/cm)	9180	8530	7820	8390	
Std. Dev.	1410	680	940	1210	
No. of Specimens	5	5	5	5	
ν_{xy}^t	0.31	0.32	0.36	0.31	
Std. Dev.	0.04	0.01	0.02	0.08	
No. of Specimens	5	5	5	5	
Test Method	Straight-sided tension				
Reference	ASTM D3039				
TENSION: 90°					
F_{tY}^u [ksi] (MPa)	[4.93] (34)	[5.51] (38)	[3.88] (27)	[3.49] (24)	
Std.Dev. [ksi] (MPa)	[0.54] (4)	[0.43] (3)	[0.53] (4)	[0.85] (6)	
Range	[4.30 - 5.43] (30 - 37)	[5.19 - 6.15] (36 - 42)	[3.09 - 4.43] (21 - 31)	[2.42 - 4.41] (17 - 30)	
No. of Specimens	5	4	5	4	
F_{tY}^{tpl} [ksi] (MPa)	[1.58] (11)	[5.51] (38)	[2.70] (19)	[2.42] (17)	
Std.Dev. [ksi] (MPa)	[0.35] (2)	[0.43] (3)	[1.74] (12)	[0.64] (4)	
No. of Specimens	5	4	5	4	
E_y^t [ksi] (GPa)	[2.27] (16)	[1.82] (13)	[1.59] (11)	[1.63] (11)	
Std.Dev. [ksi] (GPa)	[0.31] (2)	[0.27] (2)	[0.21] (1.4)	[0.11] (1)	
No. of Specimens	5	5	5	4	
ϵ_y^u [in/in] (µm/cm)	2290	3290	2490	2270	
Std. Dev.	510	440	380	780	
No. of Specimens	5	4	5	4	
ν_{yz}^t	0.038 ¹	0.031 ¹	0.027 ¹	0.025 ¹	
Std. Dev.	---	---	---	---	
No. of Specimens	---	---	---	---	
Test Method	Straight-sided tension				
Reference	ASTM D3039				

¹Computed using elastic moduli and longitudinal Poisson's ratio.

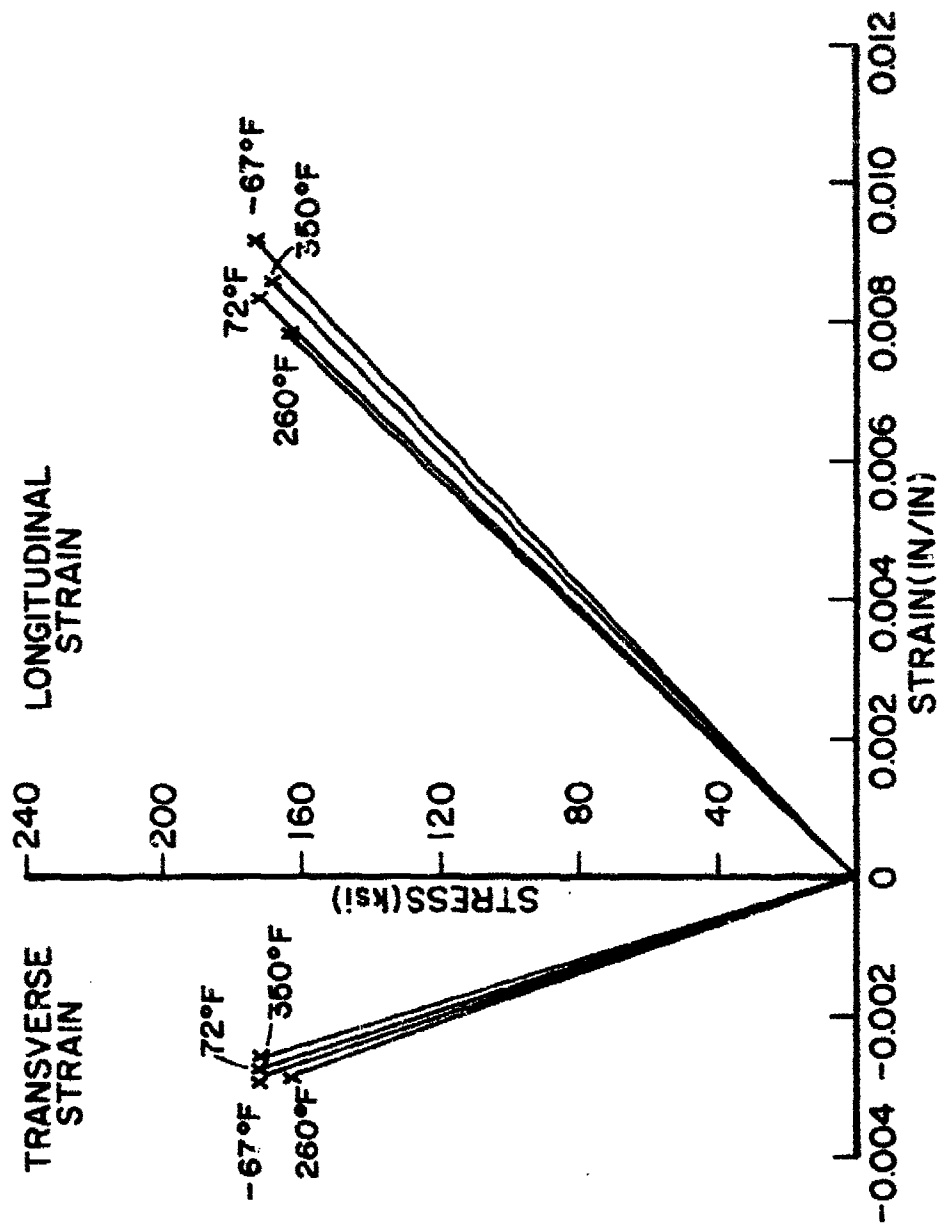


Figure 93. Tensile Stress-Strain Curves for Unidirectional G-160/6535-1 Composite Laminates: 0° Fiber Orientation.

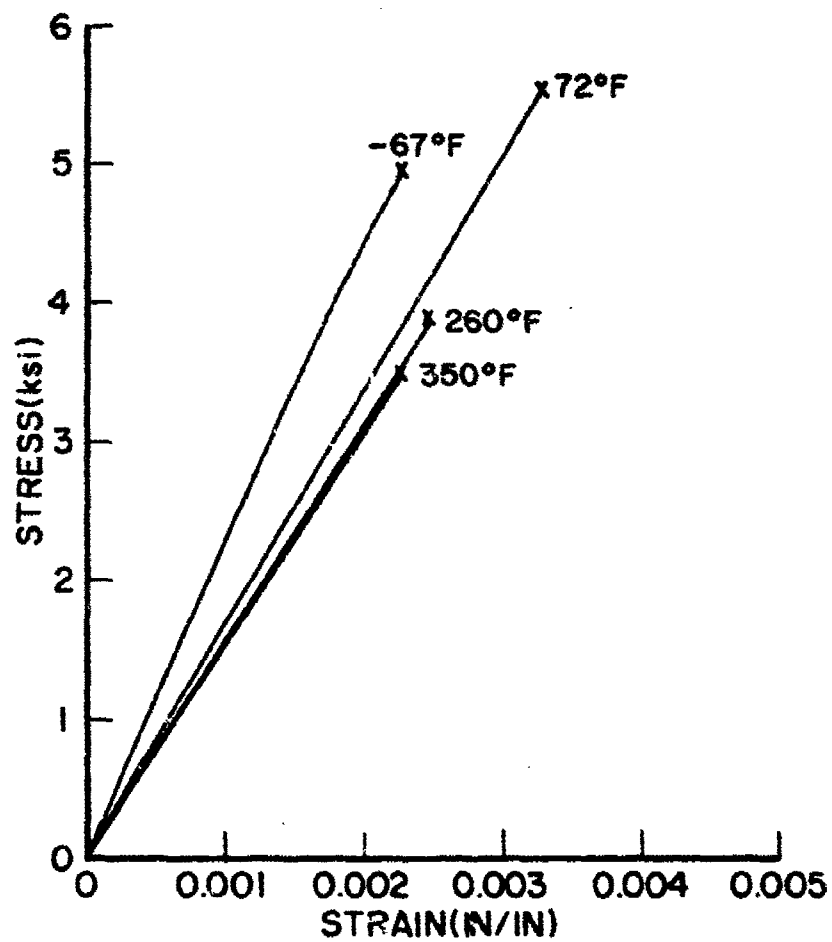


Figure 94. Tensile Stress-Strain Curves for Unidirectional G-160/6535-1 Composite Laminates: 90° Fiber Orientation.

TABLE 73
TENSILE PROPERTIES OF G-160/6535-1 COMPOSITE LAMINATES

Composite Material Properties				
Material System - G-160/6535-1		Prepreg by - AVCO	Gr/Epoxy	
Fiber - J-160	Matrix - 6535-1	Laminate Sp. Gr. - 1.61		
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.004 inch (0.13 mm)		
Resin Content - 26.0% by wt.		No. of panels from which specimens were tested		
Fiber Content - 67.7% by vol.		in this table - 8		
Void Content - 2% by vol.		Thickness of specimen - 3 plies		
TENSION: +45°				
	-67°F (-55°C)	72°F (22°C)	250°F (127°C)	350°F (177°C)
F_{tx} [ksi] (MPa)	[19.43] (134)	[16.53] (114)	[15.56] (107)	[16.48] (114)
Std.Dev. [ksi] (MPa)	10.90 (6)	[1.17] (8)	[0.41] (3)	[1.10] (8)
Range [ksi] (MPa)	[18.72-20.89] (129 - 144)	[15.36-17.77] (106 - 122)	[14.88-15.91] (103 - 110)	[15.03-17.48] (104 - 120)
No. of Specimens	5	5	5	5
F_{xtp} [ksi] (MPa)	[9.53] (66)	[5.92] (41)	[4.61] (32)	[4.05] (28)
Std.Dev. [ksi] (MPa)	[1.96] (14)	[1.41] (10)	[0.72] (5)	[0.28] (2)
No. of Specimens	5	5	5	5
E_x^t [Msi] (GPa)	[3.28] (23)	[3.12] (21)	[3.05] (21)	[2.79] (19)
Std.Dev. [Msi] (GPa)	10.21 (1)	[0.12] (1)	[0.12] (1)	[0.08] (0.6)
No. of Specimens	5	5	5	5
ϵ_{tx} [in/in] ($\mu\text{cm/cm}$)	6,890	6,940	10,520	34,800
Std. Dev.	1,380	850	2,150	---
No. of Specimens	5	5	5	2 ¹
ν_{xy}^t	0.62	0.65	0.72	0.72
Std. Dev.	0.04	0.05	0.07	0.03
No. of Specimens	5	5	5	5
Test Method	Straight-sided tension			
Reference	ASTM D3039			

¹Strain gage failed before end of test on three specimens.

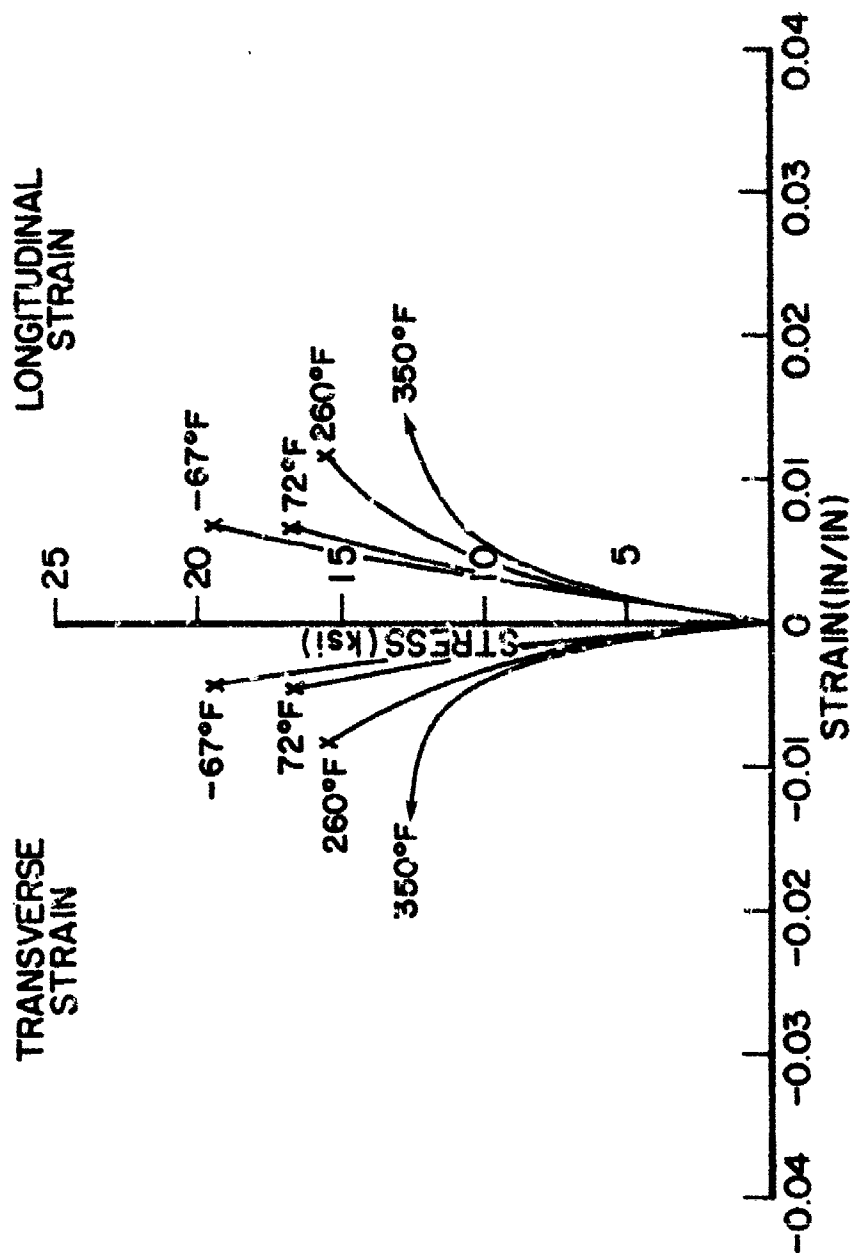


Figure 95. Tensile Stress-Strain Curves for Bidirectional G-160/6535-1 Composite Laminates: +45° Fiber Orientation.

TABLE 79
TENSILE PROPERTIES OF G-160/6535-1 COMPOSITE LAMINATES

Composite Material Properties				
Material System - G-160/6535-1		Prepreg by - AVCO		Gr/Epoxy
Fiber - G-160		Matrix - 6535-1		
Maximum Rated Temperature - 350°F(177°C)		Laminate Sp. Gr. - N.A.		
Resin Content - N.A.		Nominal Ply Thickness - 0.0048 inch (0.12 mm)		
Fiber Content - N.A.		No. of panels from which specimens were tested in this table - 9		
Void Content - N.A.		Thickness of specimen - (see footnotes)		
TENSION: 72°F (22°C)				
		(0/±45) ¹	(0/±45/90) ²	(0/±45/90) ³
F_x^{tu}	[ksi] (MPa)	[97.3] (670)	[91.5] (630)	[90.9] (626)
Std. Dev.	[ksi] (MPa)	[6.0] (41)	[8.8] (61)	[6.0] (41)
Range	[ksi] (MPa)	[88.3 - 103.2] (608 - 711)	[79.9 - 102.0] (551 - 703)	[84.8 - 100.7] (584 - 694)
No. of Specimens		5	5	5
F_x^{tpl}	[ksi] (MPa)	[97.3] (670)	[91.5] (630)	[90.9] (626)
Std. Dev.	[ksi] (MPa)	[6.0] (41)	[8.8] (61)	[6.0] (41)
No. of Specimens		5	5	5
E_x^t	[ksi] (GPa)	[11.41] (79)	[11.59] (80)	[10.92] (75)
Std. Dev.	[ksi] (GPa)	[1.11] (8)	[0.67] (5)	[0.12] (1)
No. of Specimens		5	5	5
ϵ_x^{tu}	[μ in/in] (μ cm/cm)	8170	7740	8210
Std. Dev.		680	720	560
No. of Specimens		5	5	5
ν_{xy}^t		0.62	0.41	0.37
Std. Dev.		0.04	0.02	0.02
No. of Specimens		5	5	5
Test Method Reference		Straight-sided tension ASTM D3039		

¹ (0, +45, -45, 0, 0, -45, +45, 0) - 16 ply.

² (0, 90, +45, -45, 0, 0, -45, +45, 0, 0) - 20 ply.

³ (0, +45, -45, 0, 0, -45, +45, 0, 90, 0) - 20 ply.

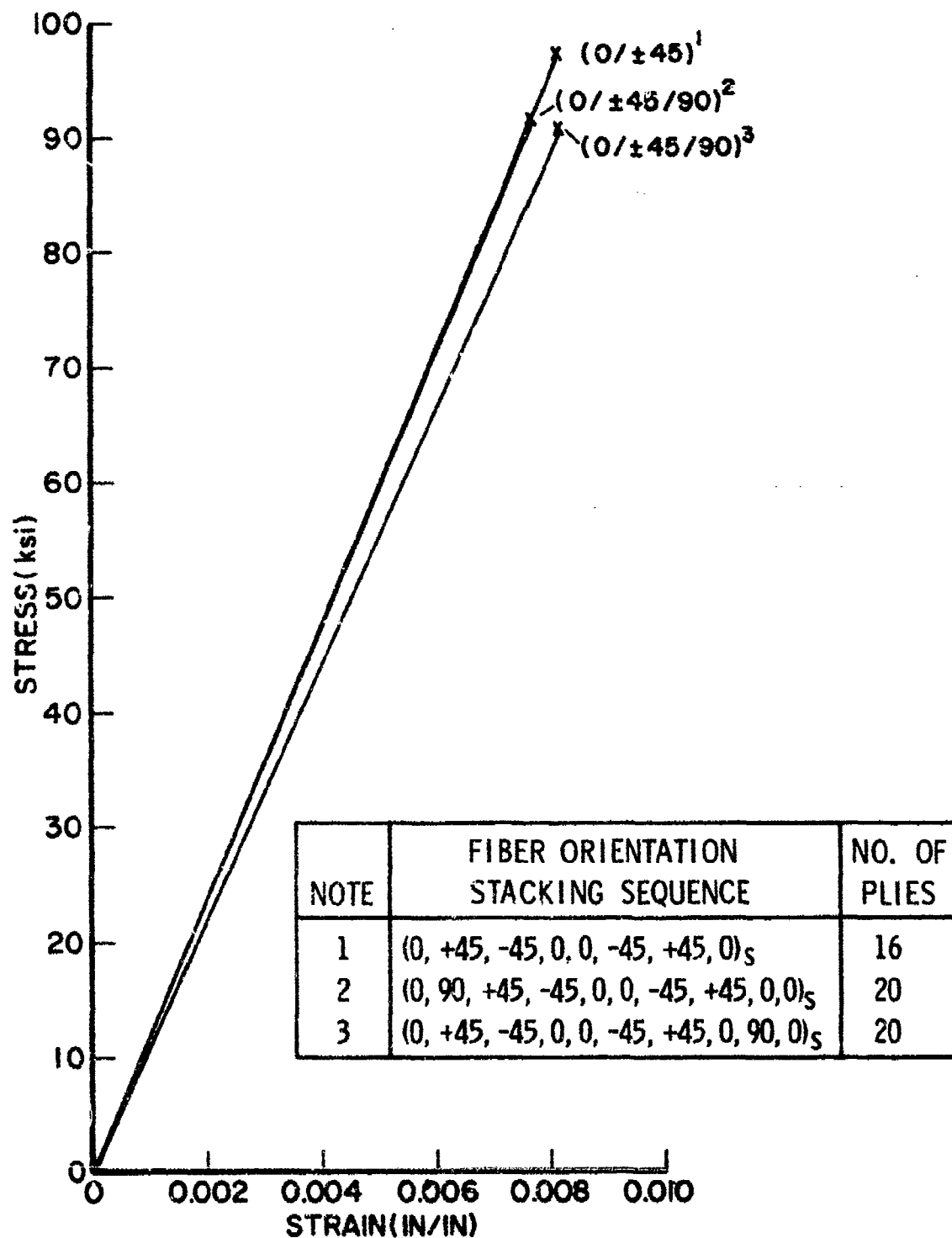


Figure 96. Tensile Stress-Strain Curves for Multidirectional G-160/6535-1 Composite Laminates.

TABLE 80
COMPRESSIVE PROPERTIES OF G-160/6535-1
COMPOSITE LAMINATES

Composite Material Properties					
Material System - G-160/6535-1		Prepreg by - AVCO		Gr/Epoxy	
Fiber - G-160 Matrix - 6535-1		Laminate Sp. Gr. - 1.61			
Maximum Rated Temperature - 350°F (177°C)		Nominal Ply Thickness - 0.0047 in. (0.12 mm)			
Resin Content - 23.9% by wt.		No. of panels from which specimens were tested			
Fiber Content - 70.0% by vol.		in this table - 3			
Void Content - ± 0% by vol.					
Thickness of each type specimen: 0° - 21 ply; 90° - 21 ply					
COMPRESSION: 0°					
	-67°F (-55°C)	72°F (22°C)	260°F (127°C)	350°F (177°C)	
F_{cu}^x [ksi] (MPa)	[214.0] (1474)	[212.3] (1463)	[188.8] (1301)	[151.4] (1043)	
Std. Dev. [ksi] (MPa)	[19.1] (132)	[8.0] (55)	[20.1] (138)	[11.3] (78)	
Range [ksi] (MPa)	[192.4 - 235.4] (1326 - 1622)	[204.0 - 223.9] (1405 - 1543)	[156.5 - 206.3] (1078 - 1421)	[145.8 - 163.0] (1005 - 1123)	
No. of Specimens	5	5	5	5	
F_{cpl}^x [ksi] (MPa)	[73.9] (509)	[106.3] (732)	[80.9] (557)	[101.9] (703)	
Std. Dev. [ksi] (MPa)	[8.6] (59)	[33.2] (229)	[13.1] (90)	[23.2] (160)	
No. of Specimens	5	5	3	5	
E_x^c [Msi] (GPa)	[20.54] (142)	[19.21] (132)	[18.73] (129)	[21.40] (147)	
Std. Dev. [Msi] (GPa)	[1.06] (7)	[1.34] (9)	[1.53] (11)	[2.45] (17)	
No. of Specimens	5	5	5	5	
ϵ_{cu}^x [in/in] ($\mu\text{cm/cm}$)	9,520 ^{+1,2}	14,800 ^{+1,3}	11,060 ^{+1,4}	8,530	
Std. Dev.	2,200	3,890	1,850	1,030	
No. of Specimens	5	5	5	5	
Test Method Reference	ASTM D3410				
COMPRESSION: 90°					
F_{cu}^y [ksi] (MPa)	[36.1] (249)	[27.0] (180)	[24.0] (165)	[19.8] (136)	
Std. Dev. [ksi] (MPa)	[6.3] (43)	[3.3] (23)	[1.3] (9)	[3.9] (27)	
Range	[29.7 - 45.5] (205 - 313)	[22.6 - 30.2] (156 - 208)	[22.0 - 25.4] (152 - 175)	[16.6 - 26.3] (114 - 181)	
No. of Specimens	5	5	5	5	
F_{cpl}^y [ksi] (MPa)	[14.1] (786)	[13.2] (91)	[15.9] (110)	[11.4] (79)	
Std. Dev. [ksi] (MPa)	[4.0] (28)	[1.5] (10)	[2.8] (19)	[1.9] (13)	
No. of Specimens	5	5	5	5	
E_y^c [Msi] (GPa)	[2.01] (14)	[2.04] (14)	[1.40] (10)	[1.80] (12)	
Std. Dev. [Msi] (GPa)	[0.16] (1)	[0.4] (3)	[0.11] (1)	[0.40] (3)	
No. of Specimens	5	5	5	5	
ϵ_{cu}^y [in/in] ($\mu\text{cm/cm}$)	25,730 ^{+1,2}	21,960 ^{+1,4}	15,660 ^{+1,5}	11,750 ^{+1,5}	
Std. Dev.	5,330	13,350	6,100	4,490	
No. of Specimens	5	5	5	5	
Test Method Reference	ASTM D3410				

¹Ultimate strain value represents maximum observed values rather than ultimate values.

²Three specimens exhibited evidence of buckling.

³One specimen exhibited evidence of buckling.

⁴Two specimens exhibited evidence of buckling.

⁵Four specimens exhibited evidence of buckling.

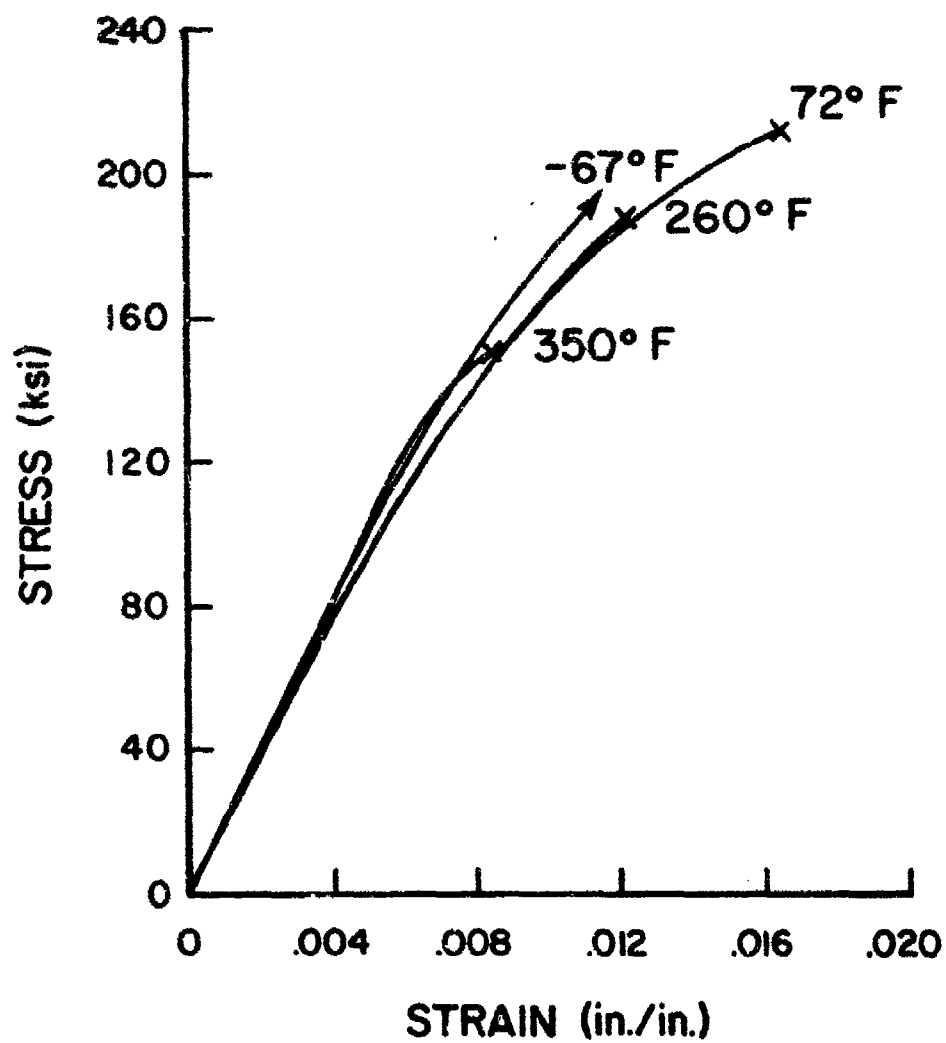


Figure 97. Compressive Stress-Strain Curves for Unidirectional G-160/6535-1 Composite Laminates: 0° Fiber Orientation.

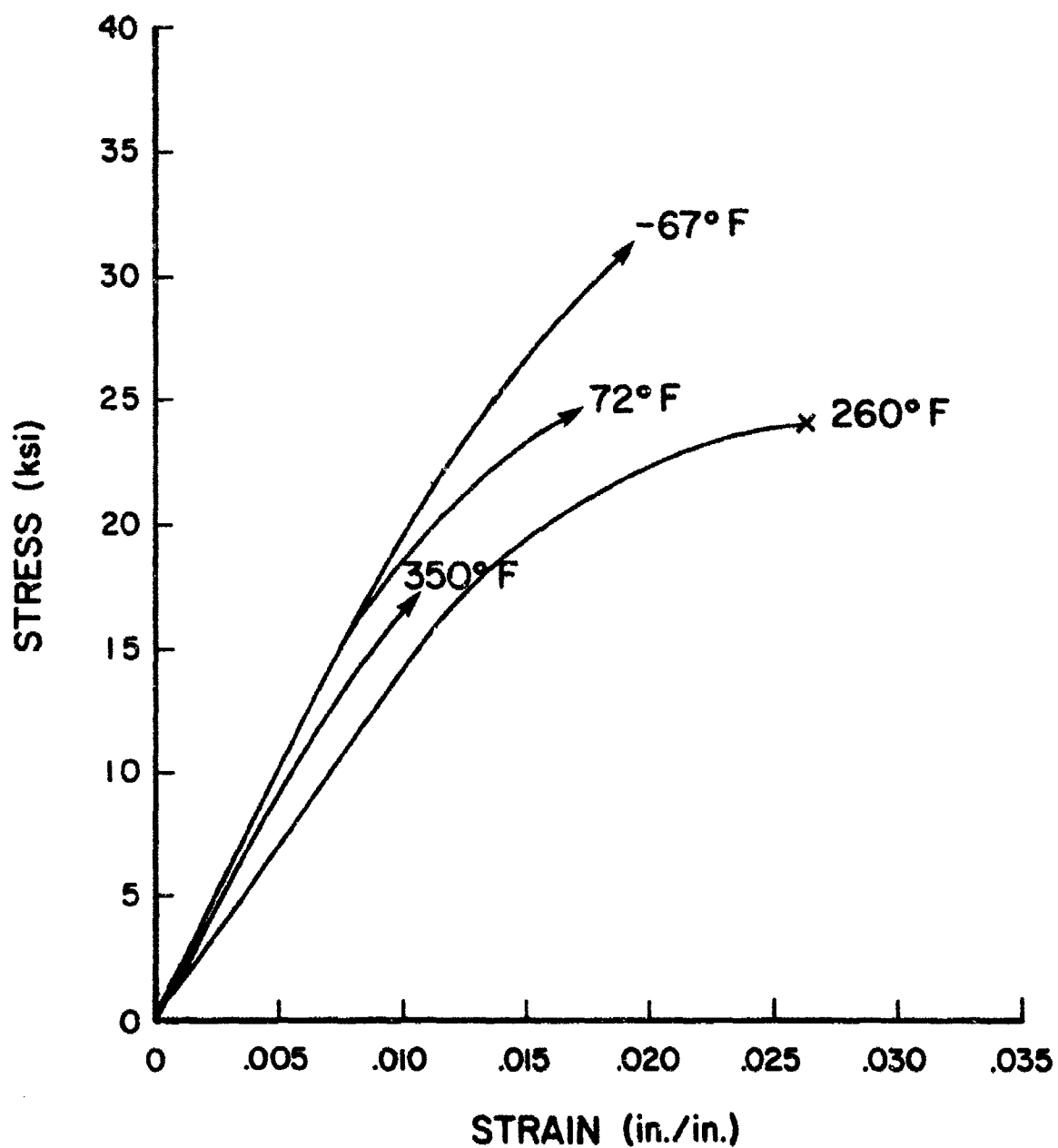


Figure 98 . Compressive Stress-Strain Curves for Unidirectional G-160/6535-1 Composite Laminates: 90° Fiber Orientation.

TABLE 81
FLEXURAL PROPERTIES OF G-160/6535-1 COMPOSITE LAMINATES

Composite Material Properties				
Material System - G-160/6535-1		Prepreg by - AVCO		Gr/Epoxy
Fiber - G-160 Matrix - 6535-1		Laminate Sp. Gr. - 1.61		
Maximum Rated Temperature - 350°F(177°C)		Nominal Ply Thickness - 0.0047 inch(0.12 mm)		
Resin Content - 24.8% by wt.		No. of panels from which specimens were tested		
Fiber Content - 69.6% by vol.		in this table - 2		
Void Content - ± 0% by vol.				
Thickness of each type specimen: 0° - 14 ply ; 90° - 14 ply				
FLEXURE: 0°				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F_x^{fu} [ksi] (MPa)	[239.9] (1653)	[231.3] (1594)	[219.7] (1514)	[181.7] (1252)
Std.Dev. [ksi] (MPa)	[17.2] (118)	[9.4] (65)	[4.9] (34)	[5.9] (53)
Range [ksi] (MPa)	[212.3 - 255.9] (1463 - 1763)	[215.2 - 237.6] (1483 - 1637)	[214.2 - 223.5] (1476 - 1540)	[175.8 - 189.4] (1211 - 1305)
No. of Specimens	5	5	3 ¹	5
E_x^f [Msi] (GPa)	[19.04] (131)	[18.49] (127)	[18.01] (124)	[16.85] (1150)
Std.Dev. [Msi] (GPa)	[1.19] (8)	[0.96] (7)	[0.60] (4)	[0.61] (4)
No. of Specimens	5	5	3	5
Test Method	3 pt.	4 pt.	3 pt.	3 pt.
Reference	Design Guide, Jan. 1971 - Corresponds to ASTM D790 except for loading points and loading speed.			
FLEXURE: 90°				
F_y^{fu} [ksi] (MPa)	[9.11] (63)	[8.86] (61)	[6.40] (44)	[6.50] (45)
Std.Dev. [ksi] (MPa)	[1.75] (12)	[0.44] (3)	[0.47] (3)	[0.22] (2)
Range [ksi] (MPa)	[7.09 - 10.14] (49 - 70)	[8.41 - 9.29] (58 - 64)	[4.70 - 7.78] (32 - 54)	[6.32 - 7.56] (44 - 52)
No. of Specimens	5	5	5	5
E_y^f [Msi] (GPa)	[1.53] (11)	[1.45] (10)	[1.45] (10)	[1.34] (9)
Std.Dev. [Msi] (GPa)	[0.04] (0.3)	[0.06] (0.4)	[0.04] (0.3)	[0.13] (1)
No. of Specimens	5	5	5	5
Test Method	4 pt. flexure } corresponds to ASTM D790 except for loading			
Reference	Design Guide, Jan. 1971 points and loading speed			

¹Two specimens tested in 4-point loading exhibited shear failure at a flexural stress of 163.7 ksi.

TABLE 82
SHEAR PROPERTIES OF G-160/6535-1 COMPOSITE LAMINATES

Composite Material Properties				
Material System - G-160/6535-1		Prepreg by - AVCO		Gr/Epoxy
Fiber - C-160		Matrix - 6535-1		
Maximum Rated Temperature - 350°F (177°C)		Laminate Sp. Gr. - 1.60		
Resin Content - 26.7% by wt.		Nominal Ply Thickness - 0.0050 inch (0.13 mm)		
Fiber Content - 66.9% by vol.		No. of panels from which specimens were tested in this table - 9		
Void Content - ± 0% by vol.				
Thickness of each type specimen - Inplane - 8 ply ; Interlaminar - 15 ply				
INPLANE SHEAR				
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)
F _{xy} [ksi](MPa)	[9.71] (67)	[8.43] (58)	[7.77] (54)	[8.24] (57)
Std.Dev.[ksi](MPa)	[0.45] (3)	[0.67] (5)	[0.21] (1)	[0.55] (4)
Range [ksi](MPa)	[9.34 - 10.44] (64 - 72)	[7.68 - 9.00] (53 - 62)	[7.42 - 7.94] (51 - 55)	[7.54 - 8.74] (52 - 60)
No. of Specimens	5	5	5	5
G _{xy} [Msi](GPa)	[1.01] (7)	[0.94] (6)	[0.89] (6)	[0.81] (6)
Std.Dev.[Msi](GPa)	[0.06] (0.4)	[0.03] (0.2)	[0.05] (0.3)	[0.03] (0.2)
No. of Specimens	5	5	5	5
Test Method Reference	ASTM D3518			
INTERLAMINAR SHEAR				
F _{isu} [ksi](MPa)	[16.96] (117)	[14.53] (100)	[11.90] (82)	[9.27] (64)
Std.Dev.[ksi](MPa)	[1.14] (8)	[1.17] (8)	[0.47] (3)	[0.62] (4)
Range	[15.19 - 18.21] (105 - 125)	[13.10 - 16.13] (90 - 111)	[11.36 - 12.39] (78 - 85)	[8.46 - 9.79] (58 - 67)
No. of Specimens	5	10	5	5
Test Method Reference	Short beam shear ASTM D2344			

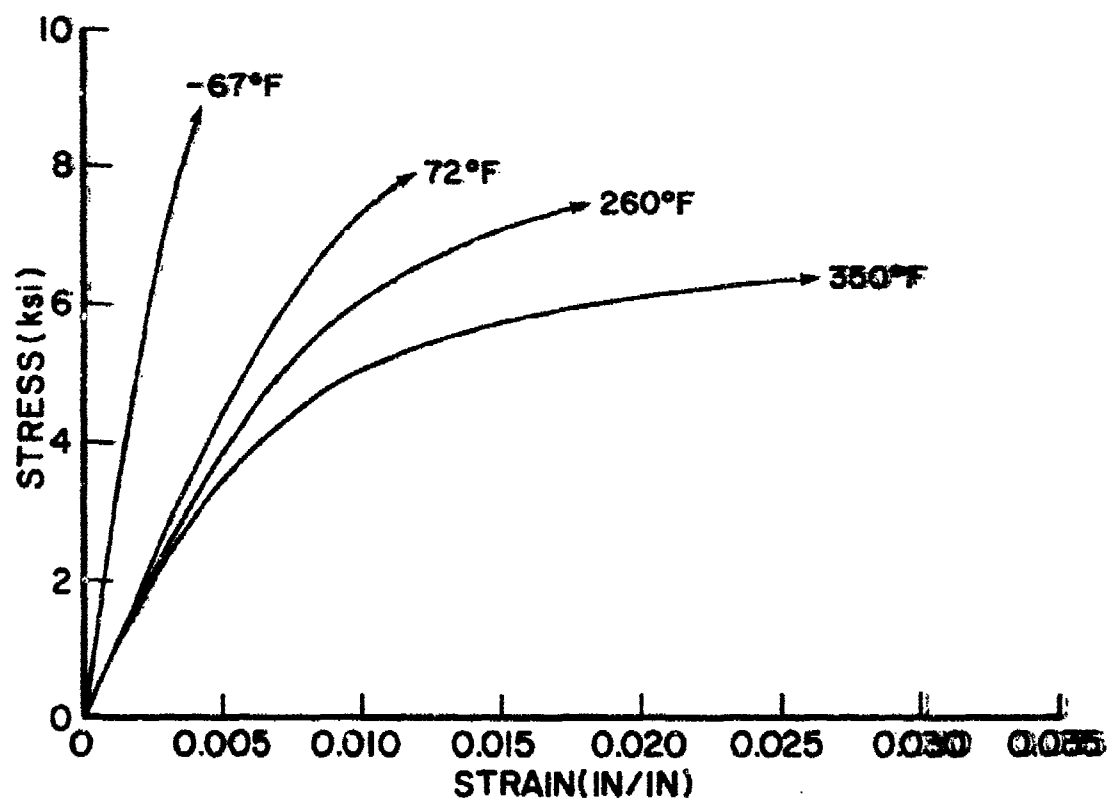


Figure 99. Inplane Shear Stress-Strain Curves for G-160/6535-1 Composite Laminates.

TABLE 83

TENSILE, COMPRESSIVE, AND SHEAR PROPERTIES OF G-160/6535-1 COMPOSITE LAMINATES AFTER HUMIDITY AGING

Composite Material Properties									
Material System - G-160/6535-1				Prepreg by - AVCO		Gr/Epoxy		Condition: 90°	
Fiber - G-160 Matrix - 6535-1				Laminate Sp. Gr. - 1.61					
Maximum Rated Temperature - 350°F				Nominal Ply Thickness - 0.0049 in. (0.12mm)					
Resin Content - 25.4% by wt. (177°C)				No. of panels from which specimens were tested in this table - 5					
Fiber Content - 69.5% by vol.				Aging Conditions - 160°F (71°C) & 100% RH					
Void Content - 5.0%				Tension - 15 ply Comp., - 20 ply					
Thickness of each type specimen:				Shear - 15 ply					
TENSION: 90°									
72°F (22°C)		260°F (127°C)		72°F (22°C)		260°F (127°C)		72°F (22°C)	
Exposure Time (hrs)		216		336		336		166.5	
Wt. Gain(% of orig. dry wt.)		0.67		1.29		1.29		0.62	
Stand. Dev. (%)		0.02		0.01		0.01		0.02	
No. of Specimens		5		5		5		5	
p _{cu} y		[ksi] (MPa)		[2.41] (17)		[2.18] (15)		[20.58] (138)	
Stand. Dev.		[ksi] (MPa)		[0.29] (2)		[0.34] (2)		[1.48] (10)	
Range		[ksi] (MPa)		[1.93-2.62] (13 - 18)		[1.72-2.56] (12 - 18)		[18.37-22.33] (127 - 154)	
No. of Specimens		5		5		5		5	
p _{pl} y		[ksi] (MPa)		[3.64] (26)		[3.71] (22)		[26.59] (182)	
Stand. Dev.		[ksi] (MPa)		[0.33] (2)		[0.26] (2)		[1.50] (10)	
Range		[ksi] (MPa)		[3.32-4.14] (23 - 29)		[3.04] (2)		[3.57] (25)	
No. of Specimens		5		5		5		5	
p _y		[ksi] (MPa)		[3.69] (12)		[3.65] (11)		[11.62] (82)	
Stand. Dev.		[ksi] (MPa)		[0.11] (1)		[0.16] (1)		[0.13] (1)	
Range		[ksi] (MPa)		[3.58] (25)		[3.49] (24)		[10.13] (71)	
No. of Specimens		5		5		5		5	
E _y [in/in] (µm/cm)		2280		1800		1320		29,180 ¹	
Stand. Dev.		179		430		150		12,070	
No. of Specimens		5		5		5		5	
Test Method Reference		Straight-tension		ASTM D3039				ASTM D3410	
Exposure Time (hrs)								91	
Wt. Gain(% of orig. dry wt.)								0.55	
Stand. Dev. (%)								0.08	
No. of Specimens								10	
p _{cu} [ksi] (MPa)								[14.26] (98)	
Stand. Dev.								[0.52] (4)	
Range								[13.56-15.08] (93 - 104)	
No. of Specimens								10	
Test Method Reference								ASTM D2344	

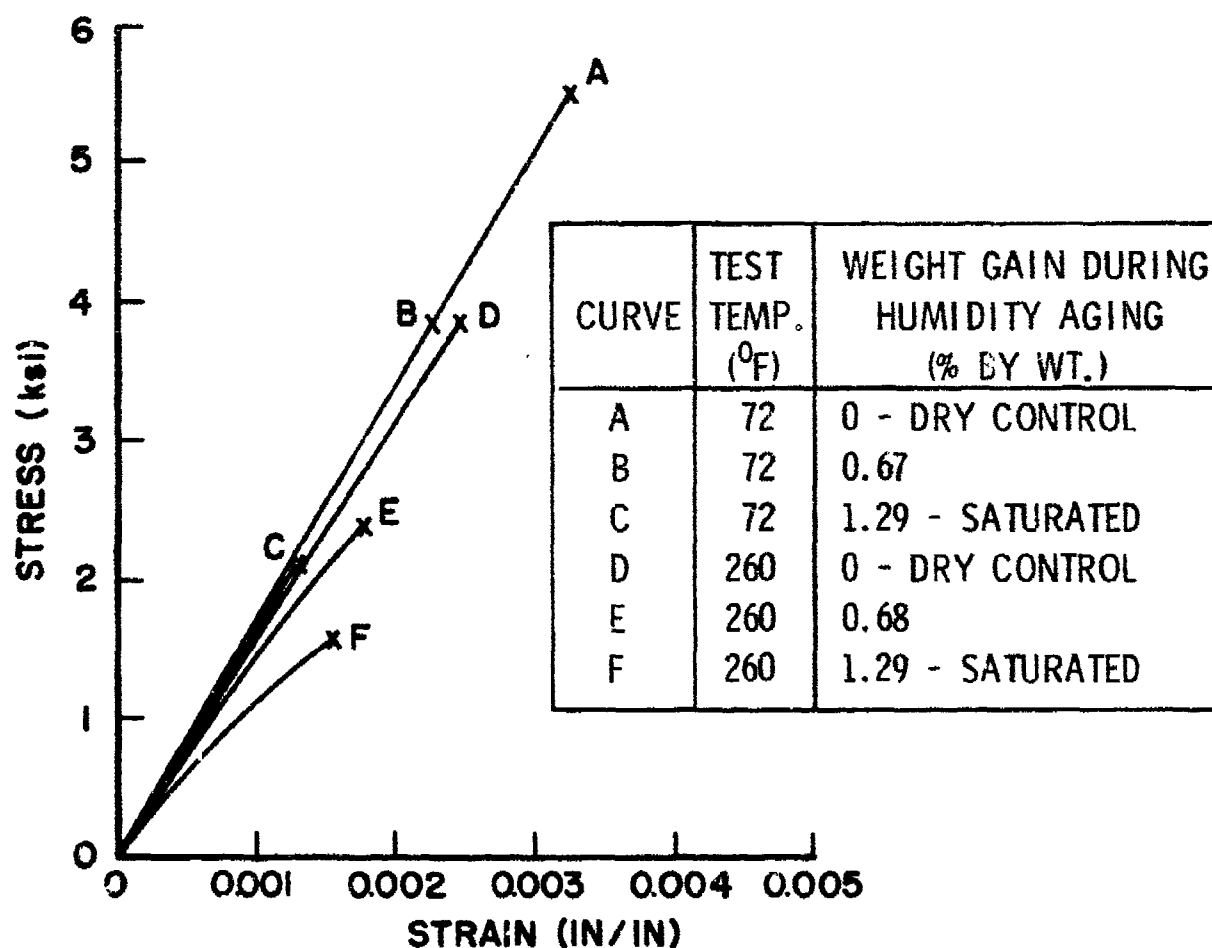
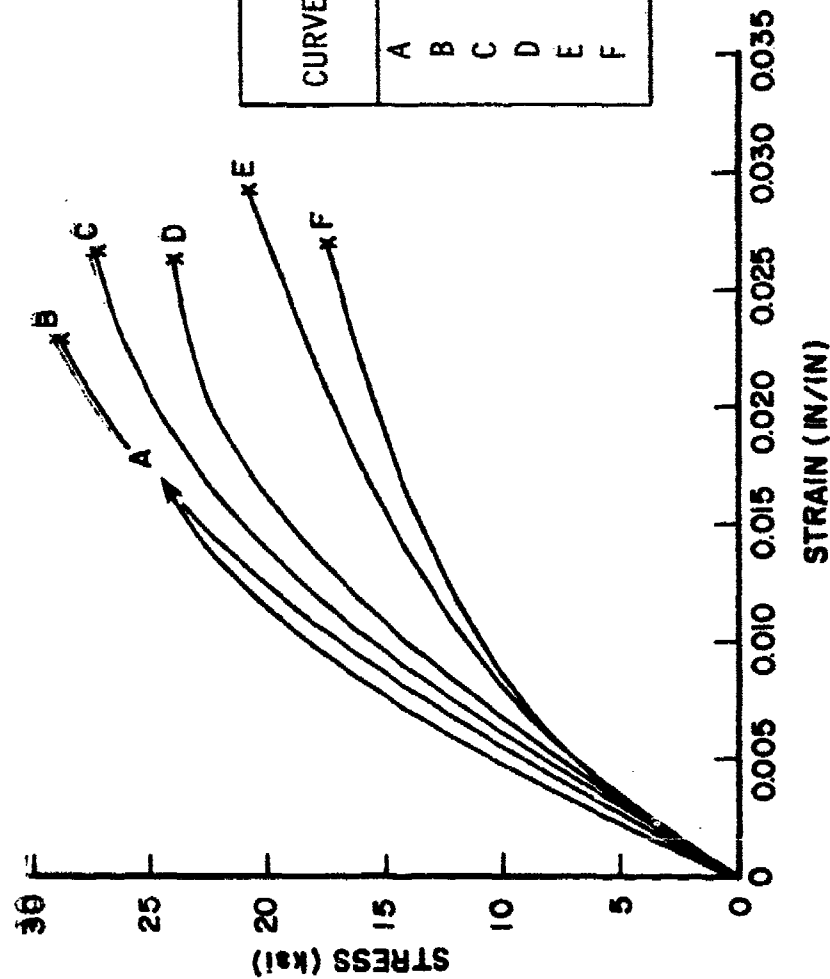


Figure 100. Tensile Stress-Strain Curves for Unidirectional G-160/6535-1 Composite Laminates After Humidity Aging: 90° Fiber Orientation.



CURVE	TEST TEMP. (°F)	WEIGHT GAIN DURING HUMIDITY AGING (% BY WT.)
A	72	0 - DRY CONTROL
B	72	0.62
C	72	1.22 - SATURATED
D	260	0 - DRY CONTROL
E	260	0.63
F	260	1.27 - SATURATED

Figure 101. Compressive Stress-Strain Curves for Unidirectional Composite Laminates After Humidity Aging: 90° Fiber Orientation.

TABLE 84
CREEP PROPERTIES OF G-160/6535-1
COMPOSITE LAMINATES

Composite Material Properties

Material System - G-160/6535-1		Frapreg by - AVCO		Gr/Ep	
Fiber - G-160 Matrix - 6535-1		Laminates Sp. Gr. - 1.61			
Maximum Temperature Rating - 350°F (177°C)		Nominal Ply Thickness - 0.0048 inch (0.12 mm)			
Resin Content - 26.2% by wt.		No. of panels from which specimens were tested in this table - 18			
Fiber Content - 67.8% by vol.		Thickness of each type specimen:			
Void Content - 0% by vol.		+45° - 8 ply		0/+45/90° - 20 ply	
Test Method - straight-sided tension		0/+45° - 16 ply		0/+45/90° - 20 ply	
Reference - ASTM D2290 and D3039					
CREEP					
Temperature	Fiber Orientation	+45°	0/+45°	0/+45/90°	0/+45/90°
72°F (22°C)	Stress Level [ksi] (MPa)	[13.22] (91)	[73.22] (504)	[72.70] (501)	[77.83] (536)
	Creep Strain, 500 hr (%)	0.2897	0.0073	0.0164	0.0102
	No. of Specimens	3	2 ⁶	2 ⁶	2 ⁶
	Residual Strength [ksi] (MPa)	[18.17] (125)	[108.40] (747)	[109.84] (757)	[113.85] (784)
	No. of Specimens	3	2	2	2
	Stress Level [ksi] (MPa)	[11.57] (80)	[64.07] (441)	[63.62] (438)	[68.10] (469)
	Creep Strain, 500 hr (%)	0.2031	0.0171	0.0148	0.0122
	No. of Specimens	3	3	3	3
	Residual Strength [ksi] (MPa)	[19.30] (133)	[103.46] (713)	[112.20] (773)	[107.24] (739)
	No. of Specimens	3	3	3	3
	Stress Level [ksi] (MPa)	[9.92] (68)			
	Creep Strain, 500 hr (%)	0.1124			
	No. of Specimens	3			
	Residual Strength [ksi] (MPa)	[19.24] (133)			
	No. of Specimens	3			
260°F (127°C)	Stress Level [ksi] (MPa)	[12.45] (86)			
	Creep Strain, 500 hr (%)	---			
	No. of Specimens	3			
	Residual Strength [ksi] (MPa)	[14.68] (101)			
	No. of Specimens	2 ⁶			
	Stress Level [ksi] (MPa)	[10.89] (75)			
	Creep Strain, 500 hr (%)	3424 ¹			
	No. of Specimens	2			
	Residual Strength [ksi] (MPa)	[16.39] (113)			
	No. of Specimens	2 ⁶			
	Stress Level [ksi] (MPa)	[9.44] (65)			
	Creep Strain, 500 hr (%)	0.2520			
	No. of Specimens	3			
	Residual Strength [ksi] (MPa)	[16.25] (112)			
	No. of Specimens	3			
350°F (177°C)	Stress Level [ksi] (MPa)	[11.54] (80)			
	Creep Strain, 500 hr (%)	1.9939			
	No. of Specimens	1 ⁵			
	Residual Strength [ksi] (MPa)	[16.01] (110)			
	No. of Specimens	3			
	Stress Level [ksi] (MPa)	[9.89] (68)			
	Creep Strain, 500 hr (%)	2.3224			
	No. of Specimens	1 ⁵			
	Residual Strength [ksi] (MPa)	[17.01] (117)			
	No. of Specimens	3			
	Stress Level [ksi] (MPa)	[8.24] (57)			
	Creep Strain, 500 hr (%)	1.7352			
	No. of Specimens	1 ⁶			
	Residual Strength [ksi] (MPa)	[15.88] (109)			
	No. of Specimens	1			

¹(0,45,-45,0,0,-45,45,0)₈-16 ply

²(0,45,-45,0,0,-45,45,0,90,0)₈-20 ply

³(0,90,45,-45,0,0,-45,45,0,0)₈-20 ply

⁴Strain gauges failed on three specimens during test.

⁵Strain gauges failed on two specimens during test.

⁶One specimen failed during test.

⁷One specimen overheated.

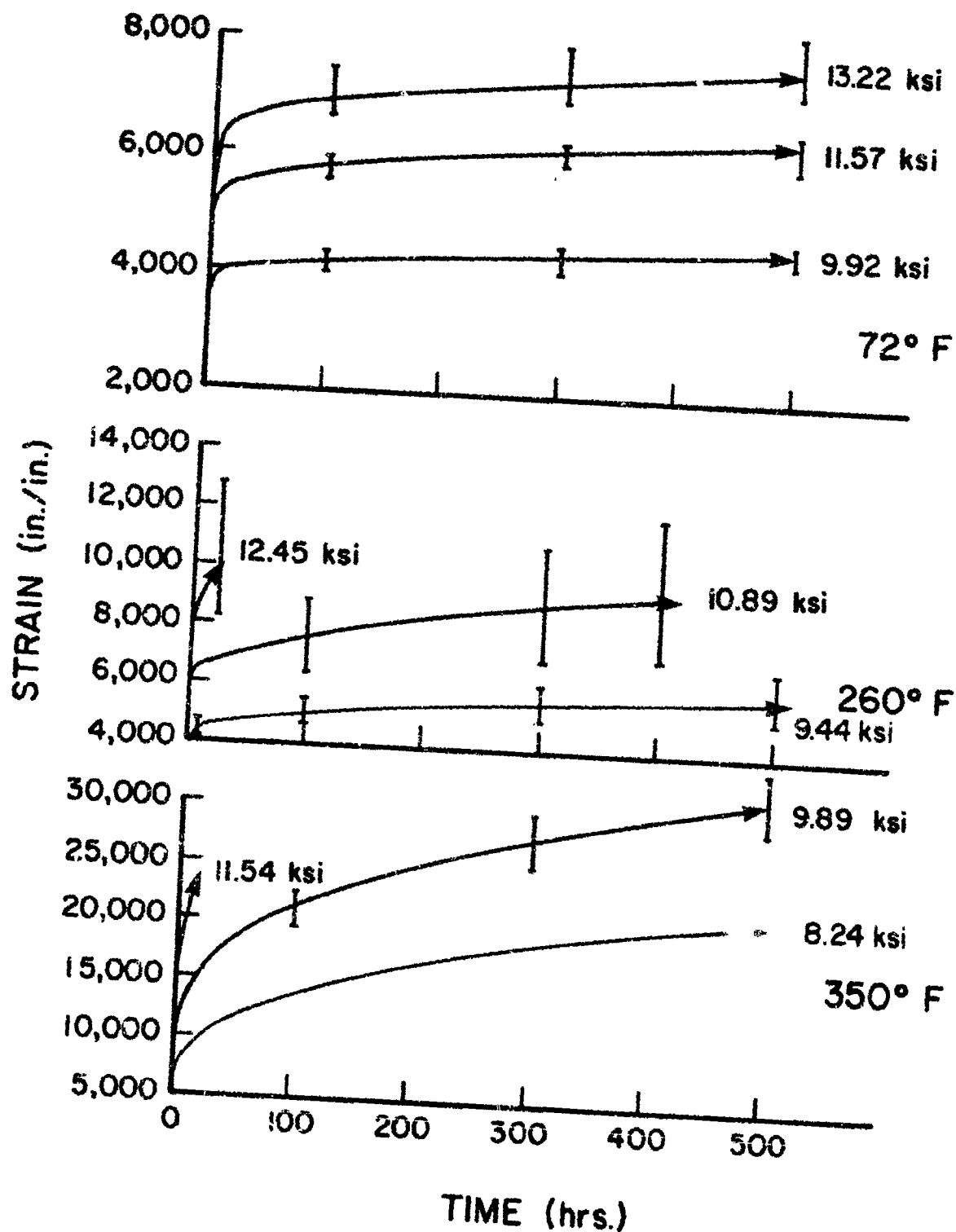


Figure 102. Tensile Creep Behavior of G-160/6535-1 Composite Laminates: $\pm 45^\circ$ Fiber Orientation.

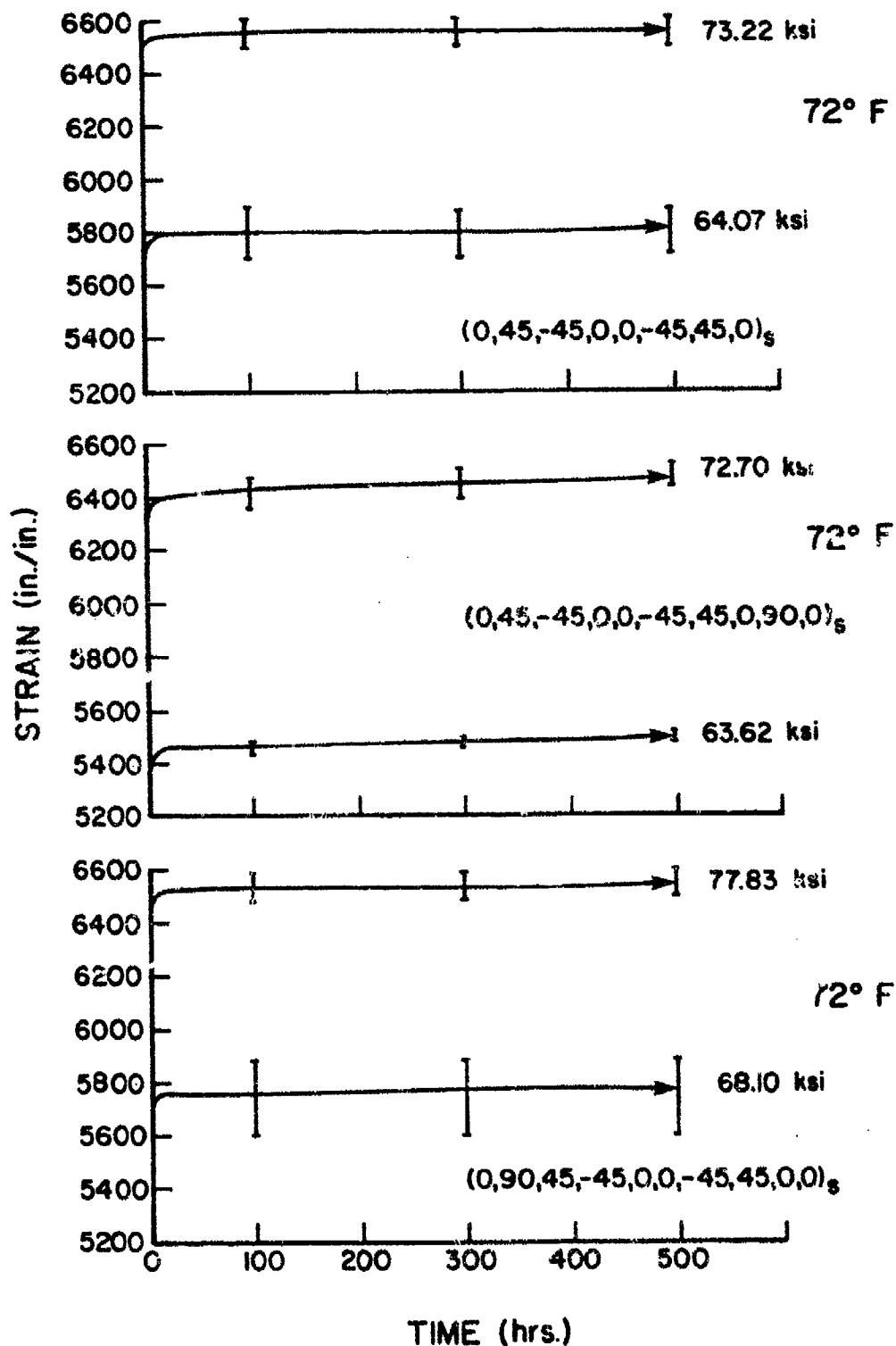


Figure 103. Tensile Creep Behavior of Multidirectional G-160/6535-1 Composite Laminates.

TABLE 85
STRESS-RUPTURE BEHAVIOR OF G-160/6535-1
COMPOSITE LAMINATES

Composite Material Properties					
Material System - G-160/6535-1		Prepreg by - AVCO		Gr/Ep	
Fiber - G-160 Matrix - 6535-1		Laminate Sp. Gr. - 1.61			
Maximum Temperature Rating - 350°F(177°C)		Nominal Ply Thickness - 0.0048 inch(0.12 mm)			
Resin Content - 26.2% by wt.		No. of panels from which specimens were tested in this table -			
Fiber Content - 67.8% by vol.		Thickness of each type specimen:			
Void Content - ± 0% by vol.		+45 - 8 ply 0/+45/90 ² - 20 ply			
Test Method - Straight-sided tension		0/+45 ¹ - 16 ply 0/+45/90 ³ - 20 ply			
Reference - ASTM D2290 and D3039					
STRESS RUPTURE					
Temperature	Fiber Orientation	+45	0/+45 ¹	0/+45/90 ²	0/+45/90 ³
72°F(22°C)	Stress Level[ksi](MPa)	[13.22](91)	[73.22](504)	[72.70](501)	[77.83](536)
	Time to Failure(hrs)	500+	369+	333+	333+
	No. of Specimens	3	3	3	3
	Residual Strength[ksi](MPa)	[18.17](125)	[108.40](747)	[109.84](757)	[113.85](784)
	No. of Specimens	3	2	2	2
	Stress Level[ksi](MPa)	[11.57](80)	[64.07](441)	[63.62](438)	[68.10](469)
	Time to Failure(hrs)	503+	510+	503+	503+
	No. of Specimens	3	3	3	3
	Residual Strength[ksi](MPa)	[19.30](133)	[103.46](713)	[112.20](773)	[107.24](739)
	No. of Specimens	3	3	3	3
260°F(127°C)	Stress Level[ksi](MPa)	[12.45](86)			
	Time to Failure(hrs)	351+			
	No. of Specimens	3			
	Residual Strength[ksi](MPa)	[14.68](101)			
	No. of Specimens	2			
	Stress Level[ksi](MPa)	[10.89](75)			
	Time to Failure(hrs)	482+			
	No. of Specimens	3			
	Residual Strength[ksi](MPa)	[16.39](113)			
	No. of Specimens	2			
350°F(177°C)	Stress Level[ksi](MPa)	[11.54](80)			
	Time to Failure(hrs)	500+			
	No. of Specimens	3			
	Residual Strength[ksi](MPa)	[16.01](110)			
	No. of Specimens	3			
	Stress Level[ksi](MPa)	[9.89](68)			
	Time to Failure(hrs)	500+			
	No. of Specimens	3			
	Residual Strength[ksi](MPa)	[17.01](117)			
	No. of Specimens	3			

¹(0,45,-45,0,0,-45,45,0)_g - 16 ply
²(0,45,-45,0,0,-45,45,0,90,0)_g - 20 ply
³(0,90,45,-45,0,0,-45,45,0,0)_g - 20 ply

TABLE 86

**TENSILE-TENSILE FATIGUE PROPERTIES
OF G-160/6535-1 COMPOSITE LAMINATES**

Composite Material Properties					
Material System - G-160/6535-1		Prepreg by - AVCO		Gr/2r	
Fiber - G-160 Matrix - 6535-1		Laminate Sp. Gr. - 1.61			
Maximum Temperature Rating - 350°F(177°C)		Nominal Ply Thickness - 0.0048 inch (0.12 mm)			
Resin Content - 36.2% by wt.		No. of panels from which specimens were tested in this table - 18			
Fiber Content - 67.8% by vol.		Thickness of each type specimen:			
Void Content - ± 0% by vol.		+45 - 8 ply 0/+45/90° - 20 ply			
Test Method - Straight-sided tension		0/+45° - 16 ply 0/+45/90° - 20 ply			
Reference - ASTM D3039					
TENSILE FATIGUE, R=0.1					
Temperature	Fiber Orientation	+45	0/+45 ¹	0/+45/90 ²	0/+45/90 ³
72°F(22°C)	Max. Stress[ksi](MPa)	[14.05](97)	[87.55](603)	[86.39](595)	[77.79](536)
	Lifetime (cycles)	4,603	1,259	962	1,767
	No. of Specimens	5	5	5	5
	Residual Strength[ksi](MPa)	---	---	---	---
	No. of Specimens	0	0	0	0
	Max. Stress[ksi](MPa)	[12.40](85)	[82.69](570)	[81.79](564)	[73.22](504)
	Lifetime (cycles)	69,314	22,478	47,309	99,022
	No. of Specimens	5	5	5	5
	Residual Strength[ksi](MPa)	---	---	---	---
	No. of Specimens	0	0	0	0
	Max. Stress[ksi](MPa)	[10.74](74)	[77.82](536)	[77.25](532)	[68.64](473)
	Lifetime (cycles)	719,082	45,079	154,164	125,270
	No. of Specimens	5	5	5	5
	Residual Strength[ksi](MPa)	---	---	---	---
	No. of Specimens	0	0	0	0
260°F(127°C)	Max. Stress[ksi](MPa)	[13.23](91)			
	Lifetime (cycles)	3,438			
	No. of Specimens	5			
	Residual Strength[ksi](MPa)	---			
	No. of Specimens	0			
	Max. Stress[ksi](MPa)	[10.89](75)			
	Lifetime (cycles)	138,999			
	No. of Specimens	5			
	Residual Strength[ksi](MPa)	---			
	No. of Specimens	0			
	Max. Stress[ksi](MPa)	[8.56](59)			
	Lifetime (cycles)	3,640,227			
	No. of Specimens	5			
	Residual Strength[ksi](MPa)	---			
	No. of Specimens	0			

¹(0,45,-45,0,0,-45,45,0)_s - 16 ply²(0,45,-45,0,0,-45,45,0,90,0)_s - 20 ply³(0,90,45,-45,0,0,-45,45,0,0)_s - 20 ply

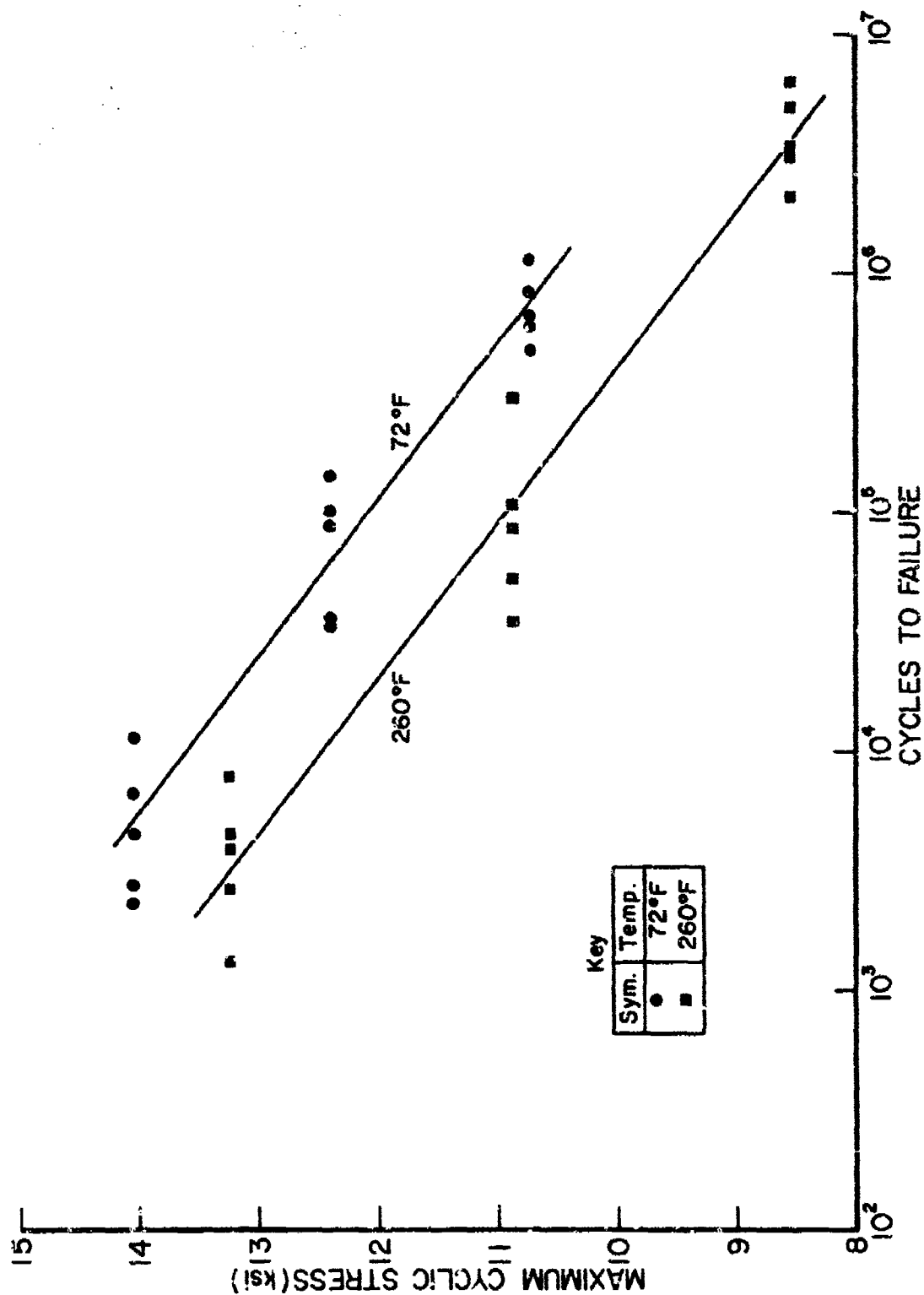


Figure 104. Tensile-Tensile Fatigue Behavior of Bidirectional G-160/6535-1 Composite Laminates: +45° Fiber Orientation.

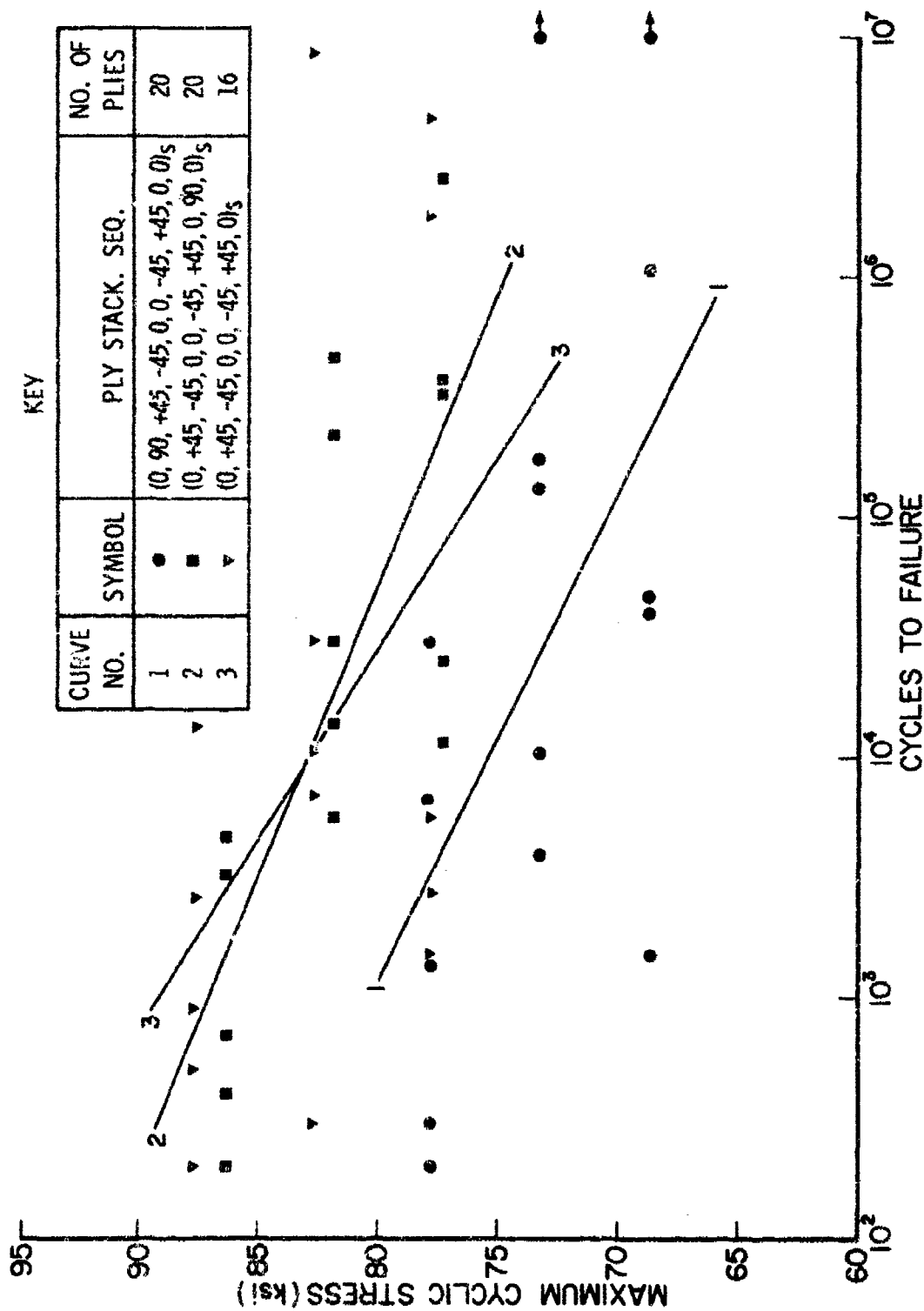


Figure 105. Tensile-Tensile Fatigue Behavior of Multidirectional G-160/6535-1 Composite Laminates.

TABLE 87
THERMOPHYSICAL PROPERTIES OF G-160/6535-1
COMPOSITE LAMINATES

Composite Material Properties					
Material System - G-160/6535-1		Prepreg by - AVCO		Gr/Epoxy	
Fiber - G-160 Matrix - 6535-1		Laminate Sp. Gr. - 1.61			
Maximum Temperature Rating - 350°F(177°C)		Average Ply Thickness - 0.0048 inch(0.12 mm)			
Resin Content - 25.5% by wt.		No. of panels from which specimens were tested			
Fiber Content - 68.5% by vol.		in this table - 3			
Void Content - ± 0% by vol.					
Thickness of each type specimen:		Therm. Exp. - 40 ply		Spec. Ht. - 1 ply	
		Therm. Cond. -40 ply		Glass Trans. -8 ply	
THERMOPHYSICAL PROPERTIES: 0°					
	-67°F(-55°C)	72°F(22°C)	260°F(127°C)	350°F(177°C)	Test Method
Thermal Expansion ¹					TMA ²
α_x [μin/in-°F] (μcm/cm-°C)	[0.04] (0.08)	[-0.21] (±0.37)	[-0.21] (±0.38)	[-0.10] (±0.20)	
α_y [μin/in-°F] (μcm/cm-°C)	[12.5] (22.5)	[13.8] (24.8)	[16.7] (30.0)	[18.0] (32.4)	
No. of Specimens per direction	3	3	3	3	
Specific Heat					DSC ³
C_p [btu/lb.-°F] (J/kg-°C)	[0.154] (644)	[0.202] (845)	[0.281] (1175)	[0.333] (1393)	
No. of Specimens	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.23] (0.40)	[0.38] (0.66)	[0.57] (0.99)	[0.66] (1.14)	
No. of Specimens	3	3	3	3	
Glass Transition Temp.					DMA ⁴
Dry [°F] (°C)	[507] (264)				
Wet [°F] (°C)	[471] (244)				
THERMOPHYSICAL PROPERTIES: +45°					
Thermal Expansion ¹					TMA ²
α_x [μin/in-°F] (μcm/cm-°C)	[1.63] (2.93)	[1.37] (2.46)	[1.24] (2.24)	[1.41] (2.54)	
No. of Specimens per direction	3	3	3	3	
Thermal Conductivity ¹					Comparative
k_z [btu-ft/ft ² -hr-°F] (W/m-°C)	[0.37] (0.64)	[0.43] (0.74)	[0.51] (0.88)	[0.55] (0.95)	
No. of Specimens	3	3	3	3	

- NOTES: 1. On the unidirectionally reinforced specimens, the x-direction is along the fiber axis, the y-direction is across the fiber axis, and the z-direction is through the thickness (identical to the y-direction). On +45° bidirectionally reinforced specimens, the x and y directions are identical and oriented at 45° to either fiber direction, while the z-direction is through the thickness.
2. Thermo-mechanical Analysis.
3. Differential Scanning Calorimetry.
4. Dynamic Mechanical Analysis.

4.7 COMPARATIVE ENVIRONMENTAL BEHAVIOR

One of the points of particular interest relative to the data generated in this program is the comparative susceptibility of the different composite materials to degradation during, or as the result of, elevated temperature, high humidity aging. Figures 106 through 108 illustrate the effect of both test temperature and moisture absorption upon the strength retention of these composite materials. The notations "saturated" and "50% saturated", recall, refer to the specimen condition just prior to testing. As discussed in Section 3.4, the specimens tested at elevated temperature undoubtedly dry out to some extent during the testing process, with the smaller specimens (shear and compression) drying out more rapidly than the larger tensile specimens.

Additionally, use of the description, "50% saturated", refers to the partial saturation condition. While the aging periods were selected so as to effect about 50% as much moisture absorption as is present at equilibrium, the actual levels of partial saturation range from 45-67% of the fully saturated levels. Further, it must be recognized that while a specimen permitted to reach an equilibrium saturation condition may have a relatively uniform moisture concentration throughout its thickness, one only "50% saturated" will have most of that moisture concentrated near the surfaces.

Several features in Figures 106-108 stand out. First, the strength levels for the HyE 2034D system (employing the 75 Msi [517 GPa], pitch-based graphite fiber) are lower for every type of test and for every temperature and moisture level than any of the other materials. This is probably due to a lower level of interfacial bonding between this particular reinforcing fiber and the 934 epoxy matrix. Relative to the strength levels in the dry material, the HyE 2034D system loses the least strength due to absorbed moisture of any of the other five materials. This, however, is probably the result

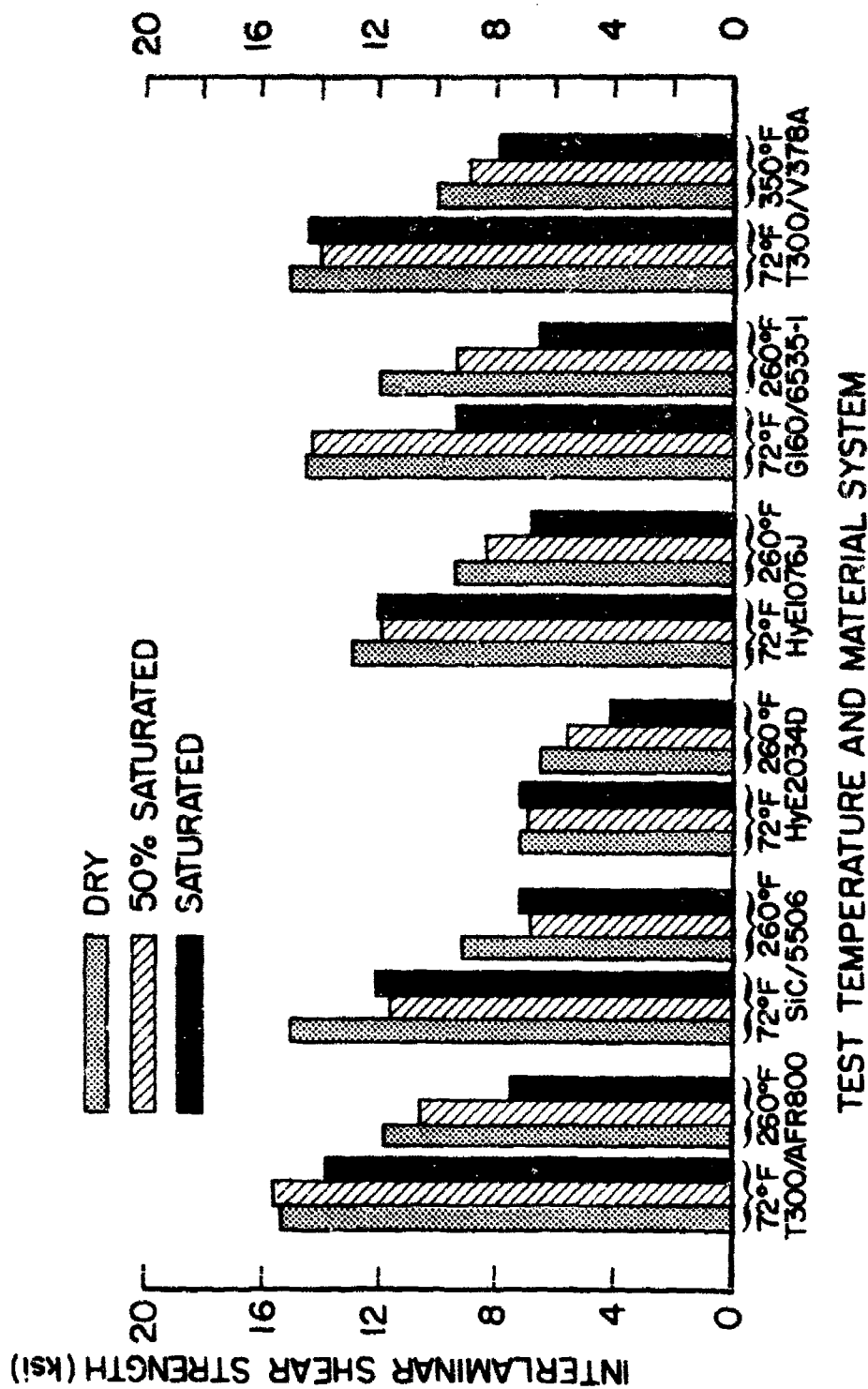


Figure 108. Comparative Interlaminar Shear Strength Retention After Aging at 160°F (71°C) and 100% Relative Humidity.

of the original below average interfacial bond strengths since the wet strength levels of the other epoxy-matrix systems are comparable to the dry strength level of the HyE 2034D.

Second, while the SiC/5506 system loses the most strength, relative to the dry state, of any of the materials tested, its absolute strength levels in 90° tension are clearly the highest and its absolute strength levels in 90° compression and interlaminar shear are comparable to the other materials.

In those instances in which a more saturated condition resulted in a higher strength than a less saturated condition, the difference is small enough to be attributable to experimental scatter.

While the fact that the T300/V378A system (polyimide) was tested at 350°F (177°C) rather than 260°F (127°C) makes it less than straightforward to compare it directly with the other five systems (all epoxy), it would appear, with the possible exception of the 350°F (177°C) saturated condition, that this material suffers less degradation due to moisture absorption than any of the other materials tested.

Elevated temperature, high humidity agings similar to those conducted during this program were previously carried out on two other polyimide systems, AS/4397 by Hercules, and T300/F178 by Hexcel, and reported in AFML-TR-77-151.[14] Comparison of the 90° tension and interlaminar shear data (both dry and humidity aged) of these two materials with that for the T300/V378A system reveals that the latter material exhibits generally equivalent or superior strength levels to either of the two systems tested earlier. This in spite of the fact that the latter material had a void content of about 0.8% while the two earlier materials were void free.

SECTION 5

CONCLUSIONS

Each of the conclusions listed in this section was arrived at through inspection of the data in Section 4 and represent generalizations of overall composite behavior. Exceptions to each of these generalized conclusions can be found if the data are scrutinized in sufficient detail. In most cases, these exceptions are at least mentioned and discussed.

1. The static strengths (tensile, compressive, flexural, inplane, and interlaminar shear) of each material evaluated in this program decreased with increasing test temperature. In those cases where this was not true, the exception usually proved to be either in a tensile specimen dominated by 0° plies, or at -67°F (-55°C). The latter situation most probably is due to increased sensitivity to brittle failure at the lower temperature.
2. In those cases where the elastic modulus is primarily fiber dependent, the test temperature had relatively little effect on the modulus (0° tension, 0/+45/90 tension, 0° compression, 0° flexure). In those cases where the composite modulus is primarily matrix dependent, however, the modulus for each material decreased with increasing temperature just as the strengths did.
3. The ultimate elongations of the fiber dependent specimens behaved in roughly the same fashion as the strength, and with the same exceptions. The ultimate elongations of the matrix dependent specimens (90° and +45° tension and 90° compression) increased with increasing temperature for any specific stress. Since the ultimate stress for these specimens, however, was simultaneously decreasing, the actual ultimate elongations for these type specimens exhibited some increases and some decreases with increasing test temperature.

4. On those systems in which holes were drilled in the center of the multidirectional tensile specimens, the static tensile strength was 76-80% of what it would have been had it followed the reduction in cross-sectional area directly. This reduction is probably due to the creation of a stress concentration around the hole (diameter = $0.1935 \times$ width of specimen).
5. On the last material tested, the presence, absence, and location of a 90° ply in the layup stack was varied because of its influence on normal edge stresses. The static tensile results indicated that the layup with a low level of normal edge stress produces a slightly higher tensile strength, while the layups which produce large tensile and large compressive edge stresses produce equivalent, and slightly lower tensile strengths. In fatigue, the layup which produces large tensile edge stresses and the stress-free layup exhibit longer lifetimes, for equivalent cyclic stress levels, than the layup which produced large compressive edge stresses. The former two layups (stress-free and tensile edge stress) exhibit comparable fatigue behavior. The difference in slope may be insignificant considering the limited amount of available data and the degree of scatter.
6. The thermal conductivity and specific heat increased with increasing temperature for all six systems.
7. The coefficient of thermal expansion (CTE) seemed relatively independent of temperature for the four systems incorporating high strength graphite fiber. On the HyE 2034D system, however, incorporating a high

modulus graphite fiber, the CTE decreased with increasing temperature while the system incorporating silicon carbide fiber exhibited an increasing CTE with temperature.

8. On all of the graphite reinforced systems, the layups incorporating 0° plies exhibited considerable scatter in fatigue lifetimes. The silicon carbide reinforced system, on the other hand, exhibited much less scatter in fatigue lifetimes on layups incorporating 0° plies. Along with the greater scatter in the graphite systems, however, these systems exhibited considerably longer fatigue lifetimes than the silicon carbide system at comparable cyclic stress levels.

For the $\pm 45^\circ$ orientations, there was relatively little scatter on any of the materials. For this orientation, the high strength graphite systems again exhibit considerably longer fatigue lifetimes than the silicon carbide system for comparable cyclic stress levels. The high modulus graphite system outperforms the silicone carbide system in fatigue for the $\pm 45^\circ$ orientation if the cyclic stress levels are converted to percent of static tensile strength.

9. The relatively large plastic strains undergone by the $\pm 45^\circ$ orientation led, in some cases, to substantial internal energy dissipation and self-heating in fatigue tests. For the materials tested here, this self heating caused typical temperature increases in $\pm 45^\circ$ orientations of $8-20^\circ\text{F}$ ($4-11^\circ\text{C}$) for cyclic stress levels in the range of 60-85% of the static ultimate. There were some specimens of course that exhibited practically no self heating while others exhibited temperature rises of up to 40°F (22°C).

10. Probably the most unusual thing observed in the creep testing was the tendency of some of the multidirectional layups (0/+45/90), particularly at elevated temperature and with the high modulus graphite fiber, to exhibit contraction rather than extension. This was not observed with the silicon carbide system. It may be attributable to the gradual relief of residual internal stresses resulting from laminate fabrication.

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APPENDIX A

COMPUTATION OF NORMAL EDGE STRESSES

It is well known that a flat composite laminate which is subjected to a basically in-plane system of loads can develop normal interlaminar stresses near free edges that are sufficient to cause delamination. This phenomenon occurs because a composite laminate is not a two-dimensional structure at all, but is a complex, non-homogeneous, three-dimensional system. In a macromechanical sense a composite laminate distributes loads much like a plate composed of a single homogeneous material. In the center of a laminate structure, at points distant from boundaries and points of load applications, the macromechanics theory of composites is sufficient to represent the state of stress accurately. However, near boundaries such as the free edges of a tension specimen, the state of stress is three-dimensional and depends on the laminate stacking sequence. In particular, interlaminar normal stresses at a free edge can be so affected by stacking sequence that changes in sign may occur simply by rearranging the layers.

This Appendix presents a brief discussion of the procedure used for analytically determining the interlaminar normal edge stresses in a composite tensile specimen. The method involves the following two steps:

- (1) Computation of the nominal stresses in each layer using macromechanics composite theory, as presented in References 15 and 16, and;
- (2) Estimation of the normal stresses between individual lamina, according to the method presented in References 17-19.

These analysis steps are discussed individually below in Sections A.1 and A.2. Section A.3 contains interlayer normal stresses computed for example composite tensile layups of various materials.

A.1 LAYER STRESSES

The nominal layer stresses in a composite laminate are computed by means of standard macromechanics theory. For completeness, the relevant equations are presented below for a general laminated composite; the special case of narrow test specimens with free edges will be considered in Section A.2

A.1.1 Stress Resultants

It is presumed that a stress analysis has been performed on a composite plate (we will specialize to the case of a tension specimen in Section A.2) referred to a two-dimensional Cartesian coordinate system x,y ; that is, at every point x,y , the in-plane stress resultants N_x , N_y , N_{xy} and the moment stress resultants M_x , M_y , M_{xy} have been determined (by plate theory, from a finite element analysis, by experimentation, etc.). These stress resultants arise from a system of mechanical and thermal loads, and they act at a reference plane (usually the middle surface) with the positive conventions shown in Figure A-1.

A.1.2 Lamina Properties

The x,y coordinate system of Figure A-1 is referred to as the structural axes. An individual lamina is referred to a 1,2 set of material axes as shown in Figure A-2. The lamina fibers are oriented along the material 1-axis which is measured relative to the structural x -axis by the angle θ . The in-plane material properties of the lamina are referred to by:

Moduli of elasticity: E_1, E_2

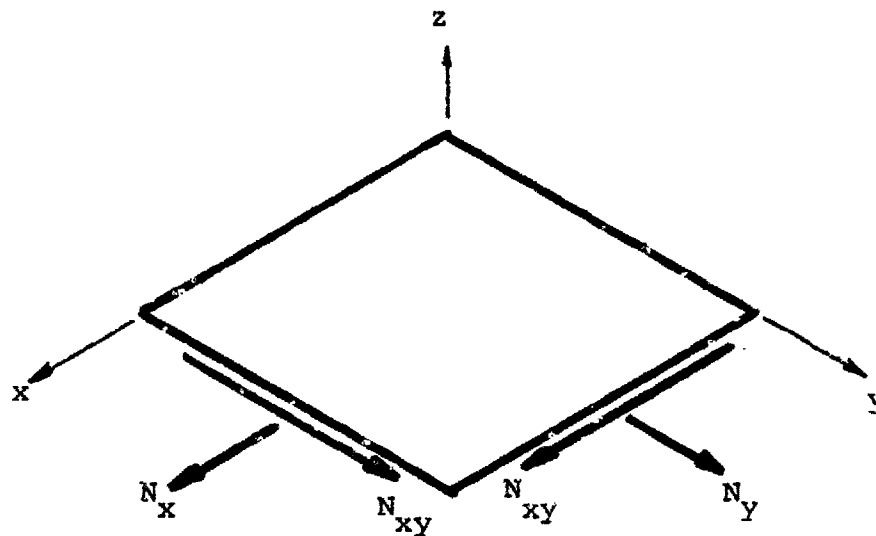
Poisson's Ratio : $\nu_{12}, \nu_{21} = \frac{E_2}{E_1} \nu_{12}$

Shear Modulus : G_{12}

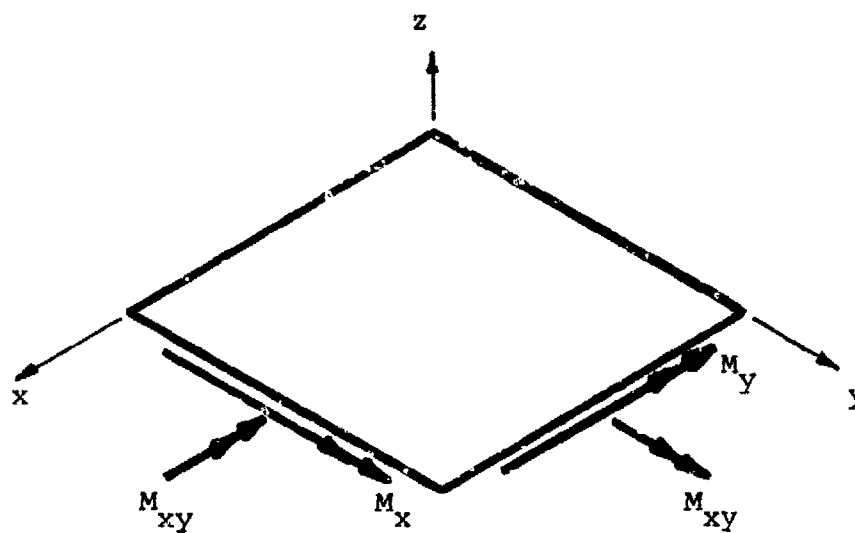
Thermal Coefficients: α_1, α_2

The stress-strain relationship for the lamina is written as

$$\begin{Bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_{12} \end{Bmatrix} = [Q] \begin{Bmatrix} \epsilon_1 - \alpha_1 \Delta T \\ \epsilon_2 - \alpha_2 \Delta T \\ \epsilon_{12} \end{Bmatrix} \quad (A.1)$$



Membrane Stress Resultants



Bending Stress Resultants

Figure A-1. Stress Resultants at the Mid-Surface of a Composite Laminate.

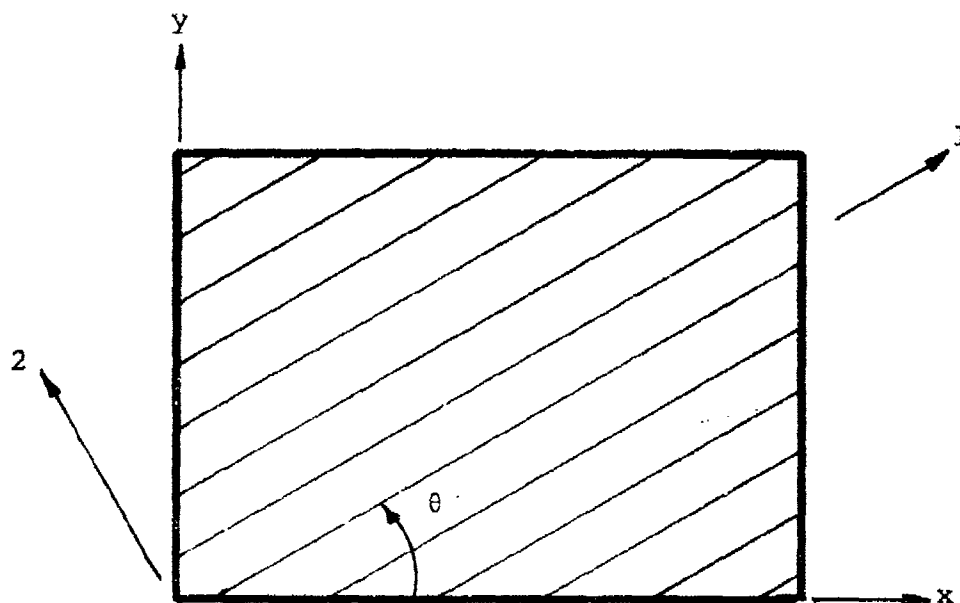


Figure A-2. Typical Lamina.

where ΔT is a change in temperature, and

$$[Q] = \begin{bmatrix} Q_{11} & Q_{12} & 0 \\ Q_{21} & Q_{22} & 0 \\ 0 & 0 & Q_{66} \end{bmatrix} \quad (A.2)$$

where,

$$\begin{aligned} Q_{11} &= \frac{E_1}{1 - \nu_{12} \nu_{21}} \\ Q_{22} &= \frac{E_2}{1 - \nu_{12} \nu_{21}} \\ Q_{12} &= Q_{21} = \frac{\nu_{12} E_2}{1 - \nu_{12} \nu_{21}} = \frac{\nu_{21} E_1}{1 - \nu_{12} \nu_{21}} \\ Q_{66} &= G_{12} \end{aligned} \quad (A.3)$$

If the lamina material properties are referred to the structural axes rather than the material axes, the following transformations are performed:

$$[\bar{Q}] = [T]^{-1} [Q] [T]^{-T} \quad (A.4)$$

$$\begin{pmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{pmatrix} = [T]^T \begin{pmatrix} \alpha_1 \\ \alpha_2 \\ 0 \end{pmatrix} \quad (A.5)$$

where the transformation matrix is given by

$$[T] = \begin{bmatrix} \cos^2 \theta & \sin^2 \theta & 2 \sin \theta \cos \theta \\ \sin^2 \theta & \cos^2 \theta & -2 \sin \theta \cos \theta \\ -\sin \theta \cos \theta & \sin \theta \cos \theta & \cos^2 \theta \sin^2 \theta \end{bmatrix} \quad (A.6)$$

and its inverse is,

$$[T]^{-1} = \begin{bmatrix} \cos^2\theta & \sin^2\theta & -2\sin\theta\cos\theta \\ \sin^2\theta & \cos^2\theta & 2\sin\theta\cos\theta \\ \sin\theta\cos\theta & -\sin\theta\cos\theta & \cos^2\theta - \sin^2\theta \end{bmatrix} \quad (A.7)$$

A.1.3 Laminate Properties

Consider a laminate formed by stacking individual laminae as shown in Figure A-3. A typical lamina is referred to by "k". For example, the thickness of layer k is h_k and the transformed material property matrix is $[\bar{Q}]_k$.

The stress-strain relationship for a laminate in terms of the reference surface stress resultants (N_x , N_y , N_{xy} , M_x , M_y , M_{xy}) computed as indicated in Section A.1, and the reference surface strains (ϵ_{xo} , ϵ_{yo} , γ_{xyo}) and curvatures (κ_x , κ_y , κ_{xy}) is given by

$$\begin{bmatrix} A_{11} & A_{12} & A_{16} & | & B_{11} & B_{12} & B_{66} \\ A_{12} & A_{22} & A_{26} & | & B_{12} & B_{22} & B_{26} \\ A_{16} & A_{26} & A_{66} & | & B_{16} & B_{26} & B_{66} \\ \hline B_{11} & B_{12} & B_{16} & | & D_{11} & D_{12} & D_{16} \\ B_{12} & B_{22} & B_{26} & | & D_{12} & D_{22} & D_{26} \\ B_{16} & B_{26} & B_{66} & | & D_{16} & D_{26} & D_{66} \end{bmatrix} \begin{bmatrix} \epsilon_{xo} \\ \epsilon_{yo} \\ \gamma_{xyo} \\ \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{bmatrix} = \begin{bmatrix} N_x \\ N_y \\ N_{xy} \\ M_x \\ M_y \\ M_{xy} \end{bmatrix} + \begin{bmatrix} N_{xt} \\ N_{yt} \\ N_{xyt} \\ M_{xt} \\ M_{yt} \\ M_{xyt} \end{bmatrix} \Delta T \quad (A.8)$$

where the composite material properties are determined by

$$\begin{aligned} A_{ij} &= \sum_{k=1}^N (\bar{Q}_{ij})_k (z_k - z_{k-1}) \\ B_{ij} &= \frac{1}{2} \sum_{k=1}^N (\bar{Q}_{ij})_k (z_k^2 - z_{k-1}^2) \\ D_{ij} &= \frac{1}{3} \sum_{k=1}^N (\bar{Q}_{ij})_k (z_k^3 - z_{k-1}^3) \end{aligned} \quad (A.9)$$

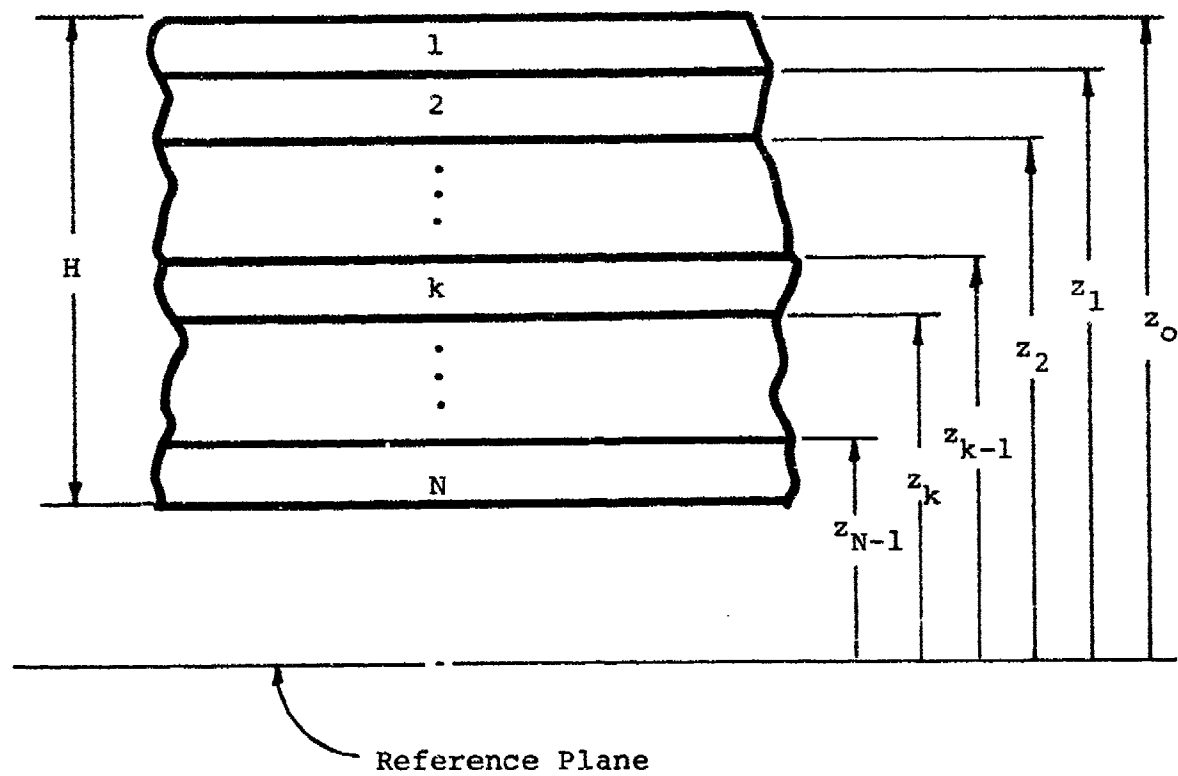


Figure A-3. Composite Laminate.

and the stress resultants due to thermal change are,

$$\begin{pmatrix} N_{xt} \\ N_{yt} \\ N_{xyt} \end{pmatrix} = \Delta T \sum_{k=1}^N \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{pmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{pmatrix}_k (z_k - z_{k-1}) \quad (\text{A.10})$$

$$\begin{pmatrix} M_{xt} \\ M_{yt} \\ M_{xyt} \end{pmatrix} = \frac{\Delta T}{2} \sum_{k=1}^N \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{pmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{pmatrix}_k (z_k^2 - z_{k-1}^2)$$

A.1.4 Strain and Stress in the Laminae

The strains (ϵ_{xo} , ϵ_{yo} , γ_{xyo}) and the curvatures (κ_x , κ_y , κ_{xy}) of the laminate reference surface are determined by solving the Equation A.8. The in-plane strains in the laminate at a distance z from the reference plane are then written as

$$\begin{pmatrix} \epsilon_x \\ \epsilon_y \\ \gamma_{xy} \end{pmatrix} = \begin{pmatrix} \epsilon_{xo} \\ \epsilon_{yo} \\ \gamma_{xyo} \end{pmatrix} + z \begin{pmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{pmatrix} \quad (\text{A.11})$$

The stresses at position z are

$$\begin{pmatrix} \sigma_x \\ \sigma_y \\ \sigma_{xy} \end{pmatrix} = \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix} \left(\begin{pmatrix} \epsilon_{xo} \\ \epsilon_{yo} \\ \gamma_{xyo} \end{pmatrix} - \begin{pmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{pmatrix} \Delta T + z \begin{pmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{pmatrix} \right) \quad (\text{A.12})$$

When z lies within layer k , then the subscript k is presumed to be attached to the material properties in Equation A.12.

A.2 NORMAL INTERLAMINAR EDGE STRESSES

Consider a laminated composite tension specimen as shown in Figure A-4. Depending on the stacking sequence of the laminae which compose the laminate, the free edge indicated in the figure can undergo delamination failure before the laminate as a whole fails. The occurrence of this disturbing phenomenon led to the development of the theory presented in References 16-19 and summarized below.

The stress resultants in the specimen due to the applied load P in the x -direction are clearly

$$\begin{aligned} N_x &= \frac{P}{2b} \\ N_y &= N_{xy} = M_x = M_y = M_{xy} = 0 \end{aligned} \tag{A.13}$$

Then the strains and stresses in the various lamina are computed by solving Equation A.8, and evaluating Equations A.11 and A.12 for appropriate values of z . In this case the lamina stresses are constant through the thickness of each layer.

Figure A-5 shows a section cut from the laminate; the section geometry is characterized by one unit in the x -direction, a symmetric half in the y -direction, and full thickness in the z direction. The forces acting on the laminate in the y -direction are also shown on the figure. Since the free edge is stress free, the forces acting at the $y=0$ must balance through the layers. Now consider layer number 1 which is isolated in Figure A-6. Clearly, since the edge $y=b$ is stress free, there must be some area near the free edge which must develop an interlaminar shear force F_1 and moment M_1 to balance the force $\sigma_{y1} h_1$ acting at $y=0$. This line of reasoning can be extended to conclude that all layers must develop interlaminar edge forces and moments as shown in Figure A-7.

If the typical layer k is required to be in equilibrium with respect to force-sums and moment sums, the following equations result:

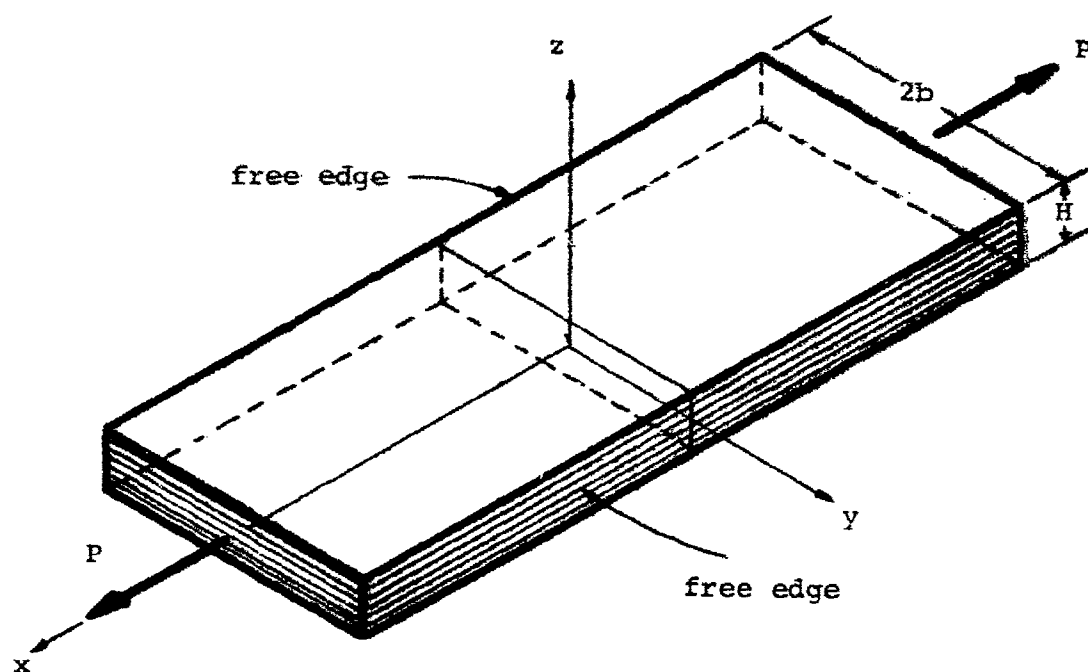


Figure A-4. Composite Tension Specimen.

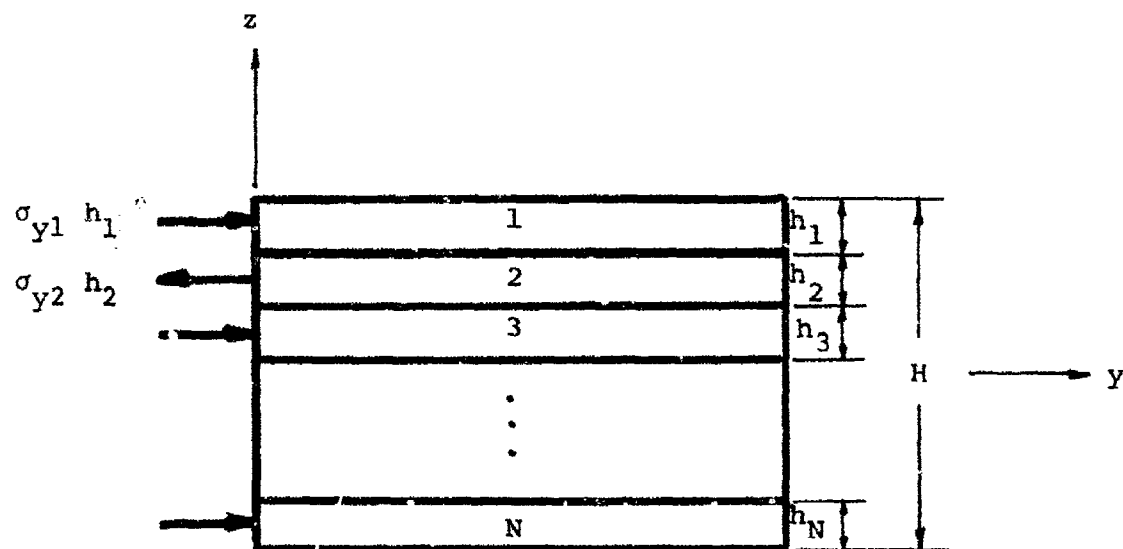


Figure A-5. Laminate Section at $X = 0$.

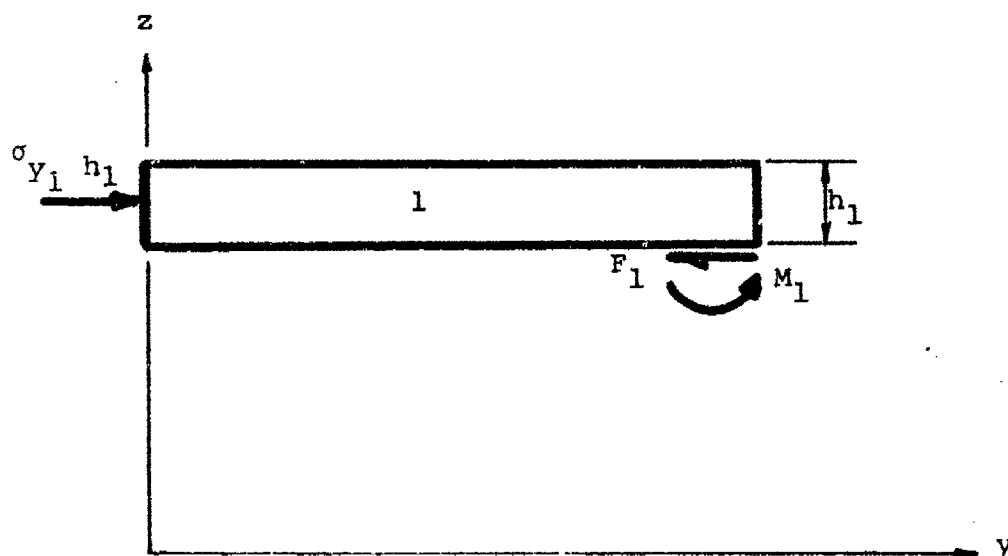


Figure A-6. Layer Number 1.

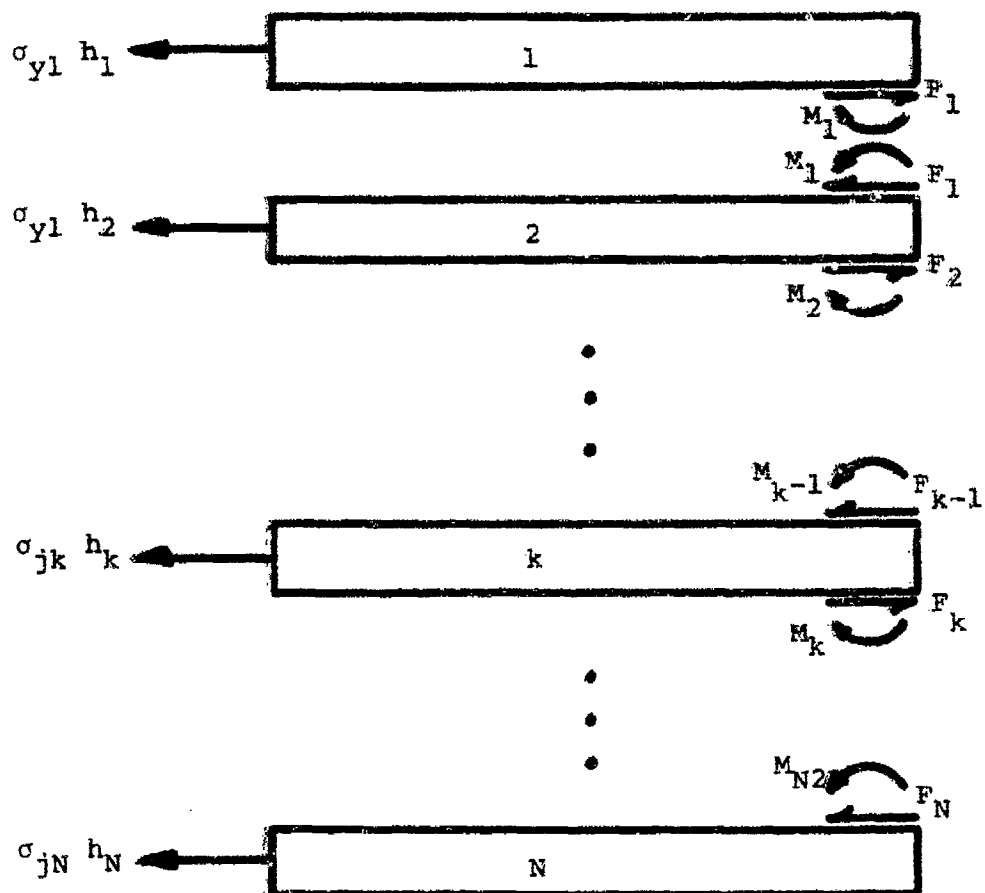


Figure A-7. Layer Edge Forces.

$$F_k = \sigma_k h_k + F_{k-1} \quad (A.14)$$

$$M_k = -\frac{\sigma_k h_k^2}{2} + F_{k-1} h_k + M_{k-1}$$

If these equations are applied sequentially starting with $k = 1$, for which $F_0 = M_0 = 0$, then each set of interlaminar forces can be determined in a recursive manner.

Now it is argued that the only way to develop edge moments near the free edge is to have a nonuniform distribution of interlaminar normal stress in that area. Such a normal stress is shown in Figure A-8, in which the distribution over a small length assures that the total moment of M_k , and the tension and compression areas balance. An approximate normal stress distribution (References 17-19) is shown in Figure A-9. Finally, using the approximate interlaminar normal stress distribution of Figure A-9, the following value is found for the normal stress at the free edge,

$$\sigma_{ek} = \frac{90}{7} \frac{M_k}{H^2} \quad (A.15)$$

A.3 COMPUTATIONS FOR SPECIFIC LAMINATES

The analysis presented above has been utilized to estimate interlaminar normal stresses for seven specific laminates. The particular material systems and stacking sequences considered, along with their respective properties are listed in Table A-1.

The normal edge stresses developed in these composites are illustrated in Figure A-10. The five curves in the tensile half of the figure all have the same ply stacking sequence. The different tensile stress levels developed indicate the influence of material properties. The three curves for G-160/6535-1 graphite/epoxy illustrate the effects of different ply stacking sequences. Orientations (1) and (3) in Figure A-10

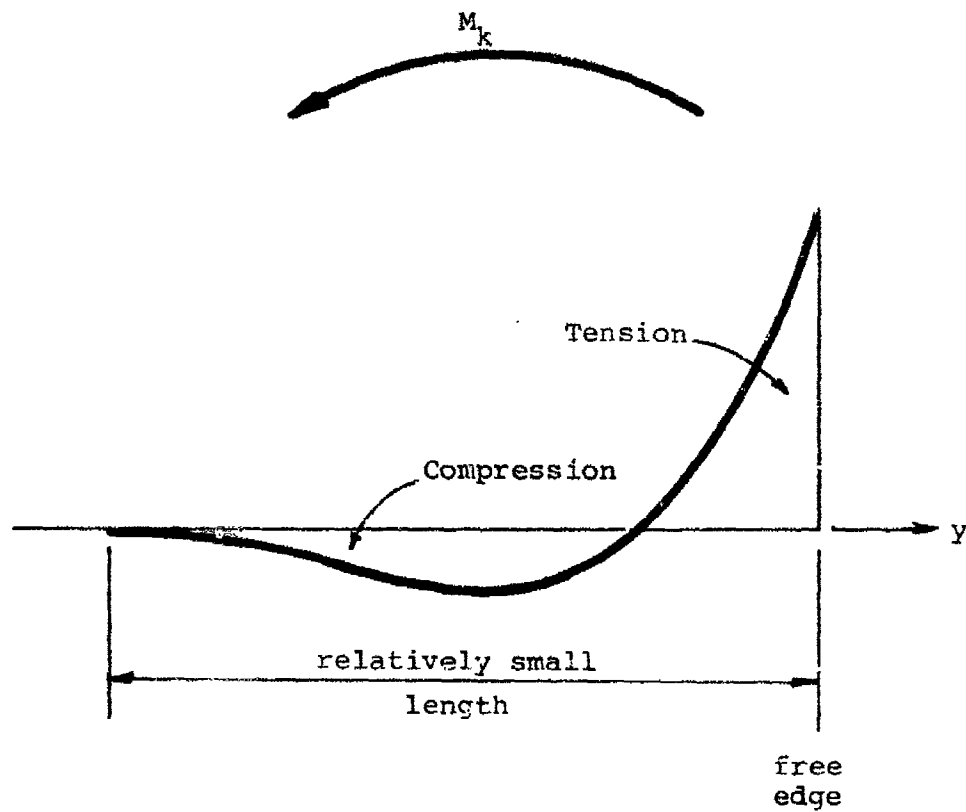


Figure A-8. Distribution of Normal Stress Near Free Edge.

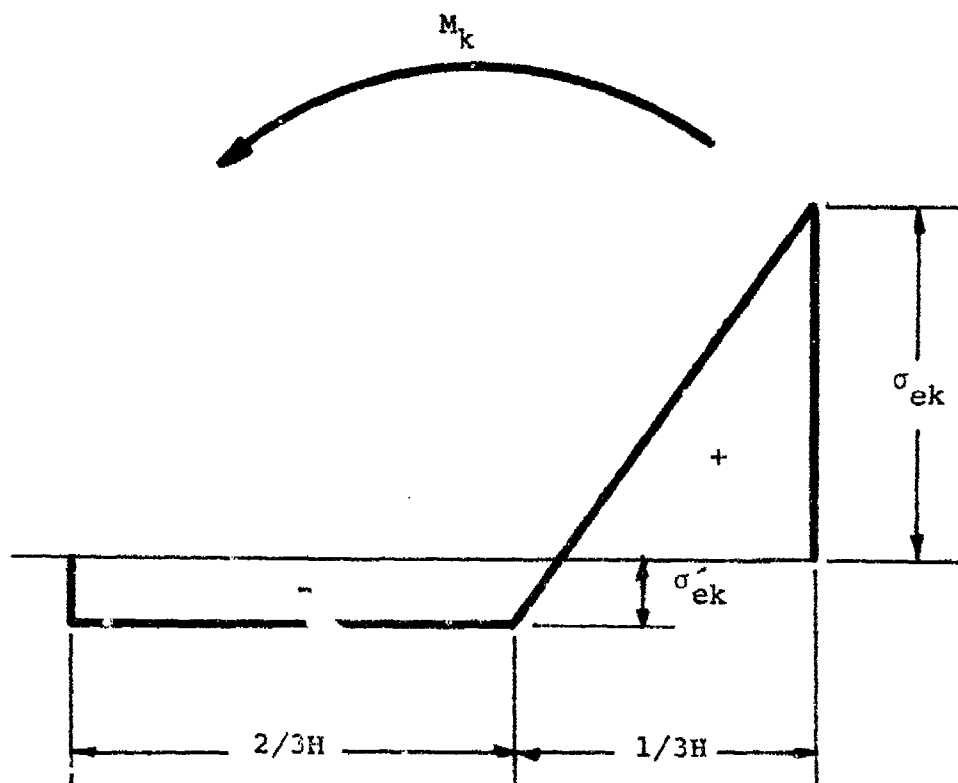


Figure A-9. Approximate Distribution of Interlaminar Normal Stress at Layer k .

TABLE A-1
LAMINATE SYSTEMS CONSIDERED IN SAMPLE INTERLAMINAR
NORMAL STRESS ANALYSIS

	HYE 2034D	HYE 1076J	SLC/5506	T300/V378A	G-160/6535-1	G-160/6535-1	G-160/6535-1
t_{ply} (inch)	0.0049	0.0051	0.0064	0.0051	0.0048	0.0048	0.0048
E_1 (psi)	44.5×10^6	20.0×10^6	33.4×10^6	20.1×10^6	18.5×10^6	18.5×10^6	18.5×10^6
E_2 (psi)	0.97×10^6	1.34×10^6	2.99×10^6	1.31×10^6	1.82×10^6	1.82×10^6	1.82×10^6
G_{12} (psi)	0.73×10^6	0.92×10^6	0.74×10^6	1.62×10^6	0.95×10^6	0.95×10^6	0.95×10^6
ν_{12}	0.22	0.32	0.23	0.30	0.32	0.32	0.32
ply orientation	(1)	(1)	(1)	(1)	(1)	(2)	(3)

(1) (0,45,-45,0,0,-45,45,0,90,0) s

(2) (0,45,-45,0,0,-45,45,0) s

(3) (0,90,45,-45,0,0,-45,45,0,0) s

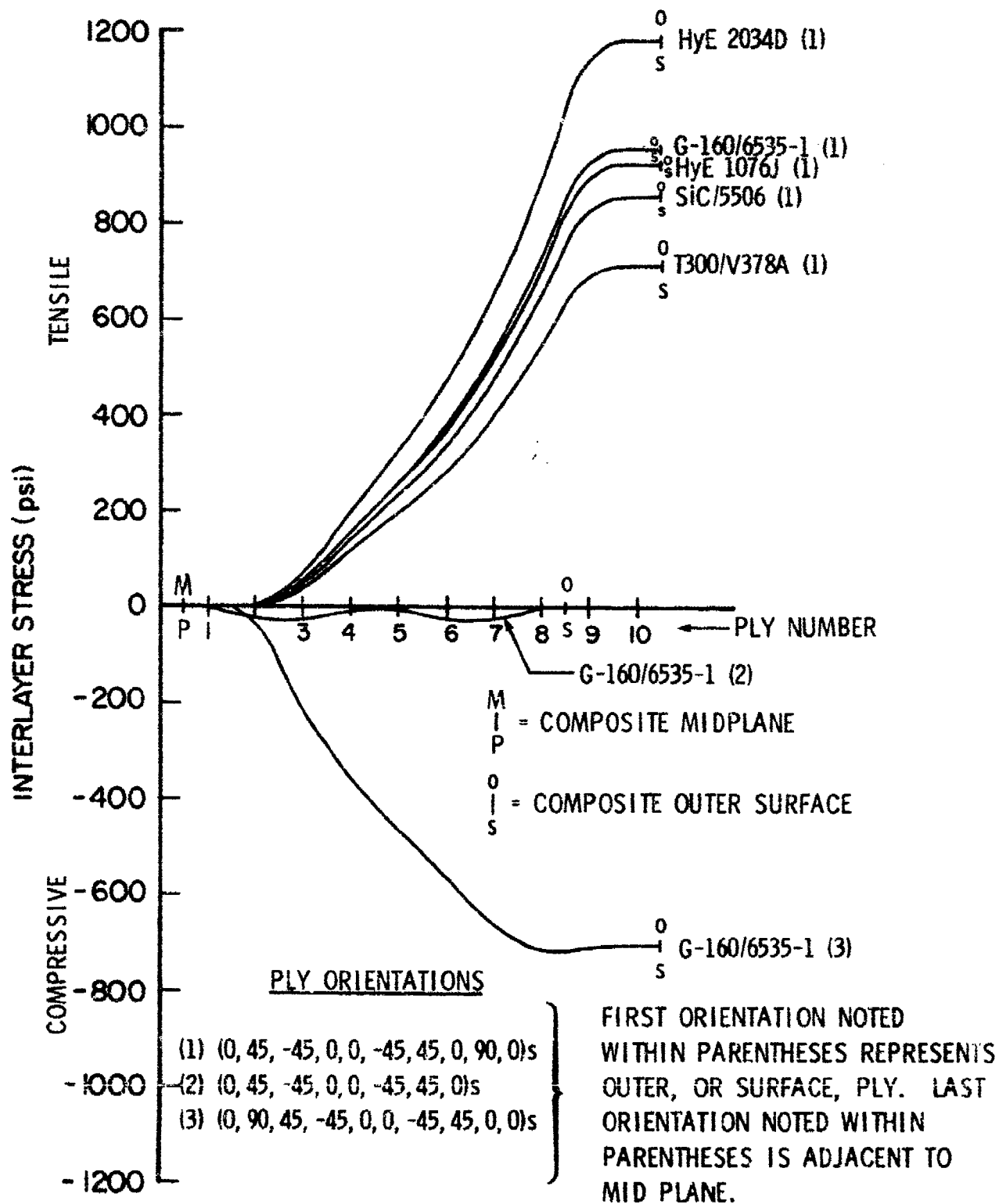


Figure A-10. Interlayer Normal Stresses for Various Composite Laminates.

differ only in the position of the 90° ply, while orientation (2) has no 90° ply and has one less 0° ply than orientations (1) and (3). All of the stresses plotted in Figure A-10 were computed for a stress resultant $N_x = 1000 \text{ lb/in}$ (1751 N/cm), as indicated in Equation (A.13).

APPENDIX B
PREPREG QUALITY CONTROL TEST PROCEDURES
AND TEST RESULTS

This appendix contains copies of the test procedures followed in determining prepreg physical properties. It also presents the test results obtained from these various tests on each prepreg material. Summaries of these data are presented in Sections 4.1 through 4.6.

In addition to the tables of physical properties, chromatographic analyses are presented for resin extracted from each prepreg.

Hercules Specification
Volatile Content

HD-SG-2-6006C

5.1.2 Test procedure. The test procedure shall be as follows:

- a. Condition new Gooch filtering crucibles in beaker containing concentrated HNO_3 for a minimum of 1 hour at $100 \pm 5^\circ \text{C}$. Wash with water, dry in oven at $93 \pm 3^\circ \text{C}$ and desiccate.
- b. Weigh conditioned filtering crucible to the nearest 0.1 milligram (mg).
- c. Carefully remove release paper from prepreg specimen and place specimen in tared crucible.
- d. Weigh crucible containing specimen to the nearest 0.1 mg.
- e. Condition crucible and specimen in an oven maintained at $93.5^\circ \pm 3^\circ \text{C}$ for a minimum of 90 minutes and a maximum of 120 minutes, unless otherwise specified in the applicable prepreg specification.

NOTE

Prepregs with polyimide resin systems should be conditioned at $288 \pm 3^\circ \text{C}$ for 60 ± 1 minutes.

- f. Remove crucible from oven, cool to room temperature in a desiccator, and reweigh.
- g. Calculate volatiles content of prepreg as follows:

$$\text{Weight \% Volatiles} = \frac{W_2 - W_3}{W_2 - W_1} \times 100$$

where: W_1 = weight of empty conditioned filtering crucible, grams (g)

W_2 = original weight of crucible and specimen before heating, g

W_3 = final weight of crucible and specimen after heating, g

Hercules Specification Resin Content

HD-SG-1-6006C

5.2.3 Procedure C (hot MEK extraction method). Determine resin content of prepreg by the hot MEK extraction method as follows:

- a. Prepreg samples shall be as specified in table I. Take duplicate test specimens, one from each end of the sample.

Table I. Resin Content Specimens for Procedures C, D, and E

Tape width	Sample size
3 inches	3 inches by 3 inches
6 inches	2 inches by 6 inches
12 inches	1 inch by 12 inches

- b. Weigh clean filtering crucible to the nearest 0.1 mg.
- c. Carefully remove release paper from the prepreg specimens and place in tared crucible.
- d. Weigh crucible containing specimen to the nearest 0.1 mg.
- e. Add 150 ml MEK to a 250 ml beaker, place beaker on a steam bath and bring to a boil. (Beaker should be covered with a watch glass to minimize evaporation.)
- f. Add prepreg sample to the hot MEK, being careful not to splash the hot MEK. Stir occasionally and let heat for ten minutes or until MEK boils.
- g. Transfer the MEK and fiber into the original tared filtering crucible positioned in a filtering flask with vacuum trap and vacuum pump.
- h. Wash the fiber three times with additional hot MEK.
- i. Remove the crucible containing fibers and dry in an oven maintained at $163^{\circ} \pm 3^{\circ} \text{C}$ for 15 to 20 minutes.
- j. Remove crucible from oven, cool in a desiccator, and weigh to the nearest 0.1 mg.
- k. Calculate resin content as follows:

$$\text{Weight \% Resin} = \left[\frac{W_2 - W_3}{W_2 - W_1} \times 100 \right] - V$$

where: W_1 = weight of empty crucible, g

W_2 = original weight of crucible and specimen, g

W_3 = final weight of crucible and fibers, g

V = weight percent volatiles from 5.1, %

Hercules Specification
Resin Flow

HD-SG-2-6006C

5.3.2 Procedure B. Determine resin flow as follows:

- a. Cut eight 4 x 4 inch plies of sample prepreg.
- b. Lay up the prepreg plies 0°/90° and weigh to the nearest 0.1 g.
- c. Place layup on 1/4 inch thick aluminum plate which has been covered with nonporous teflon.
- d. Cut one 6 x 6 inch ply of porous TFE release cloth and place on top of layup.
- e. Cut two 6 x 6 inch plies of glass bleeder cloth and place on top of TFE release cloth.
- f. Cover entire layup with 1 ply of glass bleeder cloth to be used as air breather.
- g. Place entire assembly in vacuum bag.
- h. Place in oven at room temperature and pull full vacuum (25 inches Hg).
- i. Bring oven up to 250°F (oven temperature) in 30 to 45 minutes and hold at 250°F for 30 minutes while maintaining full vacuum.
- j. Raise temperature to 350°F (oven temperature) in 30 to 45 minutes and hold at 350°F for 60 minutes.
- k. Remove from oven while hot and remove from vacuum bag.
- l. Clean any excess resin from panel.
- m. Weigh panel to the nearest 0.1 g.
- n. Calculate the resin flow as follows:

$$\text{Resin flow, percent} = \frac{W_1 - W_2}{W_1} \times 100$$

where: W_1 = original weight of prepreg layup, g.

W_2 = final weight of panel, g.

- o. Report the average of a minimum of two determinations.

Hercules Specification Gel Time

HD-SG-2-6006C

5.5 Gel time. The prepreg gel time shall be determined as follows:

5.5.1 Specimen preparation. Prepare specimen for gel time test as follows:

- a. Cut 12 to 13 prepreg strips 3/4-inch by 3-inch (4 to 5 grams) and stack strips on top of each other. Roll stacked prepreg strips to form an approximately 3/4-inch by 3/4-inch diameter cylinder as shown in figure 2.
- b. Place prepared specimen on one end of approximately 3-1/2 inch by 7-inch x 0.006 inch aluminum foil and roll tightly. Fold open ends tightly over the middle and cut one corner with scissors to make approximately 1/16 inch opening. (See figure 3.)

5.5.2 Equipment preparation. Prepare equipment for gel time testing as follows:

- a. Place bottom gel plate (figure 4) 1/4-inch from front center of bottom press platen and tape down, with three-inch wide green pressure sensitive tape.
- b. Place top gel plate (figure 4) against top press platen and center directly over bottom gel plate as shown in figures 5 and 6. Tape top gel plate in place with green pressure sensitive tape.
- c. Place a thermocouple on the center of bottom gel plate, 3/4-inch from the front end and as shown in figure 3. Stabilize at test temperature specified in the applicable prepreg specification.

5.5.3 Test procedure. The gel time test procedure shall be as follows:

- a. Place thermocouple on bottom gel plate, 3/4-inch in from the front edge of the plate and 1-1/2 inches from either left or right edge as shown in figure 5. Use green pressure sensitive tape to secure the thermocouple wire so that the thermocouple will remain in the intended position.
- b. Place gel specimen on bottom gel plate so that the cut corner is positioned 1/8 to 1/4 inch behind thermocouple and facing the operator.
- c. Close the press platen quickly and apply sufficient pressure to obtain approximately 1/4 inch resin bead. Start timing at this point. The total elapsed time from the time specimen is placed on gel plate to closing platens should be 15 ± 5 seconds.
- d. Using a wooden probe, probe the edges of the resin bead. As gel time approaches, the resin becomes quite viscous and forms a string as the wooden probe is moved away from the resin. Continue probing until the resin ceases to string and the resin mass becomes no longer plastic. At this point the resin mass should form permanent deformation when pressed with the tip of the wooden probe. Note the elapsed time and record the time and the test temperature.
- e. Report the average of a minimum of two determinations.

ADVANCED COMPOSITE DESIGN GUIDE (VOL. IV)
SPECIFICATIONS FOR PREPREG RESIN AND VOLATILE CONTENT

JANUARY 1973

4.2.3.2 RESIN CONTENT

4.2.3.2.1 Graphite

One 2-inch-square specimen with volatiles removed is placed in a 150 to 250 ml beaker. The beaker is filled with 100 ml of nitric acid (HNO_3) and placed on a hot plate maintained at $100^\circ \text{C} \pm 5^\circ \text{C}$ (212°F). The sample is digested until fiber is completely separated as determined by visual examination. The acid and fibers are transferred into a tared glass filtering crucible positioned in a filtering flask with vacuum trap and vacuum pump. Fibers are washed three times with 20 ml of HNO_3 and followed by water wash.

The crucible and fibers are dried at $93.5^\circ \text{C} \pm 3^\circ \text{C}$ (200°F) for a minimum of 60 minutes, cooled in a desiccator, and the weight (W_4) is obtained. The weight percent of resin is computed from:

$$\text{Resin content w/o} = \frac{W_3 - W_4}{W_2 - W_1} (100)$$

where

W_1 = is crucible weight

W_2 = is sample and crucible weight

W_3 = is specimen weight

W_4 = is weight after acid digest (fibers)

Compute weight percent of fiber from:

$$\text{Fiber content w/o} = \frac{W_4 - W_1}{W_2 - W_1} (100)$$

4.2.3.3 VOLATILE CONTENT

The following procedure is applicable to both graphite and boron prepreg. Filtering crucibles are conditioned in a beaker containing concentrated nitric acid (HNO_3) for a minimum of 1 hour at $100^\circ \text{C} \pm 5^\circ \text{C}$ (212°F). The crucible is washed, desiccated, and weighed (W_1). A 2-inch-square prepreg sample is placed in the crucible and weighed (W_2). Prepregs with epoxy resin systems are conditioned in a nonrecirculating oven maintained at $93.5^\circ \text{C} \pm 3^\circ \text{C}$ (200°F) for a minimum of 90 minutes and a maximum of 120 minutes. The crucible is removed from the oven, desiccated, and reweighed (W_3). The weight percent of volatiles is obtained from

$$\text{Volatiles w/o} = \frac{W_2 - W_3}{W_2 - W_1} (100)$$

Data are averaged from a minimum of three tests.

QUALITY CONTROL METHOD QCI-C-V-14

Fiberite Specification

VOLATILE CONTENT OF GRAPHITE PREPREG

1. Place a 2" x 2" sample into previously weighed Aluminum pan (W_2). Sample must lay flat and cannot be rolled up or more than one ply thick.
2. Weigh sample and pan to the nearest milligram (W_1).
3. Place into a forced air oven maintained at $163 \pm 3^\circ\text{C}$ for 20 ± 0.5 minutes.
4. Cool to room temperature in a desiccator and weigh to the nearest milligram (W_3).
5. Calculate as follows:

$$\text{Volatile content, percent} = \frac{W_1 - W_3}{W_1 - W_2} \times 100$$

W_1 = weight of pan plus specimen before volatile removal.

W_2 = weight of pan.

W_3 = weight of pan plus specimen after volatile removal.

QUALITY CONTROL METHOD R-15

Fiberite Specification

RESIN SOLIDS CONTENT OF GRAPHITE PREPREG

SCOPE: This method is applicable for the determination of percent resin solids in unfilled carbon or graphite prepreg roving or tape material where this method has been found suitable or is called out in a specification.

- PROCEDURE:
1. Run volatile content on a sample cut adjacent to the sample to be used for resin solids. The volatile procedure used shall be as specified in the material specification.
 2. Cut a sample of material approximately 3 grams in any convenient size.
 3. Weigh the sample to the nearest 0.0001 gram. Record this as W_1 .
 4. Place the sample in a 400 ml beaker. Add 200 ml of DMF (Dimethyl formamide). Boil for 5 minutes (time starts when the DMF starts to boil).
 5. Cool sample. Pour off the DMF. Wash sample twice with acetone.
 6. Place sample in a tared aluminum foil pan. Dry sample for 30 minutes in an oven maintained at $163 \pm 3^\circ\text{C}$.
 7. Cool sample to ambient temperature in a desiccator.
 8. Reweigh the sample to the nearest 0.0001 gram. Record the weight as W_2 .

CALCULATION: Resin Solids (% by weight) =

$$\frac{(W_1 - W_1 V) - W_2}{(W_1 - W_1 V)} \times 100$$

Where: W_1 = Original sample weight.

W_2 = Weight of carrier remaining after extraction.

V = Percent volatiles (Procedure as called out by the material specification).

QUALITY CONTROL METHOD QCI-C-F-42

Fiberite Specification

FLOW OF GRAPHITE PREPREG

Flow: Laminate

Form: 2 ply 2" x 2" square cut

Lay-up: Cut 6 pieces of style 1581 glass bleeder cloth, 4" x 4" square and 2 pieces of porous teflon separator cloth (EMFAB TX-1040 or equivalent) 4" x 4" square. Weigh all to the nearest milligram (W_1). Cut 2 pieces of prepreg 2" x 2", cross ply 0° and 90°, and assemble as follows: 3 pieces 1581 glass, 1 piece porous teflon, 2 pieces graphite prepreg (cross plied 0° and 90°), 1 piece porous teflon, 3 pieces 1581 glass, and weigh to the nearest milligram (W_2).

Temperature: 325 ± 5°F

Pressure: 100 psi (400# total pressure)

Time: 15 ± 1 minute

Determination: As required

Procedure: Put Mylar release film on both sides of Lay-up and place into 325°F preheated press. Apply 100 psi for 15 minutes. Remove and discard Mylar film. Remove crossplied test specimen and weigh 1581 glass and porous teflon to nearest milligram (W_3).

Calculation:
$$\text{Flow, \%} = \frac{W_3 - W_1}{W_2 - W_1} \times 100$$

W_1 = Weight of 1581 glass fabric and porous teflon separator

W_2 = Weight of 1581 glass fabric, porous teflon separator and cross plied specimen.

W_3 = Weight of 1581 glass fabric and porous teflon separator after cure.

QUALITY CONTROL METHOD G-2

Fiberite Specification

GEL TIME

Gel time of graphite prepreg tape or broadgoods materials.

SCOPE: This method is applicable for the determination of gel time on carbon or graphite prepreg materials containing a thermosetting resin which undergoes gelation at a specified temperature.

APPARATUS

1. Fisher-Johns melting point apparatus
2. Thickness No. 2 cover glasses (18 mm)
3. Timer or stopwatch
4. Wooden picks

PROCEDURE

1. Preset the Fisher-Johns melting point apparatus to read $\pm 1^\circ\text{C}$ of the specified temperature.
2. Insert a $\frac{1}{4}'' \times \frac{1}{4}''$ sample between 2 cover glasses and place on the Fisher-Johns apparatus.
3. Start the timer and probe the specimen with a wooden pick.
4. When resin gels (this is usually evident when no resin movement is seen when moderate pressure is applied to the specimen) stop the timer and report the gel time to the nearest 0.1 minute.
5. Report the gel time as the average of three determinations.

GEL TEMPERATURES FOR GRAPHITE PREPREG

RESIN SUFFIX	TEST TEMPERATURE ($^{\circ}\text{C}$)
-48	121
-30	170 C
-34	163 $^{\circ}\text{C}$ (320 $^{\circ}\text{F}$)

Example

hy-E 1348-B

— Resin Suffix

Run at 121 $^{\circ}\text{C}$

PREPREG PHYSICAL PROPERTIES				
Material: T300/AFR800			Vendor: Hexcel	
Lot/Batch Number	Spool/Roll Number	Volatile Content (% by wt)	Resin Content (% by wt)	Resin Flow (% by wt)
22300	1	0.26	41.95	14.91
22300	1	0.32	41.43	12.59
22300	1	0.32	42.99	14.19
Lot/Batch Number	Spool/Roll Number	Gel Time @ 275°F (135°C) (minutes)		
22300	1	141		
22300	1	142		
22300	1	141		
	Received:	Tested:	Remarks	
Spool #1	11-20-78	11-21-78	Volatiles, Resin Content, Flow	
		12-18-78	Gel Time	
Test Procedures Followed				
Property	Applicable Test Spec.		Source of Test Spec.	
Volatile Content	HD-SG-2-6006C (5.1.2)		Hercules	
Resin Content	HD-SG-2-6006C (5.2.3C)		Hercules	
Resin Flow	HD-SG-2-6006C (5.3.2B)		Hercules	
Gel Time	HD-SG-2-6006C (5.5)		Hercules	

PREPREG PHYSICAL PROPERTIES				
Material: T300/AFR800			Vendor: Hexcel	
Lot/Batch Number	Spool/Roll Number	Volatile Content (% by wt)	Resin Content (% by wt)	Resin Flow (% by wt)
22300	2	0.18	41.54	15.49
22300	2	0.07	39.73	15.52
22300	2	0.07	39.11	15.53
Lot/Batch Number	Spool/Roll Number	Gel Time @ 275°F (135°C) (minutes)		
22300	2	140		
22300	2	139		
22300	2	141		
Received:		Tested:	Remarks	
Spool #2	11-30-78	12-1-78	Volatiles, Resin Cont., Flow	
		12-13-78	Gel Time	
Test Procedures Followed				
Property	Applicable Test Spec.		Source of Test Spec.	
Volatile Content	HD-SG-2-6006C (5.1.2)		Hercules	
Resin Content	HD-SG-2-6006C (5.2.3C)		Hercules	
Resin Flow	HD-SG-2-6006C (5.3.2B)		Hercules	
Gel Time	HD-SG-2-6006C (5.5)		Hercules	

PREPREG PHYSICAL PROPERTIES (1)				
Material: T300/AFR800			Vendor: Hexcel	
Lot/Batch Number	Spool/Roll Number	Test Date	Gel Time (minutes)	Resin Flow (% by wt)
22300	1	1-3-79	---	21.7
22300	1	1-8-79	152	---
22300	2	1-4-79	---	19.3
22300	2	1-10-79	140	---
22300	2	1-19-79	---	21.9

(1) These tests were conducted to determine the effect of room temperature storage on prepreg properties.

Test Procedures Followed		
Property	Applicable Test Spec.	Source of Test Spec.
Volatile Content		
Resin Content		
Resin Flow	HD-SG-2-6006C(5.3.2B)	Hercules
Gel Time	HD-SG-2-6006C (5.5)	Hercules

PREPREG PHYSICAL PROPERTIES				
Material: SiC/5506			Vendor: AVCO	
Lot/Batch Number	Spool/Roll Number	Volatile Content (% by wt)	Resin Content (% by wt)	Resin Flow (% by wt)
2	1	1.28	29.18	---
2	1	1.38	28.20	---
2	1	1.49	27.25	---
2	4	---	26.68	---
2	4	1.48	27.13	---
2	4	1.56	28.28	---
2	2B	1.32	26.86	---
2	2B	1.27	26.95	---
2	2B	1.42	28.48	---
2	2A	1.28	28.49	---
2	2A	1.42	28.84	---
2	2A	---	28.37	---
Test Procedures Followed				
Property	Applicable Test Spec.		Source of Test Spec.	
Volatile Content	Section 4.2.3.3		Advanced Composites Design Guide,	
Resin Content	Section 4.2.3.2.1		Jan. 1973, Vol. IV	
Resin Flow	---		---	

HPLC ANALYSIS

SAMPLE (CONC.) AVCO 5506 SAMPLE SIZE 1.5 ml
MOBILE PHASE 1 ACETONITRILE MOBILE PHASE 2 WATER
FLOW RATE 2.0 ml/min PROGRAM METH. 0
COLUMN(S) ODS DETECTOR TRACOR 970
ATTENUATION 32 WAVE LENGTH 220 nm
CHART SPEED 0.5 in/min FULL SCALE (mV) 20 mV
DATE NOVEMBER 28 79 OPERATOR VIOLFE

TIME	WATER	ACETD.
0	76%	24%
20 MIN	18%	82%
21 MIN	1%	99%

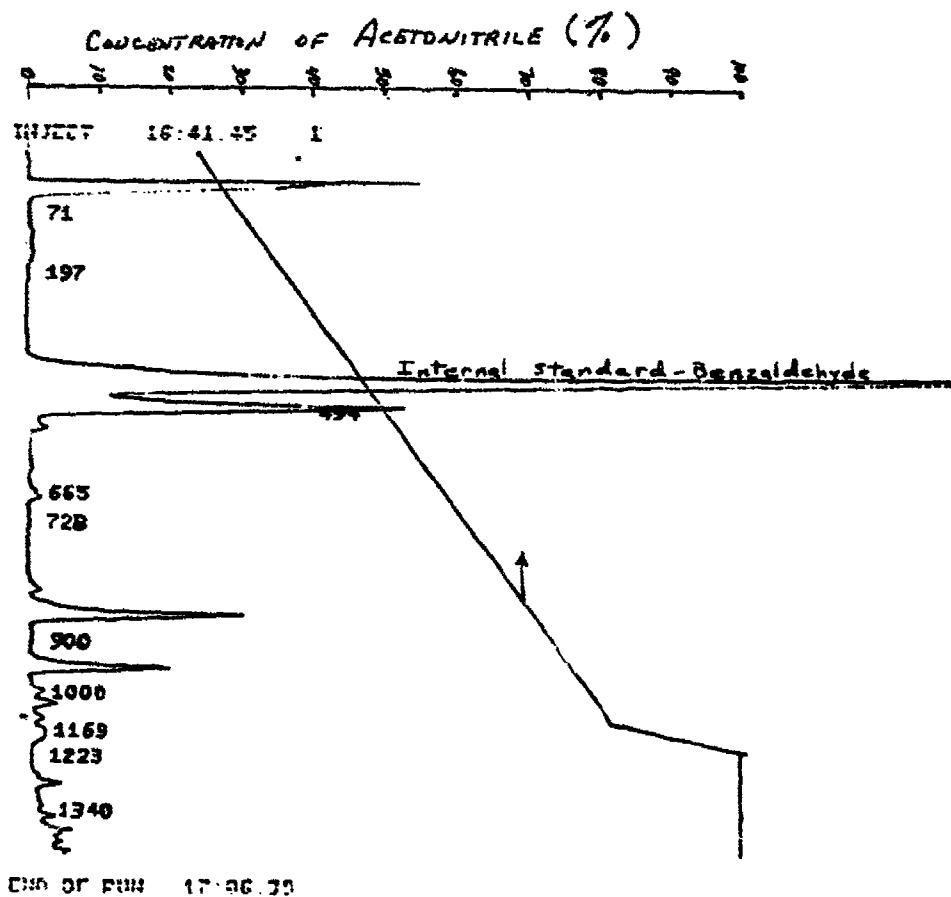


Figure B-1. HPLC Analysis of AVCO 5506 Epoxy Resin.

PREPREG PHYSICAL PROPERTIES				
Material: HyE 2034D			Vendor: Fiberite	
Lot/Batch Number	Spool/Roll Number	Volatile Content (% by wt)	Resin Content (% by wt)	Resin Flow (% by wt)
C0-010	1	0.62	39.05	22.35
		0.69	38.33	26.68
		0.69	40.16	26.35
Lot/Batch Number	Spool/Roll Number	Gel Time @ 325°F (163°C) (minutes)		
C0-010	1	12.63		
		12.48		
		12.23		
Test Procedures Followed				
Property	Applicable Test Spec.		Source of Test Spec.	
Volatile Content	QCI-C-V-14		Fiberite	
Resin Content	R-15		Fiberite	
Resin Flow	QCI-C-F-42		Fiberite	
Gel Time	G-2		Fiberite	

HPLC ANALYSIS

SAMPLE (CONC.) HYE-2034D SAMPLE SIZE 1.5 mg/ml
MOBILE PHASE 1 Acetonitrile MOBILE PHASE 2 Water
FLOW RATE 2.0 ml/min PROGRAM Method 9
COLUMN(S) 009 DETECTOR Jrator 970
ATTENUATION 32 WAVE LENGTH 330 nm
CHART SPEED 0.5 cm/min FULL SCALE (mV) 2.0 mV
DATE NOV 1981 30 71 OPERATOR WCL/CS

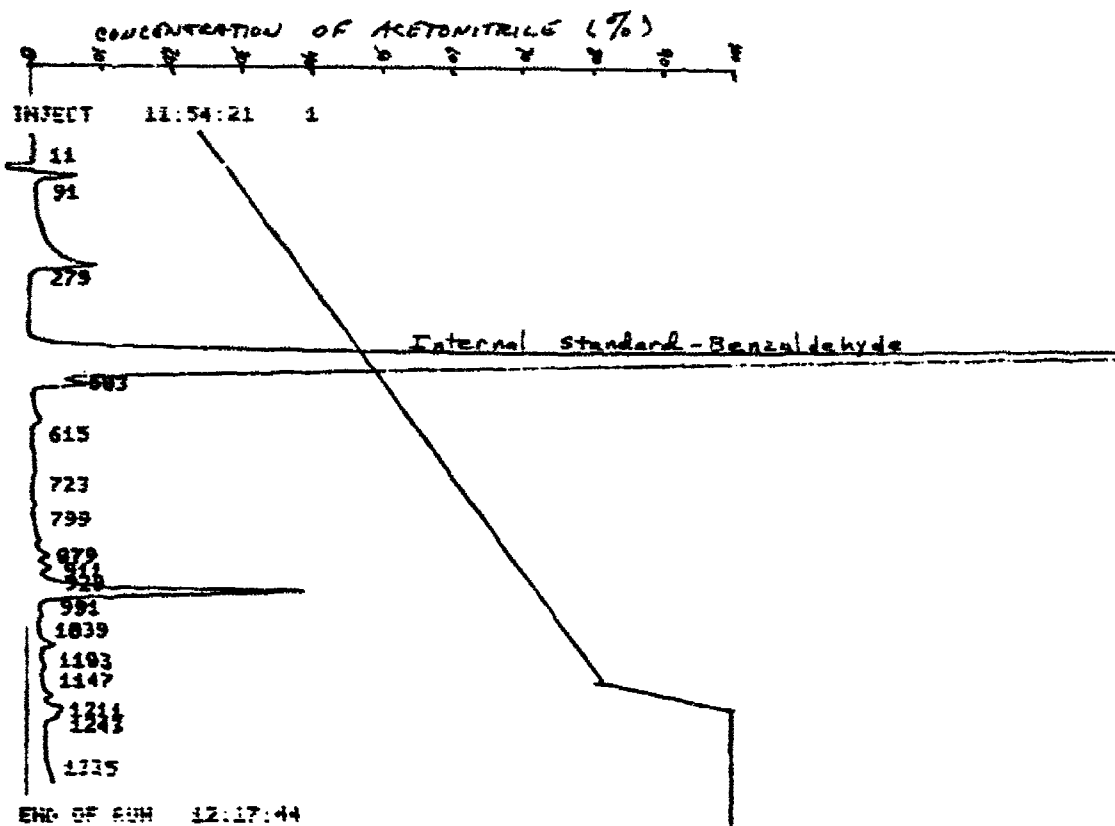
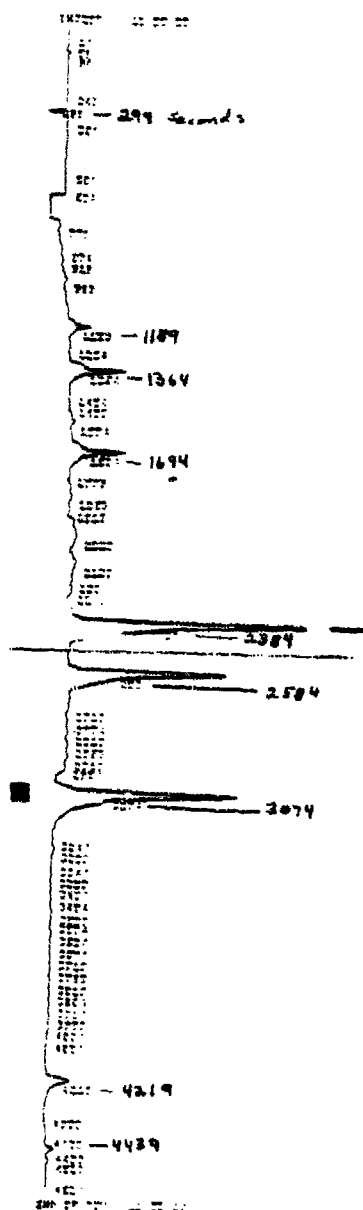


Figure B-2. HPLC Analysis of Fiberite 934 Epoxy Resin.

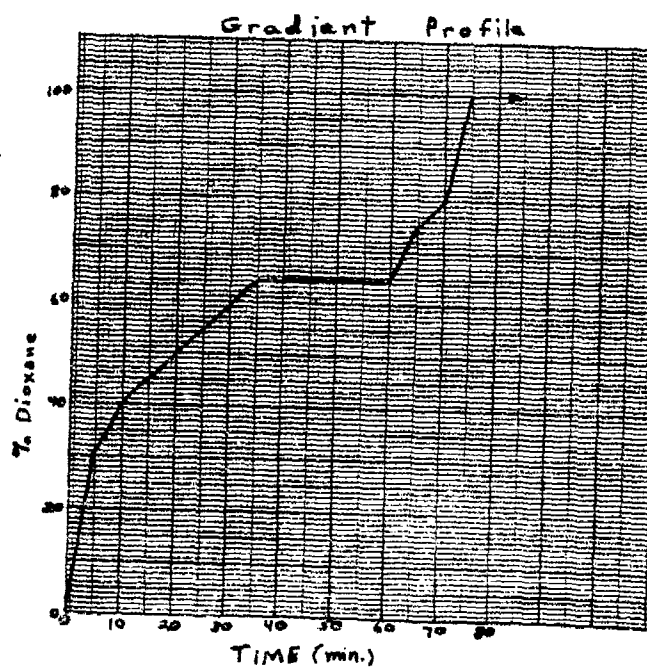
PREPREG PHYSICAL PROPERTIES				
Material: T300/V378A			Vendor: U.S. Polymeric	
Lot/Batch Number	Spool/Roll Number	Volatile Content (% by wt)	Resin Content (% by wt)	Gel Time @ 210°F(99°C) (minutes)
2W4810	1	5.79	29.00	30.52
		6.05	30.28	32.03
		4.61	32.63	31.97
2W4683	1	2.5 ¹	31.3 ¹	
¹ All data on Batch No. 2W4683 was generated by USP.				
Test Procedures Followed				
Property	Applicable Test Spec.		Source of Test Spec.	
Volatile Content	OCI-C-V-14 ²		Fiberite	
Resin Content	R-15		Fiberite	
Gel Time	G-2		Fiberite	
² Test conducted at 350°F (177°C) for 5 minutes rather than 325°F (163°C) for 20 minutes as called for in step 3 of specification.				



HPLC ANALYSIS
V378A - New*

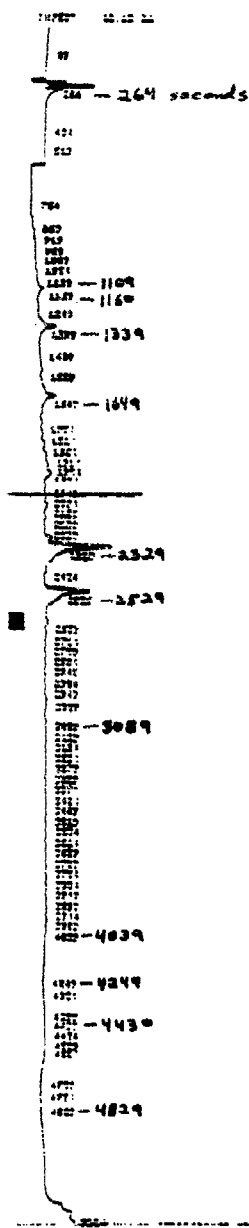
SAMPLE (CONC.)	0.197%	SAMPLE SIZE	25 μ l
MOBILE PHASE 1	H ₂ O	MOBILE PHASE 2	Dioxane
FLOW RATE	1.0 ml/min	PROGRAM	Meth 0
COLUMN(S)	RP-8 (SP)	DETECTOR	Tracer-UV
ATTENUATION	16	WAVE LENGTH	254
CHART SPEED	0.5 cm/min	FULL SCALE (mV)	40
DATE	10-2-80	OPERATOR	B. Price

* 1 month storage at 0°C



27.

Figure B-3. HPLC Analysis of New U.S. Polymeric V378A Polyimide Resin.



HPLC ANALYSIS
 V378A-old
 SAMPLE (CONC.) 0.17% SAMPLE SIZE 25ul
 MOBILE PHASE 1 H₂O MOBILE PHASE 2 Dioxane
 FLOW RATE 1.0 ml/min PUMPING Meth O
 COLUMN BP-R(5M) DETECTOR Tracer-UV
 ATTENUATION 16 WAVELENGTH 254
 CHART SPEED 0.5 mm/min PLOT SCALE 40
 DATE 10-2-80 BY B. Price

* 6 months storage at 0°F

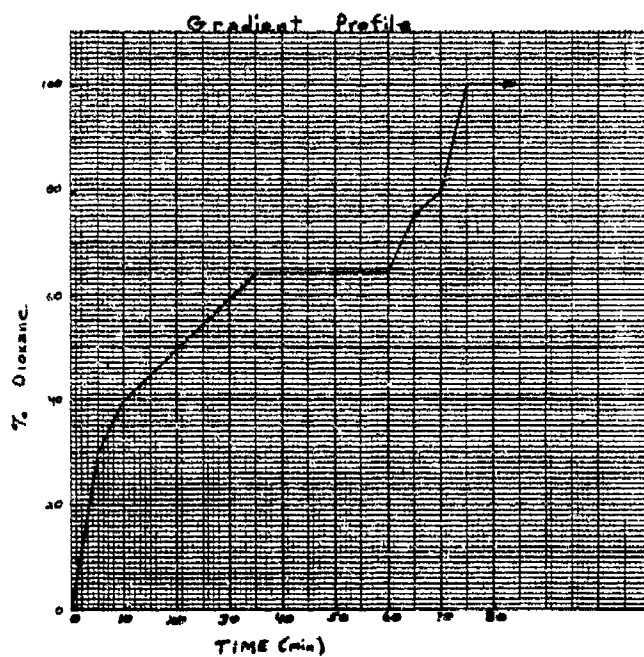


Figure B-4. HPLC Analysis of Old U.S. Polymeric V378A Polyimide Resin.

PREPREG PHYSICAL PROPERTIES				
Material: HyE 1076J			Vendor: Fiberite	
Lot/Batch Number	Spool/Roll Number	Volatile Content (% by wt)	Resin Content (% by wt)	Gel Time ¹ (min)
Cl-285	1	0.57	37.77	21.4
Cl-285	1	0.51	37.84	20.1
Cl-285	1	0.23	37.46	22.3

¹at 177°C

Test Procedures Followed		
Property	Applicable Test Spec.	Source of Test Spec.
Volatile Content	QCI-C-V-14	Fiberite
Resin Content	Method-R-15	Fiberite
Gel Time	Method-G-2	Fiberite

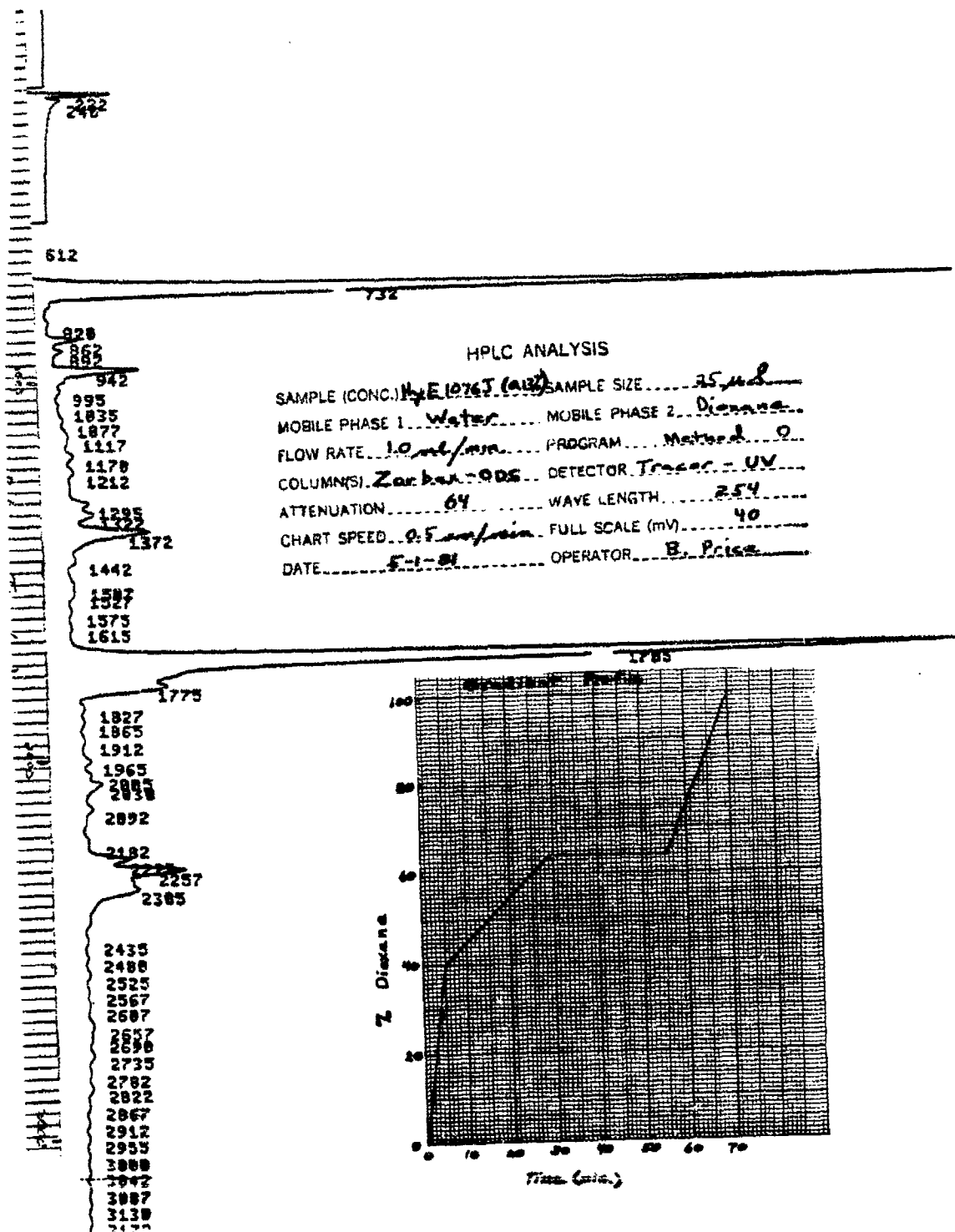


Figure B-5. HPLC Analysis of Fiberite 976 Epoxy Resin.

PREPREG PHYSICAL PROPERTIES

Material: G-160/6535-1			Vendor: AVCO	
Lot/Batch Number	Spool/Roll Number	Volatile Content (% by wt)	Resin Content (% by wt)	Gel Time @ 327°F (164°C) (minutes)
	440	0.23	39.27	38.49
		0.22	41.58	37.21
		0.14	40.82	38.55
	441	0.28	42.77	38.68
		0.13	40.73	37.75
		0.22	44.09	38.30

Test Procedures Followed

Property	Applicable Test Spec.	Source of Test Spec.
Volatile Content	QCI-C-V-14	Fiberite
Resin Content	R-15	Fiberite
Gel Time	G-2	Fiberite

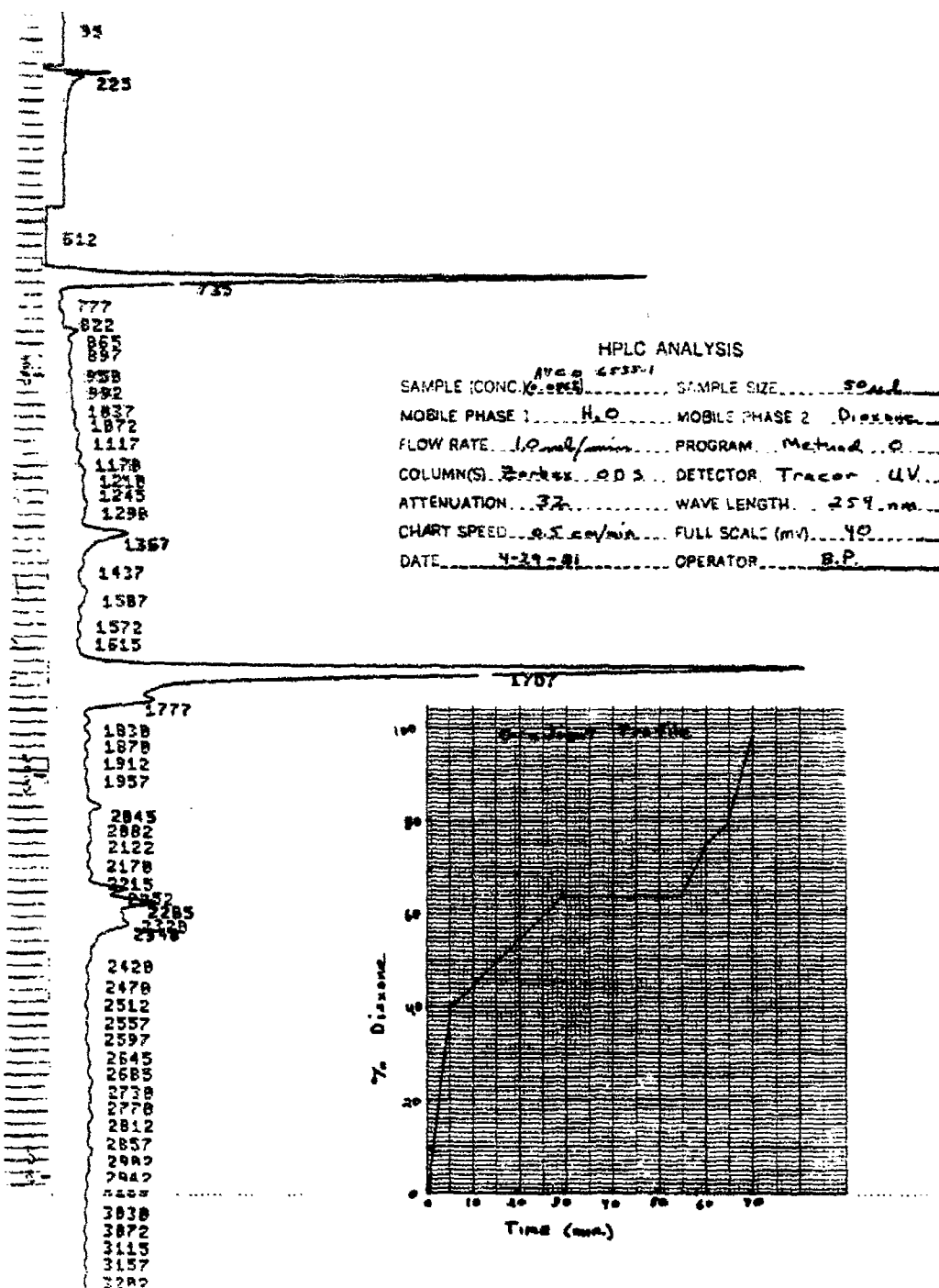


Figure B-6. HPLC Analysis of AVCO 6535-1 Epoxy Resin.

APPENDIX C
LAMINATE PHYSICAL PROPERTY DATA

All of the physical property measurements conducted upon the panels fabricated and used in this program are presented here. Summaries of these data appear in Sections 4.1 through 4.6.

LAMINATE PHYSICAL PROPERTIES

Material: T300/AFR800

Lam. No.	Fiber Orient.	No. Plies	Spec. Grav.	Resin Content (% by wt)	Fiber Content (% by vol)	Void Content (% by vol)	Thick. per ply (10 ⁻³ in.)	Prepreg Lot/ Batch No.	Prepreg Spool/Roll No.
F1	0°	6	1.60	24.4	71.2	0.0		22300	1
F3	0°	6	1.64	25.4	72.0	0.0		22300	1
F4	0°	6	1.60	25.2	70.4	0.0		22300	1
F5	0°	6	1.65	25.3	72.5	0.0		22300	1
F6	0°	6	1.58	31.8	63.4	0.0		22300	1
F7	0°	15	1.59	24.4	70.7	0.0		22300	1
F8	0°	15	1.62	25.0	71.4	0.0		22300	1
F9	0°	15	1.61	25.4	70.7	0.0		22300	1
F11	90°	15	1.60	25.0	70.6	0.0		22300	1
F12	90°	15	1.56	25.3	68.6	0.0		22300	1
F13	90°	15	1.62	24.9	71.5	0.0		22300	1
F14	90°	15	1.62	24.2	72.2	0.0		22300	1
F15	90°	15	1.62	24.5	72.0	0.0		22300	1
F16	90°	15	1.54	24.6	68.3	1.1		22300	1
F17	90°	15	1.61	24.3	71.7	0.0		22300	1
F18	90°	15	1.62	24.1	72.2	0.0		22300	1
F19	0°	14	1.67	24.1	73.9	0.0		22300	1
F20	90°	14	1.71	23.5	77.0	0.0		22300	1
F21	0°	15	1.62	24.0	72.5	2.5		22300	1
F22	0°	6	1.58	25.9	68.8	0.0		22300	1
F23	+45°	8	1.57	30.7	64.0	0.0		22300	1
F24	+45°	8	1.54	31.1	62.4	0.0		22300	1
F25	+45°	8	1.60	29.9	66.1	0.0		22300	1
F26	+45°	8	1.56	30.8	63.4	0.0		22300	1
F27	+45°	8	1.57	30.1	64.5	0.0		22300	1

[illegible]

LAMINATE PHYSICAL PROPERTIES

Material: SiC/5506

Lam. No.	Fiber Orient.	No. Plies	Spec. Grav.	Resin Content (% by wt)	Fiber Content (% by vol)	Void Content (% by vol)	Thick. per ply (10^{-3} in.)	Prepreg Lot/ Batch No.	Prepreg Spool/Roll No.
G9	90°	15	2.37	19.2	59.5	0		2	1
G10	0°	40	2.36	17.9	59.5	1.70		2	1
G14	+45°	8	2.33	19.4	57.5	1.52		2B	2
G15	+45°	8	2.34	19.1	58.1	1.27		2B	2
G16	+45°	8	2.30	22.0	53.9	0		2B	2
G17	+45°	8	2.35	20.3	57.5	0		2B	2
G20	0°	14	2.34	20.6	57.3	0		2B	2
G21	90°	14	2.40	18.2	60.4	0.02		2B	2
G22	90°	15	2.37	19.6	58.6	0		2B	2
G23	0°	6	2.39	18.4	60.0	0		2B	2
G24	90°	15	2.38	20.3	58.3	0		2B	2
G25	90°	15	2.38	18.8	59.4	0		2B	2
G26	90°	15	2.38	17.5	60.4	1.87		2B	2
G27	+45°	8	2.36	19.4	58.4	0.12		2A	2A
G28	+45°	8	2.34	19.1	58.1	1.41		2A	2A
G29	+45°	8	2.34	19.5	57.9	0.66		2A	2A
G30	+45°	8	2.33	19.3	57.6	1.41		2A	2A
G31	+45°	8	2.32	19.0	57.7	2.24		2A	2A
G32	(1)	20	2.35	19.4	58.3	1.01		2A	2A
G33	(1)	20	2.36	18.6	59.0	1.17		2A	2A
G34	(1)	20	2.35	19.0	58.6	0.85		2A	2A
G35	(1)	20	2.35	18.7	58.4	1.26		2A	2A
G36	(1)	20	2.36	18.8	58.7	0.89		2A	2A
G37	0°	14	2.41	17.4	61.2	0.46		2A	2A
G38	0°	15	2.39	18.3	60.1	0		2A	2A
G39	(1)	20	2.35	18.7	58.8	1.19		2A	2A
G40	(1)	20	2.35	19.4	58.2	0.36		2A	4

(1) (0,45,-45,0,0,-45,45,0,90,0)_S-20 ply.

[illegible]

(1) $(0, 45, -45, 0, 0, -45, 45, 0, 90, 0)_S$ -20 ply.

LAMINATE PHYSICAL PROPERTIES

Material: HyE 2034D

Lam. No.	Fiber Orient	No. Plies	Spec. Grav.	Resin Content (% by wt)	Fiber Content (% by vol)	Void Content (% by vol)	Thick. per ply (10 ⁻³ in.)	Prepreg Lot/ Batch No.	Prepreg Spool/Roll No.
H1	0°	6	1.82	23.0	70.1	0.00		C0-010	1
H2	0°	6	1.81	23.0	69.8	0.00			
H3	90°	15	1.81	23.3	69.4	0.00			
H4	90°	15	1.80	23.5	69.0	0.00			
H6	90°	15	1.81	23.7	69.1	0.00			
H7	90°	15	1.78	26.3	65.6	0.00			
H8	0°	14	1.82	23.4	69.8	0.00			
H9	90°	14	1.79	24.4	67.7	0.00			
H10	±45°	8	1.81	24.9	68.0	0.00			
H11			1.80	25.1	67.5	0.00			
H12			1.82	25.1	68.2	0.00			
H13			1.80	25.4	67.1	0.00			
H14			1.79	24.9	67.3	0.00			
H15			1.80	23.2	69.1	0.00			
H16			1.80	26.1	66.5	0.00			
H17			1.80	25.9	66.8	0.00			
H18			1.82	24.6	68.6	0.00			
H19	▼	▼	1.81	23.2	69.5	0.00			
H20	(1)	20	1.81	23.7	68.9	0.00			
H21			1.81	23.9	68.9	0.00			
H22			1.81	24.9	67.6	0.00			
H23			1.81	24.2	68.6	0.00			
H24			1.80	25.1	67.6	0.00			
H25			1.80	24.1	68.4	0.00			
H26			1.79	24.4	67.6	0.00			
H27	▼	▼	1.80	25.1	62.9	0.00		▼	▼

(1) (0,45,-45,0,0,-45,45,0,90,0)_s - 20 ply.

[illegible]

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LAMINATE PHYSICAL PROPERTIES

Material: T300/V378A

Lam. No.	Fiber Orient.	No. Plies	Spec. Grav.	Resin Content (% by wt)	Fiber Content (% by vol)	Void Content (% by vol)	Thick. per ply (10 ⁻³ in.)	Prepreg Lot/ Batch No.	Prepreg Spool/Roll No.
I-1	90°	14	1.56	23.5	68.1	3.17		2W4683	1
I-2	90°	14	1.59	22.0	70.7	1.53		2W4683	1
I-3	90°	8	1.58	23.7	68.9	1.92		2W4683	1
I-4	±45°	8	1.59	29.8	63.7	0.86		2W4683	1
I-5	±45°	8	1.61	24.6	69.4	-0.54		2W4683	1
I-6	±45°	8	1.58	26.8	66.1	0.58		2W4683	1
I-7	±45°	8	1.61	27.9	66.3	-1.70		2W4683	1
I-8	±45°	8	1.56	26.6	65.4	1.88		2W4683	1
I-9	±45°	8	1.59	28.3	65.1	-0.58		2W4683	1
I-10	±45°	8	1.61	27.4	66.8	-1.52		2W4683	1
I-11	±45°	8	1.56	27.3	64.8	1.66		2W4683	1
I-12	0/45/90	20	1.57	29.0	63.7	0.46		2W4683	1
I-13	0/45/90	20	1.57	25.2	67.1	1.75		2W4683	1
I-14	0/45/90	20	1.57	25.4	66.9	1.67		2W4683	1
I-15	90°	15	1.59	25.5	67.7	0.39		2W4683	1
I-17	0°	6	1.58	23.4	68.2	1.73		2W4683	1
I-18	90°	15	1.58	22.6	69.9	1.99		2W4683	1
I-19	90°	15	1.59	28.2	65.2	-0.54		2W4683	1
I-20	90°	15	1.57	25.7	66.7	1.58		2W4683	1
I-21	90°	15	1.57	27.9	64.7	0.83		2W4683	1
I-22	±45°	8	1.58	24.1	68.6	1.50		2W4683	1
I-35	0/90/45	20	1.58	26.6	66.3	0.65		2W4810	1
I-36	0/90/45	20	1.58	24.0	68.7	1.54		2W4810	1
I-37	0/90/45	20	1.58	26.0	66.8	0.84		2W4810	1
I-38	0/90/45	20	1.60	24.4	69.2	0.15		2W4810	1
I-39	0/90/45	20	1.59	24.9	68.3	0.63		2W4810	1

[illegible]

LAMINATE PHYSICAL PROPERTIES

Material: HyE 1076J

Lam. No.	Fiber Orient	No. Plies	Spec. Grav.	Resin Content (% by wt)	Fiber Content (% by vol)	Void Content (% by vol)	Thick. per ply (10 ⁻³ in.)	Prepreg Lot/ Batch No.	Prepreg Spool/Roll No.
J1	90°	14	1.62	26.3	67.1	-0.37		C1-285	1
J2	0°	14	1.61	23.8	68.9	1.13		C1-285	1
J3	±45°	8	1.62	26.2	67.1	-0.34		C1-285	1
J4	±45°	8	1.62	24.6	68.7	0.26		C1-285	1
J5	±45°	8	1.62	24.3	68.9	0.34		C1-285	1
J6	±45°	8	1.62	26.1	67.3	-0.28		C1-285	1
J7	±45°	8	1.61	24.7	68.5	0.40		C1-285	1
J8	±45°	8	1.62	25.2	68.1	0.05		C1-285	1
J9	±45°	8	1.62	26.2	67.2	-0.05		C1-285	1
J10	±45°	8	1.61	24.9	67.9	0.95		C1-285	1
J11	±45°	8	1.61	25.6	67.3	0.33		C1-285	1
J12	±45°	8	1.62	25.7	67.2	0.16		C1-285	1
J13	(1)	20	1.65	25.5	69.0	-1.75		C1-285	1
J14	(1)	20	1.61	25.1	67.7	0.69		C1-285	1
J15	(1)	20	1.62	25.6	67.7	-0.12		C1-285	1
J16	(1)	20	1.63	25.0	68.8	-0.73		C1-285	1
J17	(1)	20	1.62	24.8	68.5	0.18		C1-285	1
J18	0°	6	1.64	32.9	61.9	-3.95		C1-285	1
J19	0°	6	1.58	37.7	55.3	-1.85		C1-285	1
J20	(1)	20	1.62	24.1	69.1	0.42		C1-285	1
J21	(1)	20	1.60	25.4	67.0	1.18		C1-285	1
J22	(1)	20	1.62	24.6	68.6	0.23		C1-285	1
J23	(1)	20	1.62	24.4	68.9	0.10		C1-285	1
J24	(1)	20	1.62	24.8	68.5	0.17		C1-285	1
J25	(1)	20	1.63	24.9	68.8	-0.47		C1-285	1
J26	90°	15	1.63	24.0	69.7	-0.37		C1-285	1
J27	90°	15	1.64	24.2	69.9	-0.83		C1-285	1

(1) (0,45,-45,0,0,-45,45,0,90,0)_S - 20 ply.

[illegible]

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LAMINATE PHYSICAL PROPERTIES

Material: G-160/6535-1

Lam. No.	Fiber Orient.	No. Plies	Spec. Grav.	Resin Content (% by wt)	Fiber Content (% by vol)	Void Content (% by vol)	Thick. per ply (10 ⁻³ in.)	Prepreg Lot/ Batch No.	Prepreg Spool/Roll No.
K3	±45°	8	1.60	25.7	68.0	0.28			440
K4	±45°	8	1.60	26.6	67.1	-0.89			
K5	±45°	8	1.60	25.8	67.9	-0.60			
K6	±45°	8	1.61	26.1	68.0	-1.32			
K7	±45°	8	1.61	26.8	67.2	-1.36			
K8	±45°	8	1.60	25.6	67.9	-0.32			
K9	±45°	8	1.61	26.5	67.6	-1.48			
K10	±45°	8	1.61	26.3	67.6	-1.21			
K11	±45°	8	1.60	25.5	68.3	-0.70			
K12	0°	6	1.62	26.0	68.3	-2.13			
K13	0°	6	1.63	23.6	71.3	-1.92			
K14	90°	15	1.61	25.9	68.3	-1.47			
K15	90°	15	1.61	25.6	68.6	-1.37			
K16	90°	15	1.61	25.9	68.3	-1.49			
K17	90°	15	1.62	25.4	69.0	-1.49			
K18	90°	15	1.59	27.3	66.1	-0.19			
K19	90°	21	1.62	22.9	71.5	-1.00			
K20	0°	40	1.61	24.4	69.6	-0.72			
K21	0°	21	1.62	23.4	70.5	-0.37			
K24	(1)	20	1.61	26.3	67.8	-1.42			
K25	(1)	20	1.61	26.1	68.0	-1.33			
K26	(1)	20	1.61	25.3	68.7	-1.07			
K34	(2)	16	1.62	26.4	68.2	-2.06			441
K35	(2)	16	1.60	26.2	67.6	-0.95			
K36	(2)	16	1.61	26.9	67.3	-1.63			
K37	(3)	20	1.60	26.7	67.1	-0.70			
K38	(3)	20	1.60	26.6	67.3	-1.70			

(1) (0,45,-45,0,0,-45,45,0,90,0)_S-20 ply

(2) (0,45,-45,0,0,-45,45,0)_S-16 ply

(3) (0,90,45,-45,0,0,-45,45,0,0)_S-20 ply

[illegible]

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APPENDIX D
TENSION DATA

All of the tension data generated during this program are listed in this section. These data are summarized and presented in both tabular and graphical form in Sections 4.1 through 4.6.

The specimen numbering notation used in this and subsequent appendices is illustrated in the example below.

F 23-5

Indicates the material ————┐
 ├── specimen number from the panel
 └── panel number from which specimen
 was machined

F - T300/AFR800
G - SiC/5506
H - HyE 2034D
I - T300/V378A
J - HyE 1076J
K - G-160/6535-1

Test: Tension				Material: T300/APR800				
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pols. Ratio	Ultimate Strain (μ in/in)	Remarks
F1-4	0°	-67	178.6	20.37	178.6	0.32	8,400	
F3-7	0°	-67	178.9	20.38	178.9	0.33	8,200	
F4-2	0°	-67	212.1	21.46	212.1	0.32	9,400	
F4-16	0°	-67	191.5	20.95	191.5	0.33	8,700	
F5-12	0°	-67	172.2	21.21	172.2	0.30	7,900	
Avg.			186.7	20.87	186.7	0.32	8,520	
Std.Dev.			15.8	0.49	15.8	0.01	570	
F1-3	0°	72	186.0	18.85	186.0	0.31	9,000	
F3-1	0°	72	169.6	19.15	169.6	0.33	8,400	
F3-13	0°	72	161.6	18.39	161.6	0.27	8,200	
F4-8	0°	72	205.6	17.22	205.6	0.29	9,700	
F5-5	0°	72	175.1	19.86	175.1	0.35	8,200	
Avg.			179.6	18.69	179.6	0.31	8,700	
Std.Dev.			17.0	0.98	17.0	0.03	650	
F1-11	0°	260	174.3	20.14	174.3	0.29	8,400	
F3-3	0°	260	176.7	19.82	176.7	0.30	8,400	
F4-3	0°	260	204.0	20.40	204.0	0.28	9,400	
F5-7	0°	260	213.3	20.88	213.3	0.32	9,800	
F5-13	0°	260	201.2	20.76	201.2	0.34	9,200	
Avg.			193.9	20.40	193.9	0.31	9,040	
Std.Dev.			17.4	0.44	17.4	0.02	620	
F1-6	0°	350	185.8	19.51	185.8	0.37	9,200	
F1-16	0°	350	159.7	19.88	159.7	0.32	7,700	
F3-11	0°	350	147.5	19.39	147.5	0.40	7,500	
F4-7	0°	350	173.8	20.37	173.8	---	8,100	
F5-3	0°	350	200.9	20.22	200.9	0.33	9,400	
Avg.			173.5	19.87	173.5	0.36	8,380	
Std.Dev.			21.0	0.43	21.0	0.04	870	

Test: Tension				Material: AFR-800				
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
F7-8	90°	-67	4.55	1.56	4.55	---	2,940	
F8-8	90°	-67	4.58	1.63	1.60	---	2,875	
F9-10	90°	-67	5.19	1.58	5.19	---	3,015	
F11-5	90°	-67	2.80	1.70	1.20	---	1,695	
F12-2	90°	-67	6.31	1.70	1.93	---	3,825	
Avg.			4.69	1.63	2.89	---	2,870	
Std.Dev.			1.27	0.07	1.84	---	760	
F7-9	90°	72	4.90	1.47	4.90	---	3,325	
F8-9	90°	72	5.75	1.47	4.58	---	3,950	
F11-1	90°	72	5.14	1.49	4.26	---	3,450	
F12-5	90°	72	3.20	1.55	3.20	---	2,075	
F13-7	90°	72	3.93	1.44	3.93	---	2,750	
Avg.			4.58	1.48	4.17	---	3,110	
Std.Dev.			1.01	0.04	0.65	---	720	
F8-5	90°	260	5.56	1.38	5.56	---	4,050	
F9-9	90°	260	4.40	1.31	4.20	---	3,500	
F11-2	90°	260	4.33	1.39	2.46	---	3,200	
F12-8	90°	260	4.53	1.33	2.93	---	3,500	
F12-10	90°	260	4.59	1.41	3.78	---	3,290	
Avg.			4.68	1.36	3.79	---	3,510	
Std.Dev.			0.50	0.04	1.21	---	330	
F7-1	90°	350	5.19	1.20	2.08	---	4,550	
F8-3	90°	350	5.08	1.26	1.59	---	4,275	
F9-1	90°	350	4.80	1.12	3.72	---	4,350	
F12-7	90°	350	5.51	1.26	2.49	---	4,925	
F13-5	90°	350	6.53	1.09	4.40	---	6,450	
Avg.			5.42	1.19	2.86	---	4,910	
Std.Dev.			0.67	0.08	1.17	---	900	

Test: Tension		Material: AFR-800						
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
F23-5	±45°	-67	27.81	2.37	11.57	0.68	9,600+	
F24-1	±45°	-67	26.73	2.31	9.58	0.72	10,600+	
F25-7	±45°	-67	25.69	2.22	11.57	0.71	14,800	
F26-4	±45°	-67	25.24	2.10	6.09	0.62	16,000	
F27-10	±45°	-67	26.74	2.39	8.04	0.73	9,400+	
Avg.			26.44	2.28	9.37	0.69	12,080	
Std.Dev.			1.00	0.12	2.36	0.04	3,090	
F23-9	±45°	72	24.07	2.31	4.05	0.73	20,000	
F24-9	±45°	72	23.80	2.45	6.45	0.72	16,600	
F25-5	±45°	72	21.50	2.09	3.41	0.74	18,350	
F26-10	±45°	72	23.70	2.40	4.67	0.82	17,400	
F27-1	±45°	72	23.14	2.50	4.87	0.74	15,800	
Avg.			23.24	2.35	4.69	0.75	17,630	
Std.Dev.			1.03	0.16	1.14	0.04	1,630	
F23-11	±45°	260	18.0	2.26	5.53	0.78	23,100+	
F24-4	±45°	260	15.4	2.08	4.55	0.78	11,000	
F25-1	±45°	260	17.2	2.24	4.56	0.78	22,000	
F26-8	±45°	260	17.5	2.10	5.22	0.80	32,000	
F27-3	±45°	260	15.8	2.01	5.01	0.77	12,800+	
Avg.			16.8	2.14	4.93	0.78	21,580+	
Std.Dev.			1.12	0.11	0.36	0.01	7,090+	
F23-3	±45°	350	17.06	1.61	2.05	0.86	46,800+	
F24-7	±45°	350	16.37	1.73	2.67	0.94	38,800+	
F25-10	±45°	350	17.13	1.71	1.78	0.92	34,000+	
F26-2	±45°	350	15.34	1.52	1.96	0.90	37,900+	
F27-5	±45°	350	15.43	1.45	2.17	0.79	39,750+	
Avg.			16.27	1.62	2.13	0.88	39,450	
Std.Dev.			0.86	0.12	0.34	0.06	4,650	

Test: Tension			Material: SIC/5506					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (μ in/in)	Remarks
G23-2	0°	-67	204.9	33.43	160.5	0.24	7,500	
G23-5	0°	-67	198.8	31.53	101.8	0.24	7,400	
G23-12	0°	-67	235.4	31.40	157.5	0.18	7,600	
G23-14	0°	-67	233.1	33.50	80.4	0.22	7,900	
G23-17	0°	-67	235.8	31.53	147.4	0.24	7,600	
Avg.			221.6	32.28	129.5	0.22	7,600	
Std.Dev.			18.2	1.09	36.2	0.03	190	
G23-1	0°	72	232.1	32.05	92.6	---	8,100	
G23-6	0°	72	241.7	33.50	83.1	0.20	8,800	
G23-11	0°	72	220.3	33.09	58.2	0.24	7,100	
G23-16	0°	72	222.9	32.75	80.6	0.23	7,100	
G23-19	0°	72	228.5	35.59	42.7	0.24	7,200	
Avg.			229.1	33.40	71.4	0.23	7,660	
Std.Dev.			8.4	1.34	20.4	0.02	760	
G23-3	0°	260	188.1	33.50	85.8	0.30	6,300	failed @ tab
G23-9	0°	260	205.0	32.76	99.6	0.24	7,300	failed @ tab
G23-10	0°	260	178.8	33.36	74.7	0.20	5,200+	failed @ tab
Avg.			190.6	33.21	86.7	0.25	6,800	*
std.Dev.			13.3	0.39	12.5	0.05	---	
G23-13	0°	350	181.0	35.80	34.9	0.23	5,400+	
G23-15	0°	350	161.7	31.59	69.8	0.23	4,600	failed @ tab
G23-18	0°	350	180.7	31.72	67.4	0.49	5,400+	
Avg.			174.5	33.04	57.4	0.32	5,130+	
Std.Dev.			11.0	2.39	19.5	0.15	460	
				</				

*Excludes G23-10 on which strain gage malfunctioned before end of test

Test: Tension			Material: SIC/5506					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (μ in/in)	Remarks
G9-7	90°	-67	10.27	3.96	5.38	---	2,880	
G22-2	90°	-67	10.44	3.66	7.90	---	2,920	
G24-3	90°	-67	8.33	3.90	6.57	---	2,250	
G25-4	90°	-67	11.55	3.93	4.74	---	3,380	
G26-5	90°	-67	8.31	3.88	6.26	---	2,310	
Avg.			9.78	3.86	6.17	---	2,750	
Std.Dev.			1.42	0.12	1.21	---	470	
G9-3	90°	72	8.99	2.96	4.98	---	3,400	
G22-1	90°	72	10.43	3.13	4.82	---	3,910	
G24-2	90°	72	9.78	3.07	3.61	---	3,740	
G25-3	90°	72	9.62	2.89	3.92	---	3,760	
G26-4	90°	72	9.72	2.90	3.86	---	3,830	
Avg.			9.71	2.99	4.24	---	3,730	
Std.Dev.			0.51	0.10	0.62	---	190	
G9-4	90°	260	6.34	2.09	2.78	---	4,760	
G22-3	90°	260	6.56	1.88	2.76	---	4,990	
G24-1	90°	260	6.38	2.17	2.64	---	4,090	
G25-6	90°	260	6.55	1.97	3.10	---	4,640	
G26-1	90°	260	6.39	1.77	2.91	---	5,000	
Avg.			6.44	1.97	2.84	---	4,700	
Std.Dev.			0.104	0.16	0.18	---	370	
G9-9	90°	350	3.84	0.91	1.62	---	6,000	
G22-5	90°	350	4.39	1.10	1.65	---	7,500	
G24-4	90°	350	4.92	1.19	1.96	---	8,250	
G25-5	90°	350	4.40	1.13	1.76	---	8,500	
G-26-2	90°	350	4.14	0.89	1.76	---	7,500	
Avg.			4.34	1.04	1.75	---	7,550	
Std.Dev.			0.40	0.13	0.13	---	980	

Material: SIC/5506								
Test: Tension			Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (μ in/in)	Remarks
Spec. No.	Fiber Orien.	Test Temp. (°F)						
G14-3	±45°	-67	20.63	3.93	5.70	0.66	9,350	
G14-4	±45°	-67	20.24	3.93	6.48	0.73	9,800	
G15-2	±45°	-67	20.41	3.50	5.97	0.59	N.A.	Gage failed during test
G17-3	±45°	-67	17.69	3.50	5.96	0.59	7,050	
G17-6	±45°	-67	19.66	3.67	7.13	0.72	8,200	
Avg.			19.72	3.71	6.25	0.66	8,600	
Std.Dev.			1.19	0.22	0.57	0.07	123	
G14-5	±45°	72	17.69	2.65	6.76	0.69	15,950	
G15-1	±45°	72	16.52	2.96	4.80	0.66	14,700	
G15-4	±45°	72	17.52	3.08	4.81	0.80	15,900	
G17-1	±45°	72	17.95	3.40	4.90	0.71	15,200	
G17-4	±45°	72	16.92	2.75	4.42	0.86	15,800	
Avg.			17.32	2.97	5.14	0.74	15,510	
Std.Dev.			0.58	0.30	0.92	0.08	540	
G14-7	±45°	260	11.57	1.96	1.86	0.93	42,000+	Strain exceeded
G16-4	±45°	260	12.45	1.35	1.32	0.95	40,500+	gage limit
G17-2	±45°	260	12.25	1.86	2.04	0.78	34,500+	
G17-7	±45°	260	10.66	1.57	1.13	1.02	23,500+	
G17-8	±45°	260	10.69	1.40	1.57	0.76	35,000+	
Avg.			11.52	1.63	1.59	0.89	35,100+	
Std.Dev.			0.84	0.27	0.37	0.11	7,270	
G14-1	±45°	350	7.98	0.77	1.44	0.57	35,000+	Strain exceeded
G14-2	±45°	350	7.90	0.39	0.88	0.75	35,000+	gage limit
G14-6	±45°	350	7.90	0.65	0.98	0.71	20,000+	
G15-3	±45°	350	8.17	0.39	0.66	0.83	29,500+	
G17-5	±45°	350	7.67	0.36	0.67	0.83	35,000+	
Avg.			7.93	0.51	0.93	0.74	30,900+	
Std.Dev.			0.18	0.19	0.32	0.11	6,540	

Test: Tension		Material: SIC/5506						
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (min/in)	Remarks
G33-7	0/±45/90	72	125.6	21.33	19.6	N.A.	5,800	
G36-6	0/±45/90	72	N.A.	23.67	21.8	0.18	N.A.	Failed at tab end
G39-7	0/±45/90	72	105.9	19.42	39.3	0.41	5,575	
G41-5	0/±45/90	72	118.0	18.92	47.4	0.37	5,775	Failed at tab end
G44-6	0/±45/90	72	125.2	19.38	65.0	0.28	5,750	
Avg.			108.6	20.54	38.6	0.31	5,725	
Std. Dev.			24.9	1.97	18.8	0.10	100	
G33-2	0/±45/90	260	111.7	19.0	35.1	0.52	5,650+	*
G34-9	0/±45/90	260	113.6	19.0	36.6	0.61	5,750+	*
G39-3	0/±45/90	260	126.2	19.1	66.5	0.34	5,900	
G39-4	0/±45/90	260	107.4	19.6	43.6	0.40	5,650	
G41-9	0/±45/90	260	122.3	18.4	63.6	0.39	5,750	
Avg.			117.2	19.0	49.1	0.45	5,740	
Std. Dev.			7.7	0.4	15.0	0.11	100	
G34-3	0/±45/90	350	107.0	18.7	50.1	0.46	5,700	
G40-2	0/±45/90	350	115.6	17.8	62.6	0.46	4,425	*
G41-6	0/±45/90	350	102.1	17.3	53.5	0.33	5,800	
G44-5	0/±45/90	350	103.9	18.4	74.9	0.37	4,850	
Avg.			107.2	18.1	60.3	0.40	5,190	
Std. Dev.			6.0	0.6	11.1	0.06	670	
G32-8	0/±45/90	72	105.8					Based on net cross-sectional area. Specimens
G35-2	0/±45/90	72	97.6					had a 0.1935 inch dia-
G40-4	0/±45/90	72	104.2					meter hole in center of
G44-1	0/±45/90	72	100.2					gage section.
G44-3	0/±45/90	72	104.7					
Avg.			102.5					
Std. Dev.			3.5					

*Tabs debonded, retabbed and tested for strength only, elastic data taken from first test

Material: HVE 2034D									
Test: Tension			Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (µin/in)	Remarks
Spec. No.	Fiber Orien.								
H1-3	0°		-67	149.6	51.12	149.6	---	2700	gage failed
H1-10	0°		-67	108.9	50.61	108.9	0.36	---	tabs debonded
H2-4	0°		-67	105.3	72.46	105.3	---	1500	gage failed
H2-13	0°		-67	90.7	45.41	90.7	0.25	1900	
H1-17	0°		-67	157.0	60.00	157.0	0.29	2500	
Avg.				122.3	55.92	122.3	0.30	2150	
Std.Dev.				29.2	10.63	29.2	0.06	550	
H1-9	0°		72	151.6	41.75	151.6	0.03	2800	
H1-13	0°		72	80.3	47.81	80.3	0.10	2000	
H1-16	0°		72	72.1	47.71	72.1	0.45	1400	
H2-6	0°		72	130.7	41.67	130.7	0.18	2500	
H2-15	0°		72	97.5	43.54	97.5	0.35	1700	
Avg.				106.5	44.50	106.5	0.22	2080	
Std.Dev.				33.8	3.07	33.8	0.17	570	
H1-1	0°		260	96.5	44.90	96.5	0.24	1900	gage failed
H1-12	0°		260	167.3	47.81	167.3	0.47	3100	
H1-15	0°		260	120.2	47.99	120.2	0.27	2700	
H2-5	0°		260	137.4	53.76	137.4	0.34	2500	
H2-10	0°		260	146.0	47.62	146.0	0.27	2800	
Avg.				133.5	48.42	133.5	0.32	2780	excludes H1-1
Std.Dev.				26.7	3.25	26.7	0.09	250	
H1-2	0°		350	145.5	46.39	145.5	0.25	2800	
H1-7	0°		350	140.3	47.71	140.3	0.40	2800	
H2-1	0°		350	130.0	46.30	130.0	0.30	2700	
H2-9	0°		350	165.0	55.44	165.0	0.29	3200	
H2-11	0°		350	94.3	47.62	94.3	0.27	1800	
Avg.				135.0	48.69	135.0	0.30	2660	
Std.Dev.				26.1	3.83	26.1	0.06	520	

Test: Tension			Material: HVE 2034D					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (µin/in)	Remarks
H3-3	90°	-67	2.34	0.86	2.34	---	2400	
H3-7	90°	-67	2.68	1.06	2.68	---	2600	
H6-6	90°	-67	1.56	0.99	1.56	---	1800	
H7-5	90°	-67	1.72	0.87	1.72	---	1700	
H7-10	90°	-67	2.64	0.82	2.64	---	2800	
Avg.			2.19	0.92	2.19	---	2260	
Std.Dev.			0.52	0.10	0.52	---	490	
H3-1	90°	72	1.81	0.84	1.81	---	2100	
H4-5	90°	72	2.29	0.88	2.29	---	2500	
H7-3	90°	72	1.86	0.86	1.86	---	2100	
H6-7	90°	72	2.34	0.84	2.34	---	2800	
H4-9	90°	72	2.06	0.92	2.06	---	2300	
Avg.			2.07	0.87	2.07	---	2360	
Std.Dev.			0.24	0.03	0.24	---	300	
H3-6	90°	260	1.46	0.79	1.46	---	1900	
H4-4	90°	260	2.21	0.77	2.21	---	2900	
H7-2	90°	260	1.24	0.79	1.24	---	1600	
H7-8	90°	260	1.94	0.79	1.94	---	2500	
H7-9	90°	260	1.80	0.81	1.80	---	2200	
Avg.			1.73	0.79	1.73	---	2220	
Std.Dev.			0.38	0.01	0.38	---	510	
H4-2	90°	350	1.92	0.91	1.10	---	2300	
H4-10	90°	350	0.87	1.12	0.81	---	1000	
H6-3	90°	350	1.24	0.91	0.68	---	1600	
H6-9	90°	350	1.20	0.93	0.77	---	1500	
H7-7	90°	350	1.75	0.90	1.15	---	2300	
Avg.			1.40	0.96	0.90	---	1740	
Std.Dev.			0.43	0.10	0.21	---	560	

Test:		Tension		Material: HYE 2034D				
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (µin/in)	Remarks
H11-8	±45°	-67	11.67	3.40	4.17	0.77	5000	
H16-4	±45°	-67	12.24	3.50	3.92	0.71	4400	
H17-4	±45°	-67	11.62	3.50	4.65	0.73	4000	
H17-7	±45°	-67	12.45	3.43	4.69	0.71	5000	
H12-7	±45°	-67	11.34	3.70	3.90	0.80	4100	
Avg.			11.86	3.50	4.26	0.74	4500	
Std.Dev.			0.46	0.11	0.38	0.04	480	
H11-7	±45°	72	11.02	2.84	4.03	0.91	5600	
H13-8	±45°	72	11.00	2.73	4.87	0.61	5100	
H15-4	±45°	72	10.78	2.71	4.51	1.00	6800	
H15-5	±45°	72	11.18	2.78	4.75	0.89	5500	
H15-7	±45°	72	10.29	2.65	4.76	0.89	5900	
Avg.			10.85	2.74	4.58	0.87	5780	
Std.Dev.			0.35	0.07	0.34	0.12	640	
H10-2	±45°	260	9.35	2.44	3.05	0.75	6560	
H12-3	±45°	260	9.39	2.51	3.38	0.75	5380	
H13-1	±45°	260	9.75	2.50	2.50	0.88	8900	
H14-10	±45°	260	8.95	2.38	3.33	0.88	5660	
H17-6	±45°	260	9.49	1.32	5.24	1.00	5460	
Avg.			9.39	2.23	3.50	0.85	6390	
Std.Dev.			0.29	0.51	1.03	0.11	1480	
H10-5	±45°	350	8.72	2.56	2.82	0.80	7100	
H11-9	±45°	350	8.42	2.22	2.44	1.06	7100	
H14-5	±45°	350	9.08	2.02	2.90	0.83	9280	
H18-2	±45°	350	9.13	2.79	3.51	1.04	7100	
H19-4	±45°	350	8.44	2.45	3.06	1.10	7800	
Avg.			8.76	2.41	2.95	0.96	7680	
Std.Dev.			0.34	0.30	0.39	0.14	950	

Test: Tension		Material: HVE 2034D						
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
H20-10	0/±45/90°	72	81.21	29.67	62.31	*	2700	*All 90° strain measurements incorrect due to
H21-5	0/±45/90°	72	80.80	30.77	80.80	*	2600	recorder error--avg.
H22-4	0/±45/90°	72	68.37	27.61	61.06	*	2450	value from extra
H25-2	0/±45/90°	72	83.03	27.44	65.85	*	3280	specimen tested later.
H33-10	0/±45/90°	72	65.70	26.58	65.70	*	2600	
Avg.			75.82	28.41	67.14	0.42	2730	
Std.Dev.			8.12	1.74	7.92		320	
H21-8	0/±45/90°	260	82.73	28.59	82.73	0.35	3000	
H22-1	0/±45/90°	260	81.39	26.16	81.39	0.40	2800	
H22-6	0/±45/90°	260	80.36	25.64	80.36	0.45	----	gage failed
H25-1	0/±45/90°	260	88.17	26.71	88.17	0.44	----	gage failed
H25-3	0/±45/90°	260	86.27	26.16	86.27	0.36	3500	
Avg.			83.78	26.65	83.78	0.40	3100	
Std.Dev.			3.32	1.15	3.32	0.04	360	
H22-2	0/±45/90°	350	90.84	28.20	90.84	0.46	3000	
H23-3	0/±45/90°	350	89.90	33.36	89.90	0.42	2700	
H23-4	0/±45/90°	350	75.87	22.35	75.87	0.27	2500	
H27-4	0/±45/90°	350	85.86	27.39	85.86	0.39	2800	
H33-1	0/±45/90°	350	71.43	28.57	71.43	0.38	2600	
Avg.			82.78	27.98	82.78	0.38	2720	
Std.Dev.			8.69	3.92	8.69	0.07	190	
H20-4	0/±45/90°	72	67.14					Based on net cross-
H20-9	0/±45/90°	72	66.22					sectional area. Speci-
H21-6	0/±45/90°	72	61.20					mens had a 0.1935 inch
H21-10	0/±45/90°	72	65.23					diameter hole in center
H26-2	0/±45/90°	72	63.80					of gage section.
Avg.			64.72					
Std. Dev.			2.33					

Test: Tension			Material: T300/V378A					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (µin/in)	Remarks
I16-1	0°	-67	172.4	19.31	172.4	0.33	6,800	
I16-5	0°	-67	238.3	20.12	238.3	0.29	11,040	
I17-6	0°	-67	240.8	20.28	240.8	0.29	17,200	
I17-9	0°	-67	210.0	19.53	210.0	0.31	10,300	
I17-17	0°	-67	250.0	20.90	250.0	0.31	11,300	
Avg.			222.3	20.03	222.3	0.31	10,130	
Std.Dev.			31.7	0.63	31.7	0.02	1,900	
I16-7	0°	72	189.7	19.58	189.7	0.29	9,060	
I16-8	0°	72	238.4	20.24	238.4	0.26	8,960	
I17-4	0°	72	250.6	19.71	250.6	0.32	11,800	
I17-5	0°	72	224.1	20.66	224.1	0.27	11,000	
I17-14	0°	72	248.4	20.32	248.4	0.34	11,720	
Avg.			230.2	20.10	230.2	0.30	10,510	
Std.Dev.			25.0	0.45	25.0	0.03	1,400	
I16-2	0°	350	183.9	21.73	183.9	0.31	10,440	
I16-4	0°	350	213.0	21.00	213.0	0.34	10,000	
I16-9	0°	350	189.5	20.95	189.5	0.29	8,400	
I17-3	0°	350	224.7	24.51	224.7	0.37	9,800	
I17-8	0°	350	239.4	22.50	239.4	0.36	10,200	
Avg.			210.1	22.14	210.1	0.33	9,770	
Std.Dev.			23.4	1.47	23.4	0.03	800	
I16-3	0°	450	213.4	19.37	213.4	0.29	10,360	
I16-6	0°	450	200.8	18.90	200.8	0.30	11,400	
I17-1	0°	450	208.2	18.09	208.2	0.36	11,340	
I17-12	0°	450	223.8	20.04	223.8	0.37	11,100	
I17-16	0°	450	240.3	19.47	240.3	0.29	11,700	
Avg.			217.3	18.77	217.3	0.32	11,180	
Std.Dev.			15.3	1.07	15.3	0.04	510	

Test: Tension		Material: T300/V378A						
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
I18-5	90°	-67	6.67	1.39	6.67	---	4,875	
I18-8	90°	-67	6.69	1.41	6.69	---	4,745	
I19-1	90°	-67	4.68	1.41	4.68	---	3,365	
I20-4	90°	-67	5.12	1.41	5.12	---	4,515	
I21-8	90°	-67	5.96	1.39	5.96	---	4,225	
Avg.			5.82	1.40	5.82		4,345	
Std.Dev.			0.91	0.01	0.91		600	
I15-5	90°	72	4.74	1.27	4.74	---	3,735	
I18-2	90°	72	5.68	1.29	4.18	---	4,420	
I19-8	90°	72	6.11	1.35	2.44	---	4,685	
I20-7	90°	72	4.96	1.32	3.56	---	3,760	
I21-4	90°	72	5.33	1.30	2.85	---	4,115	
Avg.			5.37	1.31	3.55		4,140	
Std.Dev.			0.55	0.03	0.94		410	
I15-3	90°	350	4.42	1.04	3.45	---	4,275	
I18-8	90°	350	4.08	1.04	3.81	---	3,950	
I19-5	90°	350	4.97	1.08	4.09	---	4,700	
I20-9	90°	350	4.02	1.09	3.16	---	3,650	
I21-1	90°	350	4.44	1.12	3.62	---	4,085	
Avg.			4.84	1.07	3.63		4,130	
Std.Dev.			0.38	0.03	0.35		390	
I15-10	90°	450	3.48	1.03	2.08	---	3,365	
I18-7	90°	450	3.71	0.96	2.04	---	3,910	
I19-9	90°	450	4.51	1.00	2.17	---	4,640	
I20-1	90°	450	4.69	0.99	3.44	---	4,825	
I21-10	90°	450	4.66	1.01	3.03	---	4,705	
Avg.			4.21	1.00	2.55		4,290	
Std.Dev.			0.57	-0.02	0.64		630	

Test: Tension		Material: T300/V378A						
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
I4-6	±45°	-67	22.38	3.17	9.27	0.73	9,620	
I5-10	±45°	-67	23.12	3.35	8.63	0.71	8,800	
I6-8	±45°	-67	20.95	2.90	8.81	0.61	8,280	
I9-1	±45°	-67	20.84	3.05	7.52	0.71	10,300	
I10-5	±45°	-67	20.33	3.16	7.38	0.73	8,100	
Avg.			21.52	3.13	8.32	0.70	9,020	
Std.Dev.			1.17	0.16	0.83	0.05	930	
I4-3	±45°	72	19.18	2.97	7.36	0.60	8,000	*
I9-9	±45°	72	22.14	2.98	6.19	0.63	4,500	*
I10-7	±45°	72	21.42	2.91	6.29	0.53	12,000	
I11-5	±45°	72	21.96	2.97	6.42	0.63	9,800	*
I22-1	±45°	72	21.76	2.98	5.49	0.58	12,200	
Avg.			21.29	2.96	6.35	0.59	12,100	
Std.Dev.			1.21	0.03	0.67	0.04	---	
I8-6	±45°	350	16.26	2.39	5.36	0.93	18,200	
I9-8	±45°	350	16.17	2.64	4.04	1.08	23,600	
I10-10	±45°	350	14.96	2.41	4.83	0.95	39,400	
I11-4	±45°	350	16.77	2.58	3.95	1.03	6,800	*
I22-2	±45°	350	16.43	2.65	4.29	---	10,200	*
Avg.			16.12	2.54	4.49	1.00	27,070	
Std.Dev.			0.69	0.13	0.59	0.07	11,020	
I5-1	±45°	450	14.46	2.14	3.98	0.81	20,000	
I8-7	±45°	450	14.92	2.32	3.06	0.78	20,400	
I9-6	±45°	450	15.02	2.18	2.45	0.87	20,600	
I10-9	±45°	450	14.88	2.02	4.26	0.81	20,200	
I11-8	±45°	450	15.41	2.16	3.56	0.82	20,400	
Avg.			14.94	2.16	3.46	0.82	20,320	
Std.Dev.			0.34	0.11	0.73	0.03	230	

*Not included in ult. strain avg. and std. dev.; strain gage failed prior to end of test

Test: Tension			Material: V178					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
I128-4	0/±45/90	72	109.7	13.33	109.7	0.57	10,750	
I129-4	0/±45/90	72	102.6	12.26	102.6	0.58	10,200	
I137-3	0/±45/90	72	130.4	14.83	130.4	0.53	10,600	
I139-3	0/±45/90	72	125.4	14.80	125.4	0.63	10,500	
I140-3	0/±45/90	72	130.4	14.58	130.4	0.65	10,900	
Avg.			119.7	13.96	119.7	0.59	10,590	
Std.Dev.			12.8	1.13	12.8	0.05	270	
I112-3	0/±45/90	350	112.9	15.39	112.9	---	7,750	
I113-3	0/±45/90	350	107.7	9.83	107.7	0.66	10,250	
I125-3	0/±45/90	350	99.9	13.43	99.9	0.53	8,750	
I130-3	0/±45/90	350	90.3	12.54	90.3	0.58	9,000	
I140-2	0/±45/90	350	119.6	15.89	119.6	0.69	9,350	
Avg.			106.1	13.41	106.1	0.62	9,020	
Std.Dev.			11.4	2.43	11.4	0.07	910	
I112-10	0/±45/90	450	88.9	12.43	88.9	0.34	7,000	
I113-10	0/±34/90	450	102.4	13.68	102.4	0.57	9,000	
I126-3	0/±45/90	450	111.6	12.14	111.6	0.63	10,650	
I136-8	0/±45/90	450	115.3	13.86	115.3	0.50	10,000	
I138-10	0/±45/90	450	119.2	13.62	119.2	0.56	10,250	
Avg.			107.5	13.15	107.5	0.52	9,380	
Std.Dev.			12.1	0.80	12.1	0.11	1,460	
I112-1	0/±45/90	72	86.4	---	---	---	---	These specimens had a
I125-2	0/±45/90	72	79.9	---	---	---	---	0.1935 inch diameter
I130-2	0/±45/90	72	83.0	---	---	---	---	hole in the center of
I135-1	0/±45/90	72	103.7	---	---	---	---	the gage section.
I138-1	0/±45/90	72	112.5	---	---	---	---	Strength is based on
Avg.			93.1					net cross-sectional
Std.Dev.			14.2					area.

Test: Tension		Material: HyE 1076J						
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
J18-3	0°	-67	198.4	20.97	198.4	0.33	9000	
J18-11	0°	-67	197.0	20.12	197.0	0.30	8900	
J18-17	0°	-67	213.5	20.68	213.5	0.29	4500	gage failed
J19-4	0°	-67	202.6	19.64	202.6	0.34	8500	
J19-8	0°	-67	172.5	20.83	172.5	0.33	8000	
Avg.			196.8	20.45	196.8	0.32	8600	excludes J18-17
Std.Dev.			15.1	0.56	15.1	0.02	450	
J18-1	0°	72	190.8	18.37	190.8	0.35	10100	
J18-5	0°	72	194.4	20.03	194.4	0.31	10700	
J18-15	0°	72	219.4	20.43	219.4	0.31	10000	
J19-1	0°	72	214.5	18.15	214.5	0.29	10800	
J19-6	0°	72	216.4	19.49	216.4	0.33	10500	
Avg.			207.1	19.29	207.1	0.32	10420	
Std.Dev.			13.4	1.00	13.4	0.02	360	
J18-4	0°	260	211.5	22.53	211.5	0.31	9500	
J18-8	0°	260	254.7	21.19	254.7	0.30	10200	
J18-12	0°	260	224.6	21.64	224.6	0.36	9500	
J19-5	0°	260	235.2	22.93	235.2	0.29	10500	
J19-7	0°	260	235.8	22.61	235.8	0.30	9800	
Avg.			232.3	22.38	232.3	0.31	9900	
Std.Dev.			15.9	0.49	15.9	0.03	440	
J19-2	0°	350	228.9	22.28	228.9	0.33	5600	gage failed
J19-3	0°	350	227.4	20.16	227.4	0.33	10700	
J18-2	0°	350	242.2	23.94	242.2	0.39	9800	
J18-10	0°	350	224.9	21.71	224.9	0.37	9600	
J18-16	0°	350	218.7	22.49	218.7	0.32	9600	
Avg.			228.4	22.12	228.4	0.35	9930	excludes J19-2
Std.Dev.			8.6	1.37	8.6	0.03	530	

Test: Tension			Material: HYE 1076J					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (μin/in)	Remarks
J26-6	90°	-67	6.29	1.88	6.29	---	3100	
J27-3	90°	-67	3.23	1.78	3.23	---	1900	
J28-3	90°	-67	3.96	1.49	3.96	---	2500	
J29-2	90°	-67	5.31	1.68	3.11	---	3300	
J29-4	90°	-67	4.85	1.60	4.85	---	3000	
Avg.			4.73	1.69	4.29	---	2760	
Std.Dev.			1.19	0.15	1.32	---	560	
J26-1	90°	72	6.13	1.37	6.13	---	3900	
J26-5	90°	72	4.93	1.39	4.93	---	3200	
J28-1	90°	72	6.17	1.34	6.17	---	4300	
J29-1	90°	72	6.52	1.33	6.52	---	4600	
J30-2	90°	72	4.53	1.28	4.53	---	3500	
Avg.			5.66	1.34	5.66	---	3900	
Std.Dev.			0.87	0.04	0.87	---	570	
J26-8	90°	260	3.64	1.55	3.64	---	2100	
J27-8	90°	260	4.68	1.39	4.68	---	3400	
J28-9	90°	260	4.11	1.40	4.11	---	2800	
J29-8	90°	260	3.76	1.37	3.76	---	2600	
J30-7	90°	260	2.87	1.16	2.87	---	2300	
Avg.			3.81	1.37	3.81	---	2640	
Std.Dev.			0.66	0.14	0.66	---	500	
J26-3	90°	350	3.59	1.43	3.59	---	2300	
J27-2	90°	350	3.59	1.29	3.59	---	2800	
J28-5	90°	350	3.67	1.25	3.67	---	2800	
J29-5	90°	350	3.83	1.27	3.83	---	3000	
J30-3	90°	350	2.67	1.25	2.67	---	2200	
Avg.			3.47	1.30	3.47	---	2620	
Std.Dev.			0.46	0.08	0.46	---	350	

Test: Tension				Material: EYE 1076M				
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (µin/in)	Remarks
J4-3	±45°	-67	26.77	3.25	11.02	0.64	10700	
J6-2	±45°	-67	30.92	2.93	10.00	0.68	15300	
J8-2	±45°	-67	26.40	3.17	16.53	0.49	9400	
J10-2	±45°	-67	26.68	3.12	18.31	0.57	10200	
J11-3	±45°	-67	26.68	3.29	12.19	0.48	10000	
Avg.			27.49	3.16	13.61	0.57	11120	
Std.Dev.			1.92	0.14	3.62	0.09	2380	
J3-2	±45°	72	22.00	2.96	6.83	0.62	10300	gage failed
J5-6	±45°	72	22.18	3.16	6.08	0.68	13100	
J8-2	±45°	72	22.17	3.17	4.19	0.71	6200	gage failed
J11-2	±45°	72	22.73	3.00	9.25	0.65	11200	
J12-2	±45°	72	22.33	3.09	5.74	0.67	10700	
Avg.			22.28	3.08	6.42	0.67	11670	omits J3-2 & J8-2
Std.Dev.			0.28	0.10	1.85	0.03	1270	
J3-1	±45°	260	15.55	2.92	4.60	0.69	10400	
J5-1	±45°	260	15.81	3.11	3.58	0.71	14400	
J7-1	±45°	260	17.44	3.04	4.86	0.66	16200	
J9-1	±45°	260	16.90	3.41	4.64	0.79	20000	
J11-1	±45°	260	16.77	2.99	4.13	0.75	33400	
Avg.			16.49	3.09	4.36	0.73	18880	
Std.Dev.			0.79	0.19	0.51	0.05	8820	
J3-6	±45°	350	16.72	2.65	3.99	0.67	20000	gage failed
J4-2	±45°	350	16.37	2.84	5.19	0.74	32000	
J7-6	±45°	350	13.71	2.42	4.24	0.77	36800	
J9-7	±45°	350	15.33	2.81	3.78	0.70	8000	gage failed
J11-8	±45°	350	15.85	2.68	3.87	0.70	16000	gage failed
Avg.			16.60	2.68	4.21	0.71	34400	only J4-2 & J7-6 included
Std.Dev.			1.29	0.17	0.57	0.04	---	

Test: Tension			Material: HYE 1076J					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
J15-6	0/±45/90°	72	108.9	10.49	108.9	0.37	10200	
J17-5	0/±45/90°	72	115.0	11.00	115.0	0.36	10200	
J21-6	0/±45/90°	72	121.4	11.64	121.4	0.36	11000	
J23-4	0/±45/90°	72	110.8	11.17	110.8	0.39	10300	
J25-5	0/±45/90°	72	128.1	11.66	128.1	0.37	11400	
Avg.			116.8	11.19	116.8	0.37	10620	
Std.Dev.			7.9	0.49	7.9	0.01	550	
J13-6	0/±45/90°	260	112.2	12.46	112.2	0.45	8300	
J14-7	0/±45/90°	260	127.0	11.03	127.0	0.37	10300	
J17-4	0/±45/90°	260	121.1	12.36	121.1	0.39	10400	
J21-8	0/±45/90°	260	123.9	12.64	123.9	0.42	9900	
J23-5	0/±45/90°	260	116.2	12.50	116.2	0.39	9400	
Avg.			120.1	12.20	120.1	0.40	9780	
Std.Dev.			5.9	0.66	5.9	0.03	630	
J14-6	0/±45/90°	350	109.3	10.87	109.3	0.38	10500	
J16-6	0/±45/90°	350	114.2	11.24	114.2	0.29	9900	
J20-6	0/±45/90°	350	119.8	12.17	119.8	0.37	9500	
J22-6	0/±45/90°	350	126.3	12.83	126.3	0.37	7600	gage failed
J24-4	0/±45/90°	350	121.1	12.36	121.1	0.38	9700	
Avg.			118.1	11.89	118.1	0.36	9900	omits J22-6
Std.Dev.			6.6	0.81	6.6	0.04	430	omits J22-6
J13-2	0/±45/90°	72	86.8					These specimens had a
J14-2	0/±45/90°	72	93.4					0.1935 inch diameter
J16-2	0/±45/90°	72	99.1					hole in the center of
J21-2	0/±45/90°	72	84.5					the gage section. Strength
J25-1	0/±45/90°	72	78.6					is based on net cross-
Avg.			88.5					sectional area.
Std.Dev.			8.0					

Test:		Tension		Material: G-160/6535-1				
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
K12-4	0°	-67	213.8	18.39	213.8	0.35	11500	
K12-8	0°	-67	154.8	17.80	154.8	0.29	8450	
K13-1	0°	-67	176.4	18.65	176.4	0.37	9250	
K13-8	0°	-67	168.8	19.23	168.8	0.28	8900	
K13-5	0°	-67	148.3	18.39	148.3	0.27	7800	
Avg.			172.4	18.49	172.4	0.31	9180	
Std.Dev.			25.7	0.52	25.7	0.04	1410	
K12-2	0°	72	170.6	18.94	170.6	0.31	8500	
K12-6	0°	72	174.0	18.09	174.0	0.31	9100	
K13-4	0°	72	164.3	17.64	164.3	0.31	8640	
K13-14	0°	72	180.0	19.05	180.0	0.34	9000	
K13-7	0°	72	148.4	18.98	148.4	0.33	7400	
Avg.			167.5	18.54	167.5	0.32	8530	
Std.Dev.			12.1	0.64	12.1	0.01	680	
K12-1	0°	260	161.7	20.51	156.0	0.33	9200	
K12-5	0°	260	166.0	22.02	166.0	0.36	8400	
K13-3	0°	260	166.8	20.37	166.8	0.38	7900	
K13-10	0°	260	168.6	21.26	168.6	0.35	7100	
K13-17	0°	260	150.0	21.39	150.0	0.38	6700	
Avg.			162.6	21.11	161.5	0.36	7820	
Std.Dev.			7.5	0.68	8.1	0.02	940	
K12-3	0°	350	190.0	19.74	170.7	0.22	9450	
K12-7	0°	350	151.9	19.59	148.4	0.30	8000	
K13-2	0°	350	194.2	19.05	194.2	0.24	9350	
K13-9	0°	350	176.7	19.79	176.3	0.36	8650	
K13-16	0°	350	143.9	21.27	143.9	0.41	6500	
Avg.			171.3	19.89	166.7	0.31	8390	
Std.Dev.			22.5	0.82	20.7	0.08	1210	

Test: Tension		Material: G-160/6535-1						
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
K14-2	90°	-67	5.15	2.41	2.04	---	2260	
K15-3	90°	-67	5.36	2.61	1.47	---	2190	
K16-3	90°	-67	4.39	2.25	1.20	---	1980	
K17-3	90°	-67	4.30	2.31	1.60	---	1890	
K18-3	90°	-67	5.43	1.76	1.78	---	3160	
Avg.			4.93	2.27	1.58	---	2290	
Std.Dev.			0.54	0.31	0.35	---	500	
K45-1	90°	72	6.15	1.52	6.15	---	3940	
K15-1	90°	72	5.36	1.69	5.36	---	3090	
K16-1	90°	72	5.33	2.11	5.33	---	3090	
K17-1	90°	72	5.19	1.69	5.19	---	3040	
Avg.			5.51	1.82	5.51	---	3290	
Std.Dev.			0.43	0.27	0.43	---	440	
K15-4	90°	260	3.09	1.73	0.81	---	1820	
K16-4	90°	260	4.28	1.78	0.94	---	2600	
K17-4	90°	260	4.43	1.70	4.43	---	2610	
K18-4	90°	260	3.72	1.33	3.72	---	2690	
K45-3	90°	260	3.90	1.39	3.90	---	2710	
Avg.			3.88	1.59	2.70	---	2490	
Std.Dev.			0.53	0.21	1.74	---	380	
K15-2	90°	350	2.42	1.72	1.97	---	1360	
K16-2	90°	350	3.27	1.61	3.27	---	2035	
K17-2	90°	350	3.86	1.61	1.89	---	2510	
K45-2	90°	350	4.41	1.53	2.57	---	3200	
Avg.			3.49	1.63	2.42	---	2270	
Std.Dev.			0.85	0.11	0.64	---	780	

Test: Tension			Material: G-16C/6535-1					
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (ksi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ultimate Strain (in/in)	Remarks
K4-4	±45	-67	18.72	3.20	10.70	0.55	6520	
K6-2	±45	-67	19.71	3.14	7.73	0.62	6950	
K7-4	±45	-67	20.88	3.13	7.50	0.63	9200	
K10-3	±45	-67	16.88	3.28	9.64	0.62	5650	
K11-1	±45	-67	18.95	3.63	12.11	0.66	6120	
Avg.			19.43	3.28	9.53	0.62	6890	
Std.Dev.			0.90	0.21	1.96	0.04	1380	
K5-1	±45	72	17.70	3.15	8.40	0.68	7600	
K6-1	±45	72	16.36	3.29	4.96	0.73	6400	
K7-1	±45	72	15.36	3.13	5.46	0.60	6200	
K8-1	±45	72	17.77	2.99	5.26	0.66	8100	
K9-1	±45	72	15.45	3.02	5.54	0.60	6400	
Avg.			16.53	3.12	5.92	0.65	6940	
Std.Dev.			1.17	0.12	1.41	0.05	850	
K4-2	±45	260	17	2.85	4.48	0.73	12200	
K5-2	±45	260	15.71	3.09	3.58	0.61	12800	
K7-2	±45	260	15.91	3.06	4.76	0.72	13700	
K9-2	±45	260	15.75	3.13	4.63	0.79	10700	
K10-1	±45	260	14.88	3.11	5.60	0.75	8200	
Avg.			15.56	3.05	4.61	0.72	11520	
Std.Dev.			0.41	0.12	0.72	0.07	2150	
K4-3	±45	350	15.52	2.70	3.79	0.72	26200	
K5-3	±45	350	17.48	2.81	4.15	0.68	18000+	gage failed
K7-3	±45	350	17.32	2.91	4.46	0.70	6000+	gage failed
K9-3	±45	350	17.01	2.81	4.01	0.75	43400	
K10-2	±45	350	15.08	2.73	3.82	0.75	7200+	gage failed
Avg.			16.48	2.79	4.05	0.72	34800	excludes K5-3, K7-3, K10-2
Std.Dev.			1.10	0.08	0.28	0.03		

APPENDIX E
COMPRESSION DATA

All of the compression data generated during this program are presented in this section. They are summarized in tabular and graphical form in Sections 4.1 through 4.6.

Test: Compression				Material: T300/AFR800			
Spec. No.	Fiber Orlen.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
F35-12	0°	-67	224.8	17.93	84.8	25,000	
F35-13	0°	-67	208.3	19.91	69.4	22,500	
F35-14	0°	-67	190.0	17.80	48.0	14,500	
F35-19	0°	-67	218.2	22.67	54.0	11,500	
F36-2	0°	-67	186.4	17.43	74.1	18,000	
Avg.			205.6	19.15	66.1	18,300	
Std.Dev.			17.0	2.19	15.0	5,600	
F35-4	0°	72	145.6	19.77	19.8	9,600	
F35-5	0°	72	189.3	17.52	19.8	11,800	
F35-7	0°	72	192.9	12.21	33.3	20,800	
F35-9	0°	72	159.8	15.26	112.3	13,000	
F35-11	0°	72	185.6	15.14	38.6	18,500	
Avg.			174.6	15.98	44.6	14,700	
Std.Dev.			23.0	2.85	38.7	4,700	
F35-6	0°	260	149.5	16.97	59.4	11,300	
F35-8	0°	260	194.1	15.40	119.1	16,300	
F36-1	0°	260	220.5	22.90	48.7	13,700	
F36-3	0°	260	167.6	15.99	102.7	15,800	
F36-4	0°	260	202.5	20.64	47.0	15,000	
Avg.			188.2	18.38	75.4	14,400	
Std.Dev.			29.4	3.24	33.3	2,000	
F35-1	0°	350	163.7	17.11	63.9	9,800	
F35-10	0°	350	206.3	23.86	56.8	9,800	
F35-15	0°	350	157.4	19.53	41.5	7,300	
F35-16	0°	350	130.4	22.58	31.1	6,700	
F36-11	0°	350	163.3	20.45	163.3	8,100	
Avg.			164.2	20.71	71.3	8,300	
Std.Dev.			27.2	2.64	53.0	1,400	

Test: Compression				Material: T300/AFR800			
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
F35-3	90°	-67	29.5	1.87	10.1	39,800	
F35-5	90°	-67	40.5	1.78	12.6	28,800	
F35-15	90°	-67	42.3	1.41	25.6	37,300	
F35-23	90°	-67	55.3	1.49	11.1	26,800	
F36-9	90°	-67	23.9	1.96	9.0	25,000	
Avg.			38.4	1.70	13.7	31,500	
Std.Dev.			12.4	0.24	6.8	6,600	
F36-6	90°	72	39.1	2.91	39.1	14,800	
F36-8	90°	72	40.8	2.22	40.8	13,500+	Evidence of buckling
F36-14	90°	72	40.3	2.58	6.0	31,000	
F36-18	90°	72	45.7	2.44	45.1	21,000	
F36-23	90°	72	32.4	2.30	32.5	9,100+	Evidence of buckling
Avg.			39.7	2.50	32.8	17,900+	
Std.Dev.			4.8	0.27	15.7	9,000	
F35-15	90°	260	29.9	1.40	29.9	9,800	
F35-21	90°	260	26.7	1.57	23.9	9,800+	Evidence of buckling
F35-27	90°	260	29.2	1.40	1.9	20,000	
F36-2	90°	260	27.0	1.55	10.4	13,700	
F36-15	90°	260	29.2	1.58	29.2	10,000+	Evidence of buckling
Avg.			28.4	1.50	18.9	12,700+	
Std.Dev.			1.5	0.09	12.4	4,400	
F35-1	90°	350	25.1	1.44	9.8	34,300	
F35-11	90°	350	27.5	1.91	27.5	13,800	
F35-24	90°	350	23.0	1.56	11.0	33,300	
F35-30	90°	350	32.7	2.77	32.7	21,800	
F36-14	90°	350	30.4	2.42	30.4	35,300	
Avg.			27.7	2.02	22.3	25,800	
Std.Dev.			3.9	0.57	11.0	9,800	

Test: Compression				Material: SiC/5506			
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
G42-1	0°	-67	400.1	33.06	275.6	9,300+	Evidence of buckling
G42-7	0°	-67	396.3	33.06	295.3	15,700	
G42-11	0°	-67	434.9	33.04	184.4	16,900	
G42-17	0°	-67	387.8	28.96	305.0	15,400	
G42-19	0°	-67	334.7	37.29	160.3	7,300+	Evidence of buckling
Avg.			390.8	33.08	244.1	12,920+	
Std.Dev.			36.1	2.95	66.9	4,310	
G42-2	0°	72	338.0	32.01	81.6	5,400+	Tab debonded. Retabbed with
G42-4	0°	72	350.0	34.94	82.5	4,500+	different adhesive and tests
G42-6	0°	72	305.4	39.77	--	6,250+	rerun.
G42-8	0°	72	322.4	34.58	--	5,930+	↓
G42-10	0°	72	332.7	36.28	177.3	9,100+	
Avg.			329.7	35.52	113.8	6,220+	
Std.Dev.			16.8	2.84	55.0	1,730	
G42-12	0°	260	228.8	34.17	102.8	7,200	
G42-14	0°	260	233.2	39.02	182.0	7,800	
G42-16	0°	260	220.6	30.74	164.8	8,800	
G42-18	0°	260	240.3	31.79	124.6	6,200	
G42-20	0°	260	239.1	33.53	131.4	8,800	
Avg.			232.4	33.86	141.1	7,760	
Std.Dev.			8.1	3.22	31.9	1,110	
G42-3	0°	350	153.3	34.18	82.5	3,800+	Evidence of buckling
G42-5	0°	350	97.3	27.38	91.3	3,700	
G42-9	0°	350	102.5	27.43	100.8	3,700	
G42-13	0°	350	146.9	46.96	106.1	3,050+	Evidence of buckling
G42-15	0°	350	154.3	33.81	95.1	3,530	
Avg.			130.9	33.95	95.2	3,560+	
Std.Dev.			28.5	7.98	9.0	300	

Test: Compression				Material: SIC/5506			Remarks
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	
G42-15	90°	-67	56.6	3.97	11.0	19,200	
G42-26	90°	-67	57.7	4.34	13.4	18,100	
G42-36	90°	-67	53.4	3.84	14.4	24,100	
G42-46	90°	-67	53.7	2.97	11.0	25,700	
G42-52	90°	-67	62.3	1.93	27.9	23,900	
Avg.			56.7	3.41	15.5	22,200	
Std.Dev.			3.6	0.97	7.1	3,340	
G42-1	90°	72	34.1	4.38	8.7	4,100+	evidence of buckling
G42-14	90°	72	31.8	3.30	11.6	7,000+	evidence of buckling
G42-27	90°	72	35.5	3.03	30.5	12,000	
G42-32	90°	72	34.4	4.05	15.1	6,900+	evidence of buckling
G42-45	90°	72	36.3	3.13	24.2	16,200	
Avg.			34.4	3.58	18.0	9,240+	
Std.Dev.			1.7	0.60	9.1	4,820	
G42-7	90°	260	26.9	2.54	14.0	16,700+	evidence of buckling
G42-17	90°	260	26.7	2.41	16.9	24,200	
G42-18	90°	260	23.0	2.39	10.6	23,400	
G42-21	90°	260	25.9	2.22	11.9	21,700	
G42-35	90°	260	25.7	2.44	17.9	16,700+	evidence of buckling
Avg.			25.7	2.40	14.3	20,540+	
Std.Dev.			1.5	0.12	3.2	3,620	
G42-6	90°	350	21.6	1.87	9.8	24,800	
G42-10	90°	350	18.7	1.83	7.4	31,200	
G42-25	90°	350	20.4	1.43	10.5	24,700	
G42-35	90°	350	18.8	1.94	12.4	6,600+	evidence of buckling
G42-37	90°	350	19.3	2.34	7.0	27,700	
Avg.			19.8	1.88	9.4	27,100*	*excludes G42-35
Std.Dev.			1.2	0.32	2.2	3,070*	

Test: Compression				Material: HVE 2034D			
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
H29-2	0°	-67	61.24	42.29	28.45	2000	
H29-8	0°	-67	53.27	38.57	39.14	1400	
H29-13	0°	-67	56.64	37.19	44.34	1700	
H29-17	0°	-67	52.02	33.96	34.88	1900	
H29-22	0°	-67	45.87	33.12	31.47	1700	
Avg.			53.81	37.03	35.66	1740	
Std.Dev.			5.69	3.70	6.28	230	
H29-12	0°	72	41.91	39.91	39.81	1100	
H29-16	0°	72	47.41	37.64	38.09	1500	
H30-1	0°	72	44.60	64.00	14.40	1000	
H30-5	0°	72	53.08	41.15	12.55	1700	
H30-8	0°	72	55.56	46.78	24.00	1200	
Avg.			48.51	45.90	25.77	1300	
Std.Dev.			5.71	10.67	12.81	290	
H29-4	0°	260	31.16	54.53	13.90	1100	
H29-9	0°	260	43.60	46.84	14.34	1200	
H30-2	0°	260	48.00	46.65	19.18	1200	
H30-7	0°	260	46.32	38.92	32.65	1400	
H30-11	0°	260	40.93	34.49	33.68	1700	
Avg.			42.00	44.29	22.75	1320	
Std.Dev.			6.63	7.77	9.73	240	
H29-1	0°	350	48.53	55.78	20.08	1200	*H29-11 broke at end, just inside gripping tabs. All others broke in center of gage section.
H29-7	0°	350	42.99	46.18	29.90	1100	
H29-11	0°	350	8.73*	40.40	8.49*	200*	
H29-14	0°	350	32.21	41.90	16.98	1200	
H29-20	0°	350	44.38	32.86	34.14	1200	
Avg.			42.03**	43.42	25.28**	1180**	**excludes H29-11
Std.Dev.			6.96	8.42	8.08	50	

Test: Compression				Material: HVE 2034D			
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
H29-6	90°	-67	15.12	1.00	5.48	18500	
H29-11	90°	-67	20.41	1.23	15.59	18800	
H29-10	90°	-67	20.88	2.18	2.30	21100	
H30-2	90°	-67	19.92	2.65	3.67	21500	
H29-2	90°	-67	---	---	---	---	Broke in mounting
Avg.			19.08	1.76	5.76	19980	
Std.Dev.			2.67	0.78	6.03	1540	
H29-19	90°	72	16.00	1.77	1.53	30100	
H29-23	90°	72	3.35	---	2.33	3200	Probable damage before testing
H30-3	90°	72	15.07	1.36	2.22	53500	
H30-7	90°	72	16.73	1.48	2.15	34400	
H30-9	90°	72	22.38	1.88	6.80	25800	
Avg.			17.55	1.62	3.17	35950	Averages exclude H29-23
Std.Dev.			3.30	0.24	2.44	12220	
H30-14	90°	260	12.58	0.78	1.56	14700	
H30-19	90°	260	12.17	1.40	12.17	8000	
H29-20	90°	260	12.08	1.07	12.08	12300	
H29-25	90°	260	14.69	1.45	2.04	15900	
H29-34	90°	260	13.72	1.47	5.02	18500	
Avg.			13.05	1.24	6.58	13880	
Std.Dev.			1.13	0.30	5.22	3970	
H29-22	90°	350	12.50	0.90	4.56	22700	
H29-29	90°	350	11.50	0.92	2.11	19400	
H29-16	90°	350	8.75	1.09	1.86	21900	
H29-28	90°	350	12.25	0.76	1.44	31400	
H29-7	90°	350	12.43	0.95	0.99	29800	
Avg.			11.49	0.92	2.19	25040	
Std.Dev.			1.58	0.12	1.39	5250	

Test: Compression					Material: T300/V378A		
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop. Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
I41-2	0°	-67	220.4	18.15	64.7	20,500	
I41-4	0°	-67	238.1	19.96	48.2	8,700+	evidence of buckling
I41-9	0°	-67	213.2	19.83	25.0	9,500+	evidence of buckling
I41-16	0°	-67	189.7	17.85	51.3	17,100	
I41-23	0°	-67	205.7	21.99	37.1	8,900+	evidence of buckling
Avg.			213.4	19.56	45.3	12,940	
Std. Dev.			17.9	1.66	15.0	5,490	
I41-7	0°	72	193.2	19.49	44.8	17,000	
I41-13	0°	72	168.5	20.95	53.6	16,300	
I41-22	0°	72	212.8	19.83	212.8	11,000+	evidence of buckling
I41-27	0°	72	190.6	19.25	190.6	16,600	
I41-60	0°	72	198.2	19.35	198.2	19,700	
Avg.			192.7	19.78	140.0	16,120+	
Std. Dev.			16.0	0.60	83.3	3,170	
I41-3	0°	350	169.7	24.00	169.7	6,400	
I41-11	0°	350	162.4	21.21	162.4	5,900	
I41-15	0°	350	146.9	23.91	146.9	6,200	
I41-20	0°	350	195.0	23.09	71.1	12,000	
I41-25	0°	350	135.8	24.75	66.5	10,100	
Avg.			162.1	23.39	123.3	8,120	
Std. Dev.			22.4	1.35	50.5	2,760	
I41-6	0°	450	145.9	20.03	145.9	7,800	
I41-8	0°	450	79.4	21.35	70.9	4,100	
I41-12	0°	450	87.2	17.28	87.2	5,000	
I41-18	0°	450	100.4	23.00	100.4	4,600	
I41-24	0°	450	90.3	22.49	23.2	4,180	
Avg.			100.6	20.83	85.5	5,140	
Std. Dev.			26.4	2.29	44.6	1,530	

Test: Compression				Material: T300/V378A			Remarks
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	
I42-20	90°	-67	54.7	3.83	10.1	23,600	
I42-24	90°	-67	32.4	1.52	32.4	25,000	
I42-28	90°	-67	45.2	3.27	3.2	27,500	
I42-32	90°	-67	28.2	1.65	28.2	29,500	
I42-36	90°	-67	28.9	2.26	6.8	11,500 +	evidence of buckling
Avg.			37.9	2.51	16.1	23,360 +	
Std.Dev.			11.6	1.01	13.2	7,170	
I42-2	90°	72	24.6	2.54	4.5	25,200	evidence of buckling or gage fail
I42-6	90°	72	28.2	3.86	6.5	23,200	
I42-10	90°	72	28.5	3.09	4.2	23,100	
I42-14	90°	72	24.4	1.97	4.9	12,800	
I42-18	90°	72	28.1	1.71	9.7	34,800	
Avg.			26.8	2.53	5.9	23,820	
Std.Dev.			2.1	0.87	2.3	7,820	
I42-40	90°	350	17.8	1.41	6.7	15,500 +	evidence of buckling
I42-44	90°	350	18.8	1.61	4.2	13,500	
I42-48	90°	350	20.2	1.95	4.4	6,800 +	evidence of buckling & gage failure
I42-52	90°	350	21.8	1.59	3.9	18,100 +	evidence of buckling
I42-56	90°	350	16.3	1.25	7.0	15,200	
Avg.			19.0	1.56	5.2	13,820 +	
Std.Dev.			2.1	0.26	1.5	4,260	
I42-8	90°	450	25.5	1.30	3.1	29,800	
I42-12	90°	450	21.0	1.19	5.8	42,500	
I42-13	90°	450	17.6	1.19	3.7	17,900	
I42-16	90°	450	18.3	1.07	18.3	7,290 +	evidence of buckling
I42-17	90°	450	18.7	1.26	3.1	29,800	
Avg.			20.2	1.20	6.8	18,880 +	
Std.Dev.			3.2	0.09	6.5	16,870	

Test: Compression				Material: HYE 1076J			
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop. Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
J32-4	0°	-67	210.8	18.79	66.1	9900+	evidence of buckling
J32-8	0°	-67	253.5	21.41	69.3	13100+	evidence of buckling
J32-13	0°	-67	195.7	19.34	83.0	20000	
J32-15	0°	-67	225.0	20.33	70.8	18500	
J32-21	0°	-67	231.9	29.57	30.0	10800+	evidence of buckling
Avg.			223.4	21.89	63.8	14500+	
Std.Dev.			21.8	4.41	20.0	4600	
J32-2	0°	72	161.9	17.30	67.5	19600	
J32-7	0°	72	248.1	21.87	173.2	11200+	evidence of buckling
J32-12	0°	72	221.9	21.83	62.2	10600	
J32-18	0°	72	245.0	22.31	245.0	11800+	evidence of buckling
J32-25	0°	72	214.2	25.46	35.7	9500	
Avg.			218.2	21.75	116.7	12500+	
Std.Dev.			34.7	2.91	88.9	4000	
J32-1	0°	260	111.1	12.55	111.1	6300+	evidence of buckling
J32-6	0°	260	205.2	23.67	64.4	8000+	evidence of buckling
J32-11	0°	260	193.7	25.52	46.3	10600	
J32-17	0°	260	161.6	26.23	31.5	6800	
J32-23	0°	260	182.9	19.13	61.0	12600	
Avg.			170.9	21.42	62.9	8900+	
Std.Dev.			37.1	5.68	30.0	2700	
J32-3	0°	350	167.7	19.12	68.8	14000	
J32-10	0°	350	124.2	26.71	52.8	5000	
J32-16	0°	350	185.6	21.15	63.9	12000	
J32-20	0°	350	184.2	25.09	115.9	9500	
J32-27	0°	350	130.8	22.54	130.8	6500	
Avg.			158.5	22.92	86.4	9400	
Std.Dev.			29.3	3.03	34.6	3700	

Test: Compression				Material: HYE 1076J			
Spec. No.	Fiber Orient.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
J31-5	90°	-67	35.5	2.12	7.8	13000	
J31-18	90°	-67	32.3	2.18	13.2	25900	
J31-22	90°	-67	44.9	1.46	7.5	27400	
J31-33	90°	-67	36.0	1.85	15.0	16400+	evidence of buckling
J31-49	90°	-67	26.7	1.61	6.0	27700	
Avg.			35.1	1.84	9.9	22100+	
Std.Dev.			6.6	0.31	3.9	6400	
J31-19	90°	72	31.9	1.73	9.3	35300	
J31-29	90°	72	30.8	1.42	12.6	46300	
J31-34	90°	72	29.0	1.36	9.5	37600	
J31-43	90°	72	26.7	1.48	2.4	7900+	evidence of buckling
J31-51	90°	72	31.4	1.32	12.7	34400	
Avg.			30.8	1.46	11.0	32300+	
Std.Dev.			1.3	0.16	1.9	14400	
J31-9	90°	260	24.1	1.52	3.8	13800	
J31-21	90°	260	25.7	3.03	4.0	---	gage failed
J31-31	90°	260	21.5	1.59	4.5	---	gage failed
J31-46	90°	260	22.3	1.37	4.0	21400	
J31-55	90°	260	19.4	1.69	6.3	9600+	evidence of buckling
Avg.			22.6	1.84	4.5	17600*	*excludes J31-55
Std.Dev.			2.4	0.68	1.0	---	
J31-2	90°	350	22.8	1.65	7.4	21300	
J31-15	90°	350	19.4	1.88	3.7	7700+	evidence of buckling
J31-23	90°	350	17.4	2.02	3.2	6900+	evidence of buckling
J31-39	90°	350	18.7	1.40	11.8	20000	
J31-50	90°	350	17.3	1.25	9.4	15300+	evidence of buckling
Avg.			19.1	1.64	7.1	14200+	
Std.Dev.			2.2	0.32	3.7	6700	

Test: Compression					Material: G-160/6535-1				
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks		
K21-3	0°	-67	230.8	19.26	63.95	11,850			
K21-7	0°	-67	192.4	22.02	72.55	8,400			
K21-13	0°	-67	235.4	21.13	69.86	10,100+	Evidence of buckling		
K21-18	0°	-67	198.0	20.16	86.96	6,400+	Evidence of buckling		
K21-23	0°	-67	213.6	20.14	76.10	10,850+	Evidence of buckling		
Avg.			214.0	20.54	73.88	9,520+			
Std.Dev.			19.1	1.06	8.55	2,200			
K21-2	0°	72	209.6	17.09	88.5	14,200			
K21-8	0°	72	216.7	20.83	156.6	15,500			
K21-12	0°	72	207.2	19.51	122.4	8,600+	Evidence of buckling		
K21-17	0°	72	204.0	19.28	90.0	19,000			
K21-22	0°	72	223.9	19.32	73.9	16,700			
Avg.			212.3	19.21	106.3	14,800+			
Std.Dev.			8.0	1.34	33.2	3,890			
K21-1	0°	260	192.3	18.76	---	9,100+	Evidence of buckling		
K21-6	0°	260	206.3	19.84	75.0	12,100			
K21-11	0°	260	184.8	19.16	95.8	13,700			
K21-16	0°	260	204.3	19.76	---	9,800+	Evidence of buckling		
K21-21	0°	260	156.5	16.10	71.7	10,600			
Avg.			188.8	18.73	80.9	11,060+			
Std.Dev.			20.1	1.53	13.1	1,850			
K21-4	0°	350	152.0	18.18	88.9	9,600			
K21-9	0°	350	163.0	23.13	132.8	8,500			
K21-14	0°	350	135.4	22.30	94.0	8,200			
K21-19	0°	350	145.8	23.90	75.5	7,000			
K21-24	0°	350	160.7	19.51	118.4	9,350			
Avg.			151.4	21.40	101.9	8,530			
Std.Dev.			11.3	2.45	23.2	1,030			

Test: Compression				Material: G-160/6535-1			
Spec. No.	Fiber Crlen.	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Initial Modulus (10 ⁶ psi)	Stress at Prop.Lim. (10 ³ psi)	Ultimate Strain (μ in/in)	Remarks
K19-3	90°	-67	32.7	1.88	9.8	32,600	
K19-25	90°	-67	39.3	2.06	18.8	22,800+	Evidence of buckling
K19-41	90°	-67	33.4	2.21	10.7	23,200	
K44-4	90°	-67	29.7	2.09	13.6	20,000+	Evidence of buckling
K44-27	90°	-67	45.5	1.81	17.3	30,050+	Evidence of buckling
Avg.			36.1	2.01	14.1	25,730+	
Std.Dev.			6.3	0.16	4.0	5,330	
K19-5	90°	72	30.2	1.57	15.5	25,800	
K19-27	90°	72	22.6	1.91	11.8	7,200+	Evidence of buckling
K19-45	90°	72	30.2	2.02	12.5	36,000	
K44-1	90°	72	27.0	2.64	12.1	8,600+	Evidence of buckling
K44-22	90°	72	25.0	---	14.0	32,200	
Avg.			27.0	2.04	13.2	21,960+	
Std.Dev.			3.3	0.45	1.5	13,350	
K19-1	90°	260	25.4	1.42	20.2	14,600+	Evidence of buckling
K19-11	90°	260	24.2	1.43	15.5	13,700+	Evidence of buckling
K19-40	90°	260	22.0	1.33	14.3	26,300	
K44-3	90°	260	23.7	1.29	12.9	12,800+	Evidence of buckling
K44-25	90°	260	24.5	1.56	16.5	10,900+	Evidence of buckling
Avg.			24.0	1.40	15.9	15,660+	
Std.Dev.			1.3	0.10	2.8	6,100	
K19-4	90°	350	19.8	1.87	11.9	17,000+	Evidence of buckling
K19-26	90°	350	26.3	2.12	10.4	14,800	
K19-42	90°	350	19.0	2.19	14.3	7,000+	Evidence of buckling
K44-2	90°	350	16.6	1.63	10.7	7,230+	Evidence of buckling
K44-23	90°	350	17.1	1.21	9.6	12,700+	Evidence of buckling
Avg.			19.8	1.80	11.4	11,750+	
Std.Dev.			3.9	0.40	1.9	4,490	

APPENDIX F

FLEXURE DATA

All of the flexure data generated during this program are listed in this appendix. Summaries of these data are tabulated in Sections 4.1 through 4.6.

Test: Flexure					L/D Ratio: 32:1
Materials: T300/APR300					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
F19-5	0°	-67	299.7	21.24	4 pt./tensile failure
F19-8	0°	-67	291.5	20.59	on lower surface
F19-12	0°	-67	295.9	19.77	
F19-15	0°	-67	292.6	20.73	
F20-3	0°	-67	278.1	18.24	↓
Avg.			291.6	20.11	
Std. Dev.			8.2	1.17	
F19-2	0°	72	282.0	21.68	4 pt./tensile failure
F19-7	0°	72	280.2	20.69	on lower surface
F19-17	0°	72	272.9	20.56	
F19-20	0°	72	284.9	20.94	
F20-6	0°	72	280.7	19.63	↓
Avg.			280.1	20.70	
Std. Dev.			4.4	0.74	
F19-0	0°	260	182.4	15.23	3 pt./specimens
F19-10	0°	260	225.8	17.18	snapped in half
F19-22	0°	260	202.5	16.11	
F20-1	0°	260	248.6	19.18	↓
Avg.			214.8	16.92	
Std. Dev.			28.7	1.70	
F19-14	0°	260	206.5	20.22	4 pt./delamination
F19-16	0°	260	206.8	21.06	failures
F19-19	0°	260	230.0	20.99	
F19-23	0°	260	224.8	21.27	
F19-24	0°	260	223.1	20.57	↓
Avg.			218.2	20.82	Shear stress at
Std. Dev.			10.9	0.42	failure = 6890 psi

[illegible]

Test: Flexure			L/D Ratio: 32:1		
Materials: T300/AFR800					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (Ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
F19-4	90°	-67	13.98	---	4 pt. loading
F20-5	90°	-67	17.71	1.70	
F20-15	90°	-67	13.02	1.73	
F20-19	90°	-67	15.03	1.59	
F20-26	90°	-67	14.76	1.64	
Avg.			14.90	1.67	
Std.Dev.			1.75	0.06	
F19-2	90°	72	14.43	1.34	4 pt. loading
F20-4	90°	72	14.15	1.24	
F20-12	90°	72	13.57	1.25	
F20-20	90°	72	13.95	1.26	
F20-24	90°	72	14.42	1.24	
Avg.			14.10	1.27	
Std.Dev.			0.36	0.04	
F19-5	90°	260	10.42	1.09	4 pt. loading
F20-8	90°	260	10.83	1.14	
F20-13	90°	260	10.21	1.18	
F20-17	90°	260	11.21	1.26	
F20-23	90°	260	10.70	1.18	
Avg.			10.68	1.17	
Std. Dev.			0.44	0.07	
F19-1	90°	350	11.12	1.09	4 pt. loading
F19-6	90°	350	9.68	1.02	
F20-10	90°	350	11.75	1.22	
F20-18	90°	350	12.80	1.16	
F20-25	90°	250	10.68	1.17	
Avg.			11.21	1.13	
Std. Dev.			1.31	0.08	

Test: Flexure				L/D Ratio: 32:1	
Materials: SIC/5506					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
G20-5	0°	-67	318.7	31.42	4 pt./tensile failure
G20-11	0°	-67	317.9	32.41	on lower surface
G20-16	0°	-67	333.3	31.42	↓
G20-20	0°	-67	318.7	32.42	
G20-24	0°	-67	324.7	31.72	
G20-28	0°	-67	336.4	33.14	
Avg.			324.9	31.92	
Std. Dev.			8.1	0.71	
G20-4	0°	72	316.3	32.04	4 pt./tensile failure
G20-8	0°	72	298.0	31.29	on lower surface
G20-17	0°	72	324.1	32.98	↓
G20-22	0°	72	313.5	31.35	
G20-23	0°	72	320.8	32.42	
Avg.			314.6	31.82	
Std. Dev.			10.1	0.48	
G20-7	0°	260	187.6	30.00	4 pt./shear failure
G20-14	0°	260	166.1	28.44	↓
G20-19	0°	260	171.4	29.61	
G20-21	0°	260	204.1	29.00	
G20-27	0°	260	217.2	30.89	
Avg.			189.3	29.59	Shear stress at
Std. Dev.			21.6	0.94	failure = 5900 psi

Test: Flexure			L/D Ratio: 32:1		
Materials: SIC/5506					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
G20-2	0°	350	109.9	32.22	4 pt/shear failure
F20-10	0°	350	118.0	29.11	
F20-13	0°	350	121.5	31.23	
F20-18	0°	350	124.7	31.42	
F20-26	0°	350	126.2	27.83	
Avg.			120.0	30.36	Shear stress at
Std.Dev.			6.5	1.82	failure = 3750 psi
G37-1	0°	260	322.6	28.87	3 pt/tensile failure
G37-3	0°	260	308.7	28.67	on lower surface
G37-5	0°	260	322.9	30.23	
G37-7	0°	260	312.4	28.07	
Avg.			316.7	28.96	
Std. Dev.			7.2	0.91	
G37-2	0°	350	170.1	24.00	3 pt/shear failure
G37-4	0°	350	182.9	25.70	
G37-6	0°	350	173.8	24.04	
G37-8	0°	350	175.2	24.56	
Avg.			175.5	24.58	Shear stress at
Std.Dev.			5.4	0.79	failure = 2770 psi
G21-3	90°	-67	17.3	2.85	4 pt. loading
G21-9	90°	-67	17.3	2.62	
G21-14	90°	-67	14.9	2.58	
G21-23	90°	-67	14.6	2.95	
G21-29	90°	-67	15.2	2.54	
Avg.			15.9	2.71	
Std.Dev.			1.3	0.18	

Test: Flexure			L/D Ratio: 32:1		
Materials: SIC/5506					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
G21-1	90°	72	14.9	2.52	4 pt. loading
G21-5	90°	72	15.5	2.44	
G21-10	90°	72	13.5	2.31	
G21-15	90°	72	15.0	2.23	
G21-20	90°	72	14.3	2.17	
G21-25	90°	72	13.9	2.39	
Avg.			14.5	2.34	
Std.Dev.			0.8	0.13	
G21-2	90°	260	10.0	1.18	4 pt. loading
G21-8	90°	260	10.3	1.57	
G21-16	90°	260	10.4	1.34	
G21-24	90°	260	11.6	1.50	
G21-28	90°	260	13.2	1.62	
Avg.			11.1	1.44	
Std.Dev.			1.4	0.18	
G21-4	90°	350	6.7	0.86	4 pt. loading
G21-6	90°	350	6.9	0.85	
G21-12	90°	350	7.7	0.89	
G21-21	90°	350	7.4	0.84	
G21-27	90°	350	6.1	0.82	
Avg.			7.0	0.85	
Std.Dev.			0.6	0.03	
G37-1	90°	350	8.2	0.93	3 pt. loading
G37-2	90°	350	11.3	1.13	
G37-3	90°	350	8.9	0.96	
G37-4	90°	350	11.1	1.12	
Avg.			9.9	1.03	
Std.Dev.			1.6	0.11	

Test: Flexure					L/D Ratio: 32:1
Materials: HyE 2034D					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
H8-5	0°	-67	96.1	37.92	4 pt. loading
H8-16	0°	-67	107.1	42.31	
H8-19	0°	-67	62.2	23.14	
H8-26	0°	-67	87.1	44.66	
H8-3	0°	-67	103.8	43.71	
H8-15	0°	-67	77.0	20.18	
Avg.			88.9	35.32	
Std.Dev.			17.1	10.87	
H8-10	0°	72	91.9	39.37	4 pt. loading
H8-13	0°	72	89.7	41.07	
H8-17	0°	72	91.9	41.62	
H8-21	0°	72	87.4	41.84	
H8-24	0°	72	90.2	43.87	
Avg.			90.2	41.55	
Std.Dev.			1.9	1.62	
H8-14	0°	260	65.9	41.40	4 pt. loading
H8-18	0°	260	68.7	41.80	
H8-20	0°	260	62.8	20.70	
H8-22	0°	260	69.0	44.01	
H8-23	0°	260	66.7	39.60	
Avg.			66.6	37.50	
Std.Dev.			2.5	9.52	
H8-4	0°	350	63.3	37.49	4 pt. loading
H8-6	0°	350	64.5	45.36	
H8-11	0°	350	66.7	39.16	
H8-12	0°	350	70.0	40.81	
H8-25	0°	350	69.9	39.47	
Avg.			66.9	40.46	
Std.Dev.			3.0	2.98	

Test: Flexure			L/D Ratio: 32:1		
Materials: HyE 2034D					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
H9-1	90°	-67	5.54	1.04	4 pt. loading
H9-9	90°	-67	5.75	1.08	
H9-19	90°	-67	5.54	1.13	
H9-22	90°	-67	5.28	1.04	
H9-24	90°	-67	5.75	1.04	
Avg.			5.57	1.07	
Std. Dev.			0.19	0.04	
H9-3	90°	72	5.72	1.00	4 pt. loading
H9-6	90°	72	5.08	1.17	
H9-15	90°	72	5.57	1.08	
H9-16	90°	72	4.80	1.08	
H9-20	90°	72	5.31	1.12	
Avg.			5.30	1.09	
Std. Dev.			0.37	0.06	
H9-4	90°	260	3.78	0.91	4 pt. loading
H9-5	90°	260	3.78	0.87	
H9-8	90°	260	3.65	0.86	
H9-10	90°	260	3.38	0.91	
H9-11	90°	260	3.78	0.95	
Avg.			3.67	0.90	
Std. Dev.			0.17	0.04	
H9-12	90°	350	2.72	0.75	4 pt. loading
H9-7	90°	350	2.93	0.76	
H9-13	90°	350	2.65	0.80	
H9-14	90°	350	2.51	0.80	
H9-17	90°	350	3.20	0.76	
Avg.			2.80	0.77	
Std. Dev.			0.27	0.02	

Test: Flexure			L/D Ratio: 32:1		
Materials: T300/V378A					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
I1-6	0°	-67	289.4	17.08	3 pt/tensile failure
I1-13	0°	-67	276.3	16.13	on lower surface
I1-15	0°	-67	262.1	15.50	↓
I1-24	0°	-67	277.4	15.94	
I1-26	0°	-67	248.4	15.38	
Avg.			270.7	16.01	
Std.Dev.			15.8	0.67	
I1-5	0°	72	224.4	16.94	4 pt/mixed failure
I1-7	0°	72	232.3	15.81	modes. Some delamination; some tension on
I1-10	0°	72	220.1	19.19	lower surface; some
I1-17	0°	72	219.5	16.94	comp. under upper loading
I1-23	0°	72	226.3	16.94	
Avg.			224.6	17.16	Shear stress at failure = 7010 psi.
Std.Dev.			5.2	1.24	
I1-4	0°	350	166.6	16.89	4 pt/delamination failure
I1-11	0°	350	156.5	15.66	↓
Avg.			161.6	16.28	
					Shear stress at failure = 5040 psi
I1-16	0°	350	163.4	15.36	3 pt/mixed failure
I1-19	0°	350	175.4	16.32	modes. Some tension
I1-22	0°	350	172.8	15.18	on lower surface; some
Avg.			170.5	15.62	compression on upper
Std.Dev.			6.3	0.61	surface.

L/D Ratio: 32:1

Materials: T300/V378A

3 pt.

Test: Flexure					L/D Ratio: 32:1	
Materials: T300/V378A						
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks	
I2-2	90°	-67	10.40	1.81	4 pt. loading	
I2-6	90°	-67	9.40	1.77		
I2-14	90°	-67	12.22	1.94		
I2-20	90°	-67	9.51	1.68		
I2-24	90°	-67	14.38	1.91		↓
Avg.			11.18	1.82		
Std.Dev.			2.12	0.11		
I2-1	90°	72	10.88	1.79	4 pt. loading	
I2-7	90°	72	12.35	1.79		
I2-11	90°	72	12.14	1.74		
I2-18	90°	72	10.33	1.69		
I2-26	90°	72	12.20	1.68		↓
Avg.			11.58	1.74		
Std.Dev.			0.91	0.05		
I2-3	90°	350	6.92	1.37	4 pt. loading	
I2-8	90°	350	7.45	1.49		
I2-15	90°	350	8.68	1.50		
I2-21	90°	350	9.80	1.53		
I2-25	90°	350	9.13	1.47		↓
Avg.			8.39	1.47		
Std.Dev.			1.19	0.06		
I2-4	90°	450	8.00	1.24	4 pt. loading	
I2-12	90°	450	7.57	1.37		
I2-17	90°	450	8.52	1.28		
I2-19	90°	450	7.07	1.15		
I2-23	90°	450	8.03	1.38		↓
Avg.			7.84	1.29		
Std.Dev.			0.54	0.09		

Test: Flexure			L/D Ratio: 32:1		
Materials: HyE 1076J					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
J2-4	0°	-67	268.9	19.35	3 pt./tensile failure
J2-11	0°	-67	263.8	18.62	
J2-16	0°	-67	239.3	18.83	
J2-20	0°	-67	276.3	18.81	
J2-23	0°	-67	261.3	17.50	
Avg.			261.9	18.62	
Std. Dev.			13.9	0.68	
J2-2	0°	72	186.3	14.57	4 pt./tensile failure
J2-7	0°	72	189.7	13.84	
J2-9	0°	72	191.4	15.21	
J2-17	0°	72	187.5	15.37	
J2-22	0°	72	195.8	15.29	
Avg.			190.1	14.86	
Std. Dev.			3.6	0.65	
J2-5	0°	260	152.1	13.74	Note: primary failure
J2-8	0°	260	149.4	12.97	in compression(4 pt.)
J2-13	0°	260	148.1	12.02	
J2-18	0°	260	158.2	12.57	
J2-21	0°	260	176.2	13.97	tension failure/4 pt.
Avg.			156.8	13.05	
Std. Dev.			11.5	0.81	
J2-3	0°	350	145.7	17.08	shear failure/4 pt.
J2-10	0°	350	178.0	19.43	3 pt./compression fail
J2-12	0°	350	183.3	19.07	
J2-15	0°	350	185.0	17.49	
J2-25	0°	350	197.4	17.31	
Avg.			185.9	18.32	Avg. omits J2-3
Std. Dev.			8.2	1.08	

Test: Flexure			L/D Ratio: 32:1		
Materials: HyE 1076J					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (ksi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
J1-5	90°	-67	8.34	1.66	4 pt. loading
J1-10	90°	-67	9.21	1.58	
J1-15	90°	-67	11.78	1.98	
J1-19	90°	-67	10.48	2.01	
J1-25	90°	-67	11.73	1.98	
Avg.			10.31	1.84	
Std. Dev.			1.52	0.21	
J1-1	90°	72	8.58	1.64	4 pt. loading
J1-6	90°	72	7.38	1.57	
J1-12	90°	72	8.47	1.60	
J1-18	90°	72	10.66	1.91	
J1-24	90°	72	8.89	1.86	
Avg.			8.79	1.71	
Std. Dev.			1.19	0.16	
J1-4	90°	260	5.85	1.49	4 pt. loading
J1-8	90°	260	6.54	1.58	
J1-16	90°	260	7.04	1.72	
J1-20	90°	260	8.62	1.71	
J1-26	90°	260	9.06	1.60	
Avg.			7.42	1.62	
Std. Dev.			1.37	0.10	
J1-2	90°	350	6.53	1.35	4 pt. loading
J1-7	90°	350	6.31	1.40	
J1-14	90°	350	7.79	1.66	
J1-21	90°	350	8.66	1.58	
J1-23	90°	350	5.86	1.25	
Avg.			7.03	1.45	
Std. Dev.			1.16	0.17	

Test: Flexure			L/D Ratio: 32:1		
Materials: G-160/6535-1					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
K41-4	0°	-67	243.4	18.62	3 pt. loading/tens. fail.
K41-9	0°	-67	236.3	17.70	
K41-21	0°	-67	251.6	19.09	
K41-23	0°	-67	212.3	18.85	
K41-29	0°	-67	255.9	20.94	
Avg.			239.9	19.04	
Std. Dev.			17.2	1.19	
K41-1	0°	72	237.6	18.34	4 pt. loading/tens. & compr. failure
K41-5	0°	72	230.7	18.22	
K41-10	0°	72	235.9	18.33	
K41-20	0°	72	215.2	20.09	
K41-15	0°	72	237.0	17.48	
Avg.			231.3	18.49	
Std. Dev.			9.4	0.96	
K41-3	0°	260	199.5	19.06	4 pt. load/shear fail.
K41-7	0°	260	128.0	19.40	4 pt. load/shear fail.
K41-11	0°	260	214.2	18.49	3 pt. load/tens. & compr. failure
K41-16	0°	260	223.5	17.33	
K41-25	0°	260	221.5	18.19	
Avg.			219.7	18.00	omits K41-3 & K41-7
Std. Dev.			4.9	0.60	omits K41-3 & K41-7
K41-2	0°	350	186.5	16.21	3 pt. load/tens. & compr. failure
K41-6	0°	350	179.6	16.44	
K41-12	0°	350	177.5	17.46	
K41-18	0°	350	189.4	17.53	
K41-22	0°	350	175.8	16.62	
Avg.			181.7	16.95	
Std. Dev.			5.9	0.61	

Test: Flexure			L/D Ratio: 32:1		
Materials: G-160/6535-1					
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Modulus of Elasticity (10 ⁶ psi)	Remarks
K42-9	90°	-67	10.14	1.58	4 pt. load
K42-15	90°	-67	10.11	1.52	
K42-21	90°	-67	7.09	1.50	
K42-3	90°	-67	8.59	1.83	
K42-23	90°	-67	8.63	2.16	↓
Avg.			9.11	1.53	
Std. Dev.			1.75	0.04	
K42-1	90°	72	8.41	1.39	4 pt. load
K42-13	90°	72	9.29	1.46	
K42-25	90°	72	8.90	1.50	
K42-7	90°	72	8.73	1.46	
K42-18	90°	72	8.64	1.41	↓
Avg.			8.86	1.45	
Std. Dev.			0.44	0.06	
K42-8	90°	260	6.65	1.48	4 pt. load
K42-20	90°	260	6.67	1.47	
K42-26	90°	260	5.86	1.41	
K42-4	90°	260	7.78	1.42	
K42-14	90°	260	4.70	1.22	↓
Avg.			6.40	1.45	
Std. Dev.			0.47	0.04	
K42-2	90°	350	6.32	1.26	4 pt. load
K42-19	90°	350	6.75	1.49	
K42-24	90°	350	6.45	1.26	
K42-6	90°	350	7.15	1.44	
K42-12	90°	350	7.56	1.33	↓
Avg.			6.50	1.34	
Std. Dev.			0.22	0.13	

APPENDIX G

INPLANE SHEAR DATA

All of the inplane shear data generated during this program are presented in this section. These data are both tabularly and graphically summarized in Sections 4.1 through 4.6.

Test: Inplane Shear

Materials: T300/AFR800

Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Inplane Shear Modulus (10 ⁶ psi)	Ultimate Strain (in/in)	Remarks
F23-5	±45	-67	13,900	0.71		
F24-1	±45	-67	13,360	0.67		
F25-7	±45	-67	12,850	0.65		
F26-4	±45	-67	12,620	0.65		
F27-10	±45	-67	13,370	0.70		
Avg.			13,220	0.68		
Std.Dev.			500	0.03		
F23-9	±45	72	12,030	0.69		
F24-9	±45	72	11,900	0.72		
F25-5	±45	72	10,750	0.60		
F26-10	±45	72	11,850	0.66		
F27-1	±45	72	11,570	0.73		
Avg.			11,620	0.68		
Std.Dev.			520	0.05		
F23-11	±45	260	9,020	0.65		
F24-4	±45	260	7,720	0.59		
F25-1	±45	260	8,610	0.65		
F26-8	±45	260	8,730	0.60		
F27-3	±45	260	7,940	0.58		
Avg.			8,400	0.61		
Std.Dev.			550	0.03		
F23-3	±45	350	8,530	0.43		
F24-7	±45	350	8,180	0.45		
F25-10	±45	350	8,560	0.45		
F26-2	±45	350	7,670	0.40		
F27-5	±45	350	7,720	0.41		
Avg.			8,130	0.43		
Std.Dev.			430	0.02		

Test: Inplane Shear

Materials: SiC/5506

Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Inplane Shear Modulus (10 ⁶ psi)	Ultimate Strain (in/in)	Remarks
G14-3	±45°	-67	10.31	1.02		
G14-4	±45°	-67	10.12	1.06		
G15-2	±45°	-67	10.20	1.07		
G17-3	±45°	-67	8.85	1.12		
G17-6	±45°	-67	9.83	1.07		
Avg.			9.86	1.07		
Std.Dev.			0.59	---		
G14-5	±45°	72	8.85	0.76		
G15-1	±45°	72	8.26	0.87		
G15-4	±45°	72	8.76	0.76		
G17-1	±45°	72	8.97	0.88		
G17-4	±45°	72	8.46	0.73		
Avg.			8.66	0.80		
Std.Dev.			0.29	0.07		
G14-7	±45°	260	5.80	0.50		
G16-4	±45°	260	6.27	0.33		
G17-2	±45°	260	6.11	0.39		
G17-7	±45°	260	5.37	0.37		
G17-8	±45°	260	5.35	0.39		
Avg.			5.78	0.39		
Std. Dev.			0.42	0.06		
G14-1	±45°	350	3.97	0.12		
G14-2	±45°	350	3.93	0.11		
G14-6	±45°	350	3.94	0.18		
G15-3	±45°	350	4.09	0.11		
G17-5	±45°	350	3.84	0.10		
Avg.			3.95	0.12		
Std.Dev.			0.09	0.03		

Test: Inplane Shear						
Materials: HyE 2034D						
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Inplane Shear Modulus (10 ⁶ psi)	Ultimate Strain (in/in)	Remarks
H11-8	±45°	-67	5.83	0.99		
H16-4	±45°	-67	6.12	1.02		
H17-4	±45°	-67	5.81	1.02		
H17-7	±45°	-67	6.22	1.00		
H12-7	±45°	-67	5.67	1.31		
Avg.			5.93	1.07		
Std.Dev.			0.23	0.14		
H11-7	±45°	72	5.51	0.76		
H13-8	±45°	72	5.50	0.80		
H15-4	±45°	72	5.39	0.68		
H15-5	±45°	72	5.59	0.74		
H15-7	±45°	72	5.14	0.66		
Avg.			5.43	0.73		
Std.Dev.			0.17	0.06		
H10-2	±45°	260	4.68	0.68		
H12-13	±45°	260	4.70	0.68		
H13-1	±45°	260	4.88	0.66		
H14-10	±45°	260	4.48	0.63		
H17-6	±45°	260	4.47	0.66		
Avg.			4.69	0.66		
Std.Dev.			0.14	0.02		
H10-5	±45°	350	4.36	0.68		
H11-9	±45°	350	4.21	0.60		
H14-5	±45°	350	4.54	0.56		
H18-2	±45°	350	4.56	0.62		
H19-4	±45°	350	4.22	0.57		
Avg.			4.38	0.61		
Std.Dev.			0.17	0.04		

Test: Inplane Shear

Materials: T300/V378A

Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Inplane Shear Modulus (10 ⁶ psi)	Ultimate Strain (in/in)	Remarks
I4-6	±45	-67	11.19	0.91		
I5-10	±45	-67	11.56	0.97		
I6-8	±45	-67	10.48	0.92		
I9-1	±45	-67	10.42	0.90		
I10-5	±45	-67	10.17	0.92		
Avg.			10.76	0.92		
Std.Dev.			0.59	0.03		
I4-3	±45	72	9.59	0.89		
I9-9	±45	72	11.07	0.95		
I10-7	±45	72	10.71	0.97		
I11-5	±45	72	10.98	0.91		
I22-1	±45	72	10.88	0.95		
Avg.			10.65	0.93		
Std.Dev.			0.61	0.03		
I8-6	±45	350	8.13	0.85		
I9-8	±45	350	8.09	0.88		
I10-10	±45	350	7.48	0.76		
I11-4	±45	350	8.39	0.95		
I22-2	±45	350	8.21	---		
Avg.			8.06	0.86		
Std.Dev.			0.35	0.08		
I5-1	±45	450	7.23	0.63		
I8-7	±45	450	7.46	0.69		
I9-6	±45	450	7.51	0.58		
I10-9	±45	450	7.44	0.54		
I11-8	±45	450	7.70	0.58		
Avg.			7.47	0.60		
Std.Dev.			0.17	0.06		

Test: Inplane Shear
Materials: HyE 1076J

Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Inplane Shear Modulus (10 ⁶ psi)	Ultimate Strain (in/in)	Remarks
J4-3	±45°	-67	13.39	0.99		
J6-2	±45°	-67	15.46	0.89		
J8-2	±45°	-67	13.20	1.08		
J10-2	±45°	-67	13.34	1.03		
J11-3	±45°	-67	13.34	1.03		
Avg.			13.75	1.00		
Std.Dev.			0.96	0.07		
J3-2	±45°	72	11.00	0.90		
J5-6	±45°	72	11.09	0.84		
J8-2	±45°	72	11.08	0.94		
J11-2	±45°	72	11.36	0.93		
J12-2	±45°	72	11.17	0.96		
Avg.			11.14	0.92		
Std.Dev.			0.14	0.05		
J3-1	±45°	260	7.78	0.87		
J5-1	±45°	260	7.90	0.90		
J7-1	±45°	260	8.72	0.92		
J9-1	±45°	260	8.45	0.94		
J11-1	±45°	260	8.38	0.82		
Avg.			8.25	0.89		
Std.Dev.			0.40	0.05		
J3-6	±45°	350	8.36	0.79		
J4-2	±45°	350	8.18	0.81		
J7-6	±45°	350	9.36	0.70		
J9-7	±45°	350	7.67	0.82		
J11-8	±45°	350	7.93	0.71		
Avg.			8.30	0.77		
Std.Dev.			0.65	0.06		

Test: Inplane Shear						
Materials: G-160/6535-1						
Specimen Number	Fiber Orientation	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Inplane Shear Modulus (10 ⁶ psi)	Ultimate Strain (in/in)	Remarks
K4-4	±45°	-67	9.34	1.03		
K6-2	±45°	-67	9.85	0.97		
K7-4	±45°	-67	10.44	0.96		
K10-3	±45°	-67	9.44	1.01		
K11-1	±45°	-67	9.47	1.10		
Avg.			9.71	1.01		
Std.Dev.			0.45	0.06		
K5-1	±45°	72	8.87	0.94		
K6-1	±45°	72	9.00	0.96		
K7-1	±45°	72	7.68	0.98		
K8-1	±45°	72	8.90	0.90		
K9-1	±45°	72	7.72	0.94		
Avg.			8.43	0.94		
Std.Dev.			0.67	0.03		
K4-2	±45°	260	7.74	0.82		
K5-2	±45°	260	7.90	0.96		
K7-2	±45°	260	7.94	0.89		
K9-2	±45°	260	7.86	0.87		
K10-2	±45°	260	7.42	0.89		
Avg.			7.77	0.89		
Std.Dev.			0.21	0.05		
K4-3	±45°	350	7.76	0.79		
K5-3	±45°	350	8.74	0.84		
K7-3	±45°	350	8.66	0.86		
K9-3	±45°	350	8.50	0.80		
K10-2	±45°	350	7.54	0.78		
Avg.			8.24	0.81		
Std.Dev.			0.55	0.03		

APPENDIX H
INTERLAMINAR SHEAR DATA

All of the interlaminar shear data generated during this program are tabulated in this appendix. Tabular summaries of these data appear in Sections 4.1 through 4.6.

Test: Interlaminar (Short-Beam) Shear			
Materials: T300/AFR800		L/D Ratio: 4/1	
Specimen Number	Test Temp. (°F)	Ultimate Strength (psi)	Remarks
F21-23	-67	19,020	
F21-45	-67	17,550	
F21-55	-67	17,700	
F21-58	-67	17,270	
F21-61	-67	19,290	
Avg.		18,170	
Std.Dev.		920	
F21-6	72	15,290	
F21-9	72	15,520	
F21-11	72	17,160	
F21-20	72	14,440	
F21-36	72	15,310	
F21-53	72	15,340	
F21-64	72	14,370	
F21-66	72	14,620	
F21-69	72	15,400	
F21-75	72	15,160	
Avg.		15,270	
Std.Dev.		790	
F21-33	260	12,810	
F21-43	260	11,020	
F21-44	260	11,920	
F21-57	260	11,300	
F21-68	260	11,820	
Avg.		11,770	
Std. Dev.		690	

Test: Interlaminar (Short-Beam) Shear			
Materials: sic/5506		L/D Ratio: 4/1	
Specimen Number	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Remarks
G38-6	-67	21.27	
G38-28	-67	21.63	
G38-51	-67	21.32	
G38-57	-67	21.06	
G38-63	-67	21.10	
Avg.		21.29	
Std.Dev.		0.25	
G38-2	72	14.80	
G38-4	72	14.85	
G38-8	72	14.96	
G38-12	72	15.01	
G38-20	72	15.21	
G38-24	72	14.72	
G38-30	72	14.96	
G38-36	72	15.20	
G38-40	72	15.19	
G38-48	72	15.31	
Avg.		15.02	
Std.Dev.		0.20	
G38-1	260	8.81	
G38-16	260	9.55	
G38-39	260	8.86	
G38-41	260	9.20	
G38-54	260	9.18	
Avg.		9.12	
Std.Dev.		0.30	

Test: Interlaminar (Short-Beam) Shear			
Materials: HyE 2034D		L/D Ratio: 4/1	
Specimen Number	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Remarks
H31-2	-67	9.06	
H31-7	-67	7.83	
H31-16	-67	8.14	
H31-44	-67	7.91	
H31-54	-67	7.51	
Avg.		8.09	
Std.Dev.		0.59	
H31-1	72	7.57	
H31-5	72	7.17	
H31-10	72	7.07	
H31-22	72	7.85	
H31-36	72	7.06	
H31-42	72	7.57	
H31-48	72	7.57	
H31-51	72	6.55	
H31-55	72	6.97	
H31-66	72	6.45	
Avg.		7.18	
Std.Dev.		0.46	
H31-3	260	7.12	
H31-8	260	6.24	
H31-28	260	6.13	
H31-30	260	6.04	
H31-46	260	6.87	
Avg.		6.48	
Std.Dev.		0.48	

Test: Interlaminar (Short-Beam) Shear			
Materials: T300/V378A		L/D Ratio: 4/1	
Specimen Number	Test Temp. (°F)	Ultimate Strength (psi)	Remarks
I15-9	-67	18,800	
I15-14	-67	17,300	
I15-26	-67	18,540	
I15-38	-67	18,250	
I15-39	-67	17,720	
Avg.		18,140	
Std.Dev.		630	
I15-1	72	15,400	
I15-4	72	15,560	
I15-8	72	14,860	
I15-13	72	14,230	
I15-20	72	14,520	
I15-25	72	15,550	
I15-29	72	15,160	
I15-32	72	15,170	
I15-37	72	14,410	
I15-45	72	15,320	
Avg.		15,020	
Std.Dev.		490	
I15-10	350	9,030	
I15-16	350	10,090	
I15-24	350	10,190	
I15-27	350	10,760	
I15-34	350	10,010	
Avg.		10,020	
Std.Dev.		620	

Test: Interlaminar (Short-Beam) Shear			
Materials: HYE 1076J		L/D Ratio: 4/1	
Specimen Number	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Remarks
J26-23	-67	16.26	
J26-41	-67	14.24	
J26-67	-67	19.64	
J26-78	-67	15.25	
J26-80	-67	17.72	
Avg.		16.62	
Std.Dev.		2.12	
J26-16	72	11.04	
J26-19	72	9.42	
J26-26	72	10.96	
J26-33	72	14.94	
J26-40	72	11.67	
J26-49	72	12.66	
J26-53	72	11.67	
J26-69	72	17.11	
J26-74	72	14.70	
J26-83	72	14.56	
Avg.		12.87	
Std.Dev.		2.36	
J26-18	260	8.59	
J26-34	260	10.79	
J26-38	260	8.96	
J26-52	260	8.61	
J26-64	260	9.85	
Avg.		9.36	
Std.Dev.		0.95	

L/D Ratio: 4/1

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Test: Interlaminar (Short-Beam) Shear			
Materials: G-160/6535-1		L/D Ratio: 4/1	
Specimen Number	Test Temp. (°F)	Ultimate Strength (10 ³ psi)	Remarks
K18-12	-67	17.51	
K18-28	-67	18.21	
K18-38	-67	15.19	
K18-46	-67	16.65	
K18-62	-67	17.20	
Avg.		16.96	
Std. Dev.		1.14	
K18-1	72	14.03	
K18-10	72	15.55	
K18-18	72	15.87	
K18-23	72	14.21	
K18-31	72	13.10	
K18-34	72	14.26	
K18-37	72	12.84	
K18-41	72	13.79	
K18-47	72	16.13	
K18-52	72	15.54	
Avg.		14.53	
Std. Dev.		1.17	
K18-2	260	11.36	
K18-16	260	11.46	
K18-48	260	12.39	
K18-57	260	12.28	
K18-63	260	12.02	
Avg.		11.90	
Std. Dev.		0.47	

Test: Interlaminar (Short-Beam) Shear

Materials: G-160/6535-1

L/D Ratio: 4/1

[illegible]

APPENDIX I

FATIGUE DATA

All of the tensile-tensile fatigue data generated during the program, along with residual strengths of specimens which "ran out" to 10^7 cycles are presented here. The residual strengths were all determined with a tensile test at 72°F (22°C), regardless of what temperature the specimen saw during the fatigue test. Summaries of these data are presented in Sections 4.1 through 4.6 in both tabular and graphical form.

Test: Tensile-Tensile Fatigue									
Material: T300/AFR800									
R = +0.1 Frequency = 30 Hz Function: Sine									
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (% ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
F1-2	0°	72	143.7	14.4	80	327,700	---	---	
F1-4	0°	72	143.7	14.4	80	23,600	---	---	
F1-10	0°	72	143.7	14.4	80	51,200	---	---	
F3-5	0°	72	143.7	14.4	80	1,400	---	---	
F3-6	0°	72	143.7	14.4	80	345,500	---	---	
F5-6	0°	72	134.7	13.5	75	10,000,000+	---	229.9	
F6-4	0°	72	134.7	13.5	75	160,200	---	---	
F6-12	0°	72	134.7	13.5	75	2,294,900	---	---	
F22-3	0°	72	134.7	13.5	75	10,000,000+	---	151.3	
F22-5	0°	72	134.7	13.5	75	10,000,000+	---	239.7	
F22-11	0°	72	134.7	13.5	75	10,000,000+	---	223.3	
F2-12	0°	72	125.7	12.6	70	7,800	---	---	
F4-4	0°	72	125.7	12.6	70	10,000,000+	---	201.7	
F4-5	0°	72	125.7	12.6	70	10,000,000+	---	198.8	
F5-1	0°	72	125.7	12.6	70	10,000,000+	---	209.3	
F6-7	0°	72	125.7	12.6	70	1,999,400	+5	---	
F22-16	0°	72	125.7	12.6	70	5,888,600	---	---	failed by operator error

[illegible]

Test: Tensile-Tensile Fatigue

Material: SiC/5506

[illegible][illegible]

Test: Tensile-Tensile Fatigue									
Material: HVE 2034D									
R = +0.1									
Frequency = 30 Hz									
Function: Sine									
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (% ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
H17-1	+45°	72	6.51	0.65	60	3,543,500	2	---	
H14-3	+45°	72	6.51	0.65	60	10,000,000	2	10.33	
H13-5	+45°	72	6.51	0.65	60	10,000,000	2	9.71	
H10-1	+45°	72	6.51	0.65	60	10,000,000	3	9.36	
H19-2	+45°	72	8.14	0.81	75	69,500	6	---	
H16-1	+45°	72	8.14	0.81	75	39,300	4	---	
H14-1	+45°	72	8.14	0.81	75	47,300	3	---	
H13-2	+45°	72	8.14	0.81	75	150,900	4	---	
H11-1	+45°	72	8.14	0.81	75	107,300	10	---	
H18-9	+45°	72	8.60	0.87	80	64,200	3	---	
H15-3	+45°	72	8.68	0.87	80	58,000	4	---	
H13-7	+45°	72	8.68	0.87	80	13,800	3	---	
H12-2	+45°	72	8.68	0.87	80	2,700	3	---	
H10-10	+45°	72	8.68	0.87	80	43,500	7	---	
H19-3	+45°	260	6.10	0.61	65	7,767,200	0	---	
H16-2	+45°	260	6.57	0.66	70	88,300	3	---	
H14-2	+45°	260	6.57	0.66	70	1,543,000	5	---	
H13-3	+45°	260	6.57	0.66	70	1,372,400	7	---	
H11-4	+45°	260	6.57	0.66	70	5,089,600	2	---	

Test: Tensile-Tensile Fatigue									
R = +0.1									
Frequency = 30 Hz									
Material: HYE 2034D									
Function: Sine									
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (8 ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
H18-10	±45°	260	7.04	0.70	75	117,200	4	---	
H15-1	±45°	260	7.04	0.70	75	316,600	2	---	
H13-6	±45°	260	7.04	0.70	75	98,700	8	---	
H12-1	±45°	260	7.04	0.70	75	113,700	4	---	
H10-3	±45°	260	7.04	0.70	75	97,800	5	---	
H19-1	±45°	260	7.98	0.80	85	2,300	2	---	
H15-8	±45°	260	7.98	0.80	85	3,100	4	---	
H13-10	±45°	260	7.98	0.80	85	6,100	6	---	
H12-6	±45°	260	7.98	0.80	85	3,500	5	---	
H11-2	±45°	260	7.98	0.80	85	5,700	7	---	
H22-8	0/±45/90°	72	73.92	7.39	97.5	800	3	---	
H23-8	0/±45/90°	72	73.92	7.39	97.5	467,600	3	---	
H28-10	0/±45/90°	72	73.92	7.39	97.5	4,200	9	---	
H25-5	0/±45/90°	72	72.03	7.20	95	13,600	5	---	
H26-8	0/±45/90°	72	72.03	7.20	95	500	0	---	
H27-7	0/±45/90°	72	72.03	7.20	95	10,000,000+	8	78.78	
H21-9	0/±45/90°	72	72.03	7.20	95	12,000	10	---	
H33-4	0/±45/90°	72	72.03	7.20	95	10,000,000+	5	79.68	
H21-7	0/±45/90°	72	75.82	7.58	100	15,900	9	---	
H22-5	0/±45/90°	72	75.82	7.58	100	300	1	---	
H23-2	0/±45/90°	72	75.82	7.58	100	1,200	1	---	
H24-9	0/±45/90°	72	75.82	7.58	100	1,058,200	6	---	
H24-4	0/±45/90°	72	75.82	7.58	100	7,638,000	5	---	

(0, +45, -45, 0, 0, -45, +45, 0, 90, 0) _s - 20 ply

Test: Tensile-Tensile Fatigue									
Material: T300/V378A									
R = 40.1									
Frequency = 30 Hz									
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (% ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
I2-6	±45°	72	15.97	1.60	75	31,000	8	---	
I7-2	±45°	72	15.97	1.60	75	24,200	9	---	
I10-3	±45°	72	15.97	1.60	75	9,100	7	---	
I11-6	±45°	72	15.97	1.60	75	20,500	8	---	
I22-C	±45°	72	15.97	1.60	75	9,400	9	---	
I3-2	±45°	72	14.90	1.49	70	47,600	6	---	
I7-3	±45°	72	14.90	1.49	70	92,700	6	---	
I10-6	±45°	72	14.90	1.49	70	61,600	6	---	
I11-2	±45°	72	14.90	1.49	70	82,700	6	---	
I3-9	±45°	72	13.84	1.38	65	582,500	5	---	
I7-6	±45°	72	13.84	1.38	65	269,900	4	---	
I10-2	±45°	72	13.84	1.38	65	210,000	8	---	
I11-3	±45°	72	13.84	1.38	65	433,000	5	---	
I22-4	±45°	72	13.84	1.38	65	1,020,700	6	---	
I3-8	±45°	350	13.70	1.37	85	9,400	14	---	
I6-1	±45°	350	13.70	1.37	85	3,900	19	---	
I7-1	±45°	350	13.70	1.37	85	500	5	---	
I10-8	±45°	350	13.70	1.37	85	10,300	15	---	
I22-3	±45°	350	13.70	1.37	85	12,500	13	---	
I6-7	±45°	350	12.90	1.29	80	59,300	9	---	
I10-1	±45°	350	12.90	1.29	80	50,500	6	---	
I11-1	±45°	350	12.90	1.29	80	43,100	5	---	
I22-8	±45°	350	12.90	1.29	80	56,700	9	---	

Test: Tensile-Tensile Fatigue									
Material: T330/V378A									
R = +0.1									
Frequency = 30 Hz									
Function: Sine									
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (8 ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
I35-6	0/±45/90 ¹	350	90.10	9.01	85	328,700	42	---	
I36-6	0/±45/90 ¹	350	90.10	9.01	85	613,500	24	---	
I37-8	0/±45/90 ¹	350	90.10	9.01	85	960,500	34	---	
I14-6	0/±45/90 ¹	350	87.45	8.75	82.5	1,229,400	38	---	
I36-7	0/±45/90 ¹	350	87.45	8.75	82.5	2,128,300	20	---	overheated to 525°F
I39-10	0/±45/90 ¹	350	87.45	8.75	82.5	332,400	17	---	
I12-8	0/±45/90 ¹	350	84.80	8.48	80	102,400	52	---	
I13-8	0/±45/90 ¹	350	84.80	8.48	80	660,000	29	---	
I33-8	0/±45/90 ¹	350	84.80	8.48	80	626,100	22	---	
I39-8	0/±45/90 ¹	350	84.80	8.48	80	432,200	32	---	
I40-8	0/±45/90 ¹	350	84.80	8.48	80	2,320,600	54	---	
I13-2	0/±45/90 ^{1,2}	72	88.45	8.85	95	260,100	59	---	
I14-2	0/±45/90 ^{1,2}	72	88.45	8.85	95	2,191,900	45	---	
I36-1	0/±45/90 ^{1,2}	72	88.45	8.85	95	2,012,300	75	---	
I39-1	0/±45/90 ^{1,2}	72	88.45	8.85	95	225,500	57	---	
I13-1	0/±45/90 ^{1,2}	72	83.79	8.38	90	61,300	53	---	
I14-1	0/±45/90 ^{1,2}	72	83.79	8.38	90	932,600	54	---	
I37-1	0/±45/90 ^{1,2}	72	83.79	8.38	90	1,587,800	32	---	
I12-2	0/±45/90 ^{1,2}	72	79.14	7.91	85	265,700	42	---	
I28-2	0/±45/90 ^{1,2}	72	79.14	7.91	85	1,252,600	50	---	
I38-2	0/±45/90 ^{1,2}	72	79.14	7.91	85	1,024,200	58	---	
I40-1	0/±45/90 ^{1,2}	72	79.14	7.91	85	2,399,300	52	---	

¹(0, +45, -45, 0, 0, -45, -45, 0, 90, 0) _s - 20 ply

²These specimens had a 0.1935 inch (0.491 cm) hole in center of test section. Stresses based on net cross-sectional area.

Test: Tensile-Tensile Fatigue									
R = +0.1									
Frequency = 30 Hz									
Material: HYE 1076J									
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (% ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
									Function: Sine
J3-5	±45	72	17.82	1.78	80	11,600	9	---	
J6-1	±45	72	17.82	1.78	80	1,700	11	---	
J7-4	±45	72	17.82	1.78	80	5,400	6	---	
J9-6	±45	72	17.82	1.78	80	6,500	9	---	
J11-7	±45	72	17.82	1.78	80	8,700	9	---	
J4-5	±45	72	15.60	1.56	70	200,300	8	---	
J6-6	±45	72	15.60	1.56	70	210,200	24	---	
J8-5	±45	72	15.60	1.56	70	153,800	20	---	
J10-5	±45	72	15.60	1.56	70	72,600	19	---	
J12-5	±45	72	15.60	1.56	70	188,800	12	---	
J7-5	±45	72	14.48	1.45	65	1,202,100	7	---	
J8-7	±45	72	14.48	1.45	65	883,600	8	---	
J10-7	±45	72	14.48	1.45	65	1,005,800	4	---	
J12-7	±45	72	14.48	1.45	65	1,475,500	8	---	
J5-4	±45	72	13.37	1.34	60	5,000,000+	9	20.07	test terminated
J4-1	±45	260	14.02	1.40	85	43,400	18	---	
J6-5	±45	260	14.02	1.40	85	42,200	5	---	
J8-1	±45	260	14.02	1.40	85	17,700	11	---	
J10-1	±45	260	14.02	1.40	85	17,300	24	---	
J12-1	±45	260	14.02	1.40	85	12,000	8	---	

Test: Tensile-Tensile Fatigue										R = +0.1
Material: HYE 1076J										Frequency = 30 Hz
										Function: Sine
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (% ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks	
J3-4	+45	260	13.19	1.32	80	83,800	10	---		
J5-5	+45	260	13.19	1.32	80	133,800	14	---		
J7-7	+45	260	13.19	1.32	80	106,500	10	---		
J9-5	+45	260	13.19	1.32	80	25,700	26	---		
J11-6	+45	260	13.19	1.32	80	60,500	10	---		
J4-6	+45	260	12.37	1.24	75	924,300	5	---		
J6-7	+45	260	12.37	1.24	75	935,200	7	---		
J8-6	+45	260	12.37	1.24	75	158,400	7	---		
J10-6	+45	260	12.37	1.24	75	513,200	7	---		
J12-6	+45	260	12.37	1.24	75	397,800	6	---		
J14-3	0/+45/90	72	105.14	10.51	90	4,800	46	---		
J17-2	0/+45/90	72	105.14	10.51	90	8,900	42	---		
J21-3	0/+45/90	72	105.14	10.51	90	88,200	65	---		
J23-7	0/+45/90	72	105.14	10.51	90	2,400	30	---		
J25-3	0/+45/90	72	105.14	10.51	90	285,000	38	---		
J20-3	0/+45/90	72	102.22	10.22	87.5	25,300	39	---		
J22-4	0/+45/90	72	102.22	10.22	87.5	575,800	25	---		
J24-2	0/+45/90	72	102.22	10.22	87.5	417,300	36	---		
J13-3	0/+45/90	72	99.30	9.93	85	580,800	46	---		
J15-3	0/+45/90	72	99.30	9.93	85	6,349,300	23	---		
J17-3	0/+45/90	72	99.30	9.93	85	546,200	42	---		
J22-3	0/+45/90	72	99.30	9.93	85	8,077,000	32	---		
J23-8	0/+45/90	72	99.30	9.93	85	12,400	39	---		

'(0, +45, -45, 0, 0, -45, +45, 0 90, 0)s -20 ply

Test: Tensile-Tensile Fatigue									
Material: HVE 1076J									
R = +0.1									
Frequency = 30 Hz									
Function: Sine									
Specimen Number	Y/θ Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (% ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
J17-1	0/±45/90	72	97.35	9.74	110	900	---	---	
J21-1	0/±45/90	72	97.35	9.74	110	600	---	---	
J15-1	0/±45/90	72	97.35	9.74	110	993,800	55	---	
J25-2	0/±45/90	72	97.35	9.74	110	6,178,200	54	---	
J16-1	0/±45/90	72	92.93	9.29	105	2,207,400	52	---	
J20-2	0/±45/90	72	92.93	9.29	105	1,100	9	---	
J22-2	0/±45/90	72	92.93	9.29	105	1,100	---	---	
J24-1	0/±45/90	72	92.93	9.29	105	700	---	---	
J23-9	0/±45/90	72	90.00	9.00	102	1,593,700	49	---	
J13-1	0/±45/90	72	88.50	8.85	100	900	---	---	
J15-2	0/±45/90	72	88.50	8.85	100	10,000,000+	46	118.35	
J20-1	0/±45/90	72	88.50	8.85	100	1,483,700	34	---	
J22-1	0/±45/90	72	88.50	8.85	100	620,900	45	---	
J23-10	0/±45/90	72	88.50	8.85	100	900	5	---	
J14-1	0/±45/90	72	84.08	8.41	95	10,000,000+	44	102.44	

¹ (0, +45, -45, 0, 0, -45, +45, 0, 90, 0)_s -20 ply

² These specimens had a 0.1935 inch (0.491 cm) hole in center of test section. Stresses based on net cross-sectional area.

Test: Tensile-Tensile Fatigue									
R = +0.1									
Frequency = 30 Hz									
Material: G-160/6535-1									
Function: Sine									
Specimen Number	Fiber Orientation	Test Temp. (°F)	Max. Stress (10 ³ psi)	Min. Stress (10 ³ psi)	Max. Stress (% ult.)	Cycles to Failure	Temp. Rise (°F)	Residual Strength (10 ³ psi)	Remarks
K37-1	0/45/90 ¹	72	68.64	6.86	75	46,700	30		
K37-6	0/45/90 ¹	72	68.64	6.86	75	1,094,400	18		
K38-2	0/45/90 ¹	72	68.64	6.86	75	1,500	5		
K38-8	0/45/90 ¹	72	68.64	6.86	75	10,136,000+	21		
K39-6	0/45/90 ¹	72	68.64	6.86	75	39,700	39		
K24-3	0/45/90 ²	72	86.34	8.63	95	700	5		
K24-7	0/45/90 ²	72	86.34	8.63	95	200	---		
K25-6	0/45/90 ²	72	86.34	8.63	95	3,200	9		
K26-3	0/45/90 ²	72	86.34	8.63	95	400	6		
K26-6	0/45/90 ²	72	86.34	8.63	95	4,600	30		
K24-2	0/45/90 ²	72	81.79	8.18	90	453,400	23		
K24-6	0/45/90 ²	72	81.79	8.18	90	5,600	36		
K25-4	0/45/90 ²	72	81.79	8.18	90	217,300	24		
K25-8	0/45/90 ²	72	81.79	8.18	90	30,900	33		
K26-5	0/45/90 ²	72	81.79	8.18	90	13,900	39		
K24-5	0/45/90 ²	72	77.25	7.73	85	363,400	25		
K25-2	0/45/90 ²	72	77.25	7.73	85	2,578,800	15		
K25-7	0/45/90 ²	72	77.25	7.73	85	24,900	13		
K26-4	0/45/90 ²	72	77.25	7.73	85	321,700	32		
K26-7	0/45/90 ²	72	77.25	7.73	85	11,600	18		

¹ (0,90,+45,-45,0,0,-45,+45,0,0) s-20 ply; ² (0,45,-45,0,0,-45,45,0,90,0) s-20 ply.

[illegible] $^3(0,45,-45,0,0,-45,45,0)_S-16 \text{ ply.}$

APPENDIX J

CREEP AND STRESS RUPTURE DATA

All of the tensile creep data generated during this program, along with residual strengths of specimens which "ran out" to 500 hours are presented in this section. The residual strengths were all determined with a 72°F (22°C) tensile test regardless of what temperature the specimen saw during the creep test.

The stress rupture data were also obtained from these same specimens with the characteristic of interest being time to fracture rather than elongation.

Summaries of these data are presented in Sections 4.1 through 4.6 in both tabular and graphical form.

In the succeeding tables the specimen numbering system can be used to identify the material being tested. The letter, appearing first, in the specimen numbering code indicates the material, as follows:

- F - T300/AFR800
- G - SiC/5506
- H - HyE 2034D
- I - T300/V378A
- J - HyE 1076J
- K - G-160/6535-1

AFR-800

[illegible][illegible][illegible]

[illegible][illegible][illegible]

AFR-800

[illegible][illegible]

Test: <u>Creep</u>		
Orient: <u>0°</u>		
Spec. No: <u>F4-12</u>		
Temp: <u>260°F (127°C)</u>		
Stress <u>174.5 ksi</u> <u>90% ult.</u>		
Elap. Time (hrs.)	Accum. Strain (μin/in)	Remarks
0	8531	
0.017	8531	
0.10	8531	
0.25	8531	
0.50	8531	
1	8532	
2	8532	
3	8537	
4	8525	
6	8529	
24	8554	
51.5	8604	
79	8680	
310	9726	
486	---	gage failed
500+		
specimen did not fail		
Recovery		

[illegible][illegible][illegible]

[illegible][illegible][illegible]

[illegible]

Test: <u>Creep</u>		
Orient: <u>0°</u>		
Spec. No: <u>F22-1</u>		
Temp: <u>350°F (177°C)</u>		
Stress: <u>156.2 ksi 90 % ult.</u>		
Elap. Time (hrs.)	Accum. Strain (in/in)	Remarks
0	8310	
0.017	8324	
0.10	8337	
0.25	8340	
0.50	8359	
1	8318	
2	8307	
4	8329	
5	8313	
6	8314	
7	8306	
24	8280	
168	8221	
264	8221	
360	8216	
432	8256	
503	8271	
Recovery		
0	366	Load off
1	306	
2	296	
3	291	

[illegible]

[illegible][illegible][illegible]

[illegible][illegible][illegible]

[illegible]

Test: <u>Creep</u>		
Orient: <u>0°</u>		
Spec. No: <u>F3-14</u>		
Temp: <u>350°F(177°C)</u>		
Stress: <u>121.5 ksi</u> <u>70 %</u> ult.		
Elap. Time (hrs.)	Accum. Strain (μin/in)	Remarks
0	missed reading	
0.75	6526	
1	6535	
2	6541	
3	6551	
4	6557	
5	6558	
6	6566	
24	6622	
95	6723	
144	6762	
192	6792	
264	6812	
360	6847	
432	6880	
503	6892	
Recovery		
0	1402	Load off
1	1368	
2	1355	
3	1353	

[illegible]

AFR-800

[illegible][illegible][illegible]

~~APP-006~~

[illegible]

Test: <u>Creep</u>		
Orient: <u>90°</u>		
Spec. No: <u>P9-3</u>		
Temp: <u>72°F (22°C)</u>		
Stress: <u>2.75 ksi</u> <u>60 %</u> ult.		
Elap. Time (hrs.)	Accum. Strain (Min/in)	Remarks
0	missed	reading
0.017	1893	
0.10	1905	
0.25	1919	
0.50	1928	
1	1933	
2	1950	
5	1968	
8	1981	
24	2002	
145	2116	
194	2142	
318	2199	
482	2261	
530.4	2248	
Recovery		
0	376	Load off
1	314	

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Test: Creep		
Ori.ent: 90°		
Spec.No: F9-8		
Temp: 72°F (22°C)		
Stress 2.29 ksi 50 % ult.		
Elap. Time (hrs.)	Accum. Strain ($\mu\text{in/in}$)	Remarks
0	1543	
0.017	1553	
0.10	1567	
0.25	1579	
0.50	1581	
1	1591	
2	1599	
3	1618	
5	1630	
6	1638	
7	1640	
8	1644	
24	1660	
72	1688	
145	1702	
245	1806	
435	1857	
482	1885	
602	1959	
Recovery		
0	420	Load off
1	374	
3	358	

AFR-300

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[illegible][illegible]

Test: <u>Creep</u>		
Orient: <u>90°</u>		
Spec. No: <u>P14-5</u>		
Temp: <u>260°F (127°C)</u>		
Stress <u>2.57 ksi</u> <u>55% ult.</u>		
Elap. Time (hrs.)	Accum. Strain (in/in)	Remarks
0	1955	
0.017	1966	
0.10	1976	
0.33	2031	
0.50	2034	
1	2059	
2	2082	
3	2091	
5	2100	
6	2105	
7	2106	
24.3	2109	
72	2143	
144	2190	
240	2272	
313	2319	
408	2340	
506	2393	
Recovery		
0	501	Load off
1	409	
3	375	

[illegible]

Test: Creep		
Orient: 90°		
Spec. No: F34-1		
Temp: 350°F (177°C)		
Stress: 2.71 ksi 50% ult.		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	2319	
0.017	2398	
0.10	3401	
0.25	3860	
0.50	4112	
1	4800	
2	5052	
3	5084	
4	5059	
5	5070	
6	5065	
24	5374	
68	--	Failure
Recovery		

[illegible]

AFH-800

[illegible][illegible][illegible]

Test: <u>Creep</u>		
Orient: <u>90°</u>		
Spec. No: <u>F34-7</u>		
Temp: <u>350°F (177°C)</u>		
Stress: <u>1.63 ksi 30% ult.</u>		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	2230	0 = 1000
0.017	2245	
0.10	2277	
0.25	2305	
0.50	2371	
1	2460	
2	2589	
5.2	2731	
6	2754	
7	2701	
48	2689	
52	3091	
72	3289	
145	3618	
240	3760	
312	3900	
414	4140	
505	4164	
Recovery		
0	2876	Load off
1	2529	
2	2365	
4.5	2198	

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[illegible][illegible][illegible]

AFR-800

Test: Creep
 Orient: +45°
 Spec. No: F23-2
 Temp: 72°F(22°C)
 Stress: 13.94 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6540	
0.017	6653	
0.10	6779	
0.25	6935	
0.583	7235	
1	7297	
2	7450	
3	7542	
5.2	7601	
7.2	7654	
47.4	8187	4112
148	8725	
217	8793	
366	9254	
413	9267	4127
480	9362	
503	9404	

Recovery

0	2674	Load off
1	1972	
2	1932	

Test: Creep
 Orient: +45°
 Spec. No: F23-4
 Temp: 72°F(22°C)
 Stress: 13.94 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6449	
0.017	6543	
0.10	6630	
0.25	6747	
0.583	7036	
1	7114	
2	7230	
3	7294	
5.2	7362	
7.2	7392	
47.4	7887	
148	8376	
217	8440	
366	8894	
413	8895	
480	8967	
503	9001	

Recovery

0	2336	Load off
1	1811	
2	1760	

Test: Creep
 Orient: +45°
 Spec. No: F25-2
 Temp: 72°F(22°C)
 Stress: 13.94 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6457	
0.017	6536	
0.10	6620	
0.25	6778	
0.583	7064	
1	7129	
2	7280	
3	7371	
5.2	7378	
7.2	7497	
47.4	7874	
148	8478	
217	8546	
366	8978	
413	8989	
480	9067	
503	9119	

Recovery

0	2400	Load off
1	1908	
2	1864	

AFR-600

[illegible][illegible][illegible]

AFR-800

[illegible][illegible][illegible]

AFR-800

Test: Creep		
Orient: +45°		
Spec. No: F30-11		
Temp: 269°F(127°C)		
Stress: 11.76 ksi 70% ult.		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	7818	
0.017	9154	
0.10	10116	
0.25	10805	
0.50	11275	
1	11857	
2	12437	
2.5	12635	
4.5	13160	
5.5	13331	
6.6	13480	
7.5	13585	
24	14538	
48	14180	
74	16238	
144	17074	
366	18704	
484	19334	
506	19474	
Recovery		
0	13529	Load off
2.3	11777	
3	11627	
4	11517	

[illegible][illegible]

AFR-800

Test: Creep		
Orient: +45°		
Spec. No: P26-3		
Temp: 260°F.(127°C)		
Stress: 10.08 ksi60 % ult.		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	5039	
0.017	5212	
0.10	5585	
0.25	5788	
0.50	5973	
1	6197	
2	6426	
4	6685	
5	6768	
6	6833	
7	6959	
24	7576	
48	7891	
120	8463	
216	8955	
314	9317	
385	9572	
528	9958	
Recovery		
0	5166	Load off
1	4362	
2	4217	
4	4058	

[illegible]

Test: Creep		
Orient: +45°		
Spec. No: F26-9		
Temp: 260°F(127°C)		
Stress 10.08 ksi 60 % ult.		
Elap. Time (hrs.)	Accum. Strain ($\mu\text{in}/\text{in}$)	Remarks
0	6025	
0.017	6228	
0.10	6950	
0.25	7249	
0.42	7434	
0.50	7504	
1	7799	
2	8175	
4	8580	
5	9214	
6	9624	
7	10001	
24	12067	
48	13482	
120	15606	
216	17545	
314	19022	
385	19931	
528	21504	
Recovery		
0	15576	Load off
1	13988	
2	13611	
4	13266	

AFR-800

[illegible][illegible][illegible]

Test: Creep
Orient: +45°
Spec. No: P29-5
Temp: 350°F (177°C)
Stress: 8.14 ksi 50% ult.

[illegible]

Test: Green
Orient: +45°
Spec. No: F30-8
Temp: 350°F(177°C)
Stress: 8.14 ksi 50% ult.

[illegible]

Test: Creep
Orient: +45°
Spec. No: F33-7
Temp: 350°F (177°C)
Stress 8.14 ksi 50% ult.

[illegible]

AFR-800

[illegible][illegible][illegible]

54C/5506

Test: Creep		
Orient: +45°		
Spec. No: G28-7		
Temp: 72°F(22°C)		
Stress: 13.86 ksi 80% ult.		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	7790	
0.017	8352	
0.10	9077	
0.25	9634	
0.50	10053	
1	10545	
2	11069	
6.5	12079	
7	12211	
25	13414	
145	15490	
312	16368	
360	16566	
438	16851	
534	17166	
Recovery		
0	10178	Load off
1	7640	
1.5	7433	

[illegible][illegible]

SIC/5506

[illegible]

Test:	<u>Creep</u>	
Orient:	<u>+45°</u>	
Spec. No:	<u>G27-8</u>	
Temp:	<u>72°F(22°C)</u>	
Stress: <u>12.13 ksi</u> <u>70 % ult.</u>		
Elap. Time (hrs.)	Accum. Strain ($\mu\text{in/in}$)	Remarks
0	5367	
0.017	5681	
0.10	6017	
0.25	6297	
0.50	6519	
1	6764	
2	7033	
4.3	7379	
5	7460	
6	7543	
7	7597	
24	8175	
48	8514	
127	9380	
360	9706	
408	9773	
486	9879	
533	9928	
Recovery		
0	5010	Load off
1	3615	
2	3382	
2.5	3314	

[illegible]

SLC/5506

[illegible][illegible][illegible]

[illegible][illegible][illegible]

Test: Creep
Orient: +45°
Spec. No: G28-5
Temp: 260°F (127°C)
Stress: 8.07 ksi 70 % ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	11579	
0.027	17765	
0.10	20601	
0.25	21806	
0.50	22931	
1	23930	
2	27336	
5	32579	
6	33463	
7		gage failed
308		no failure

Recovery

Test: Creep
Orient: +45°
Spec. No: G29-7
Temp: 260°F (127°C)
Stress: 8.07 ksi 70% ult.

Elap. Time (hrs.)	Accum. Strain (in/in)	Remark
0	41063	
0.017	41063	gage failed
7	specimen	failure

Recovery

Test: Creep
Orient: +45°
Spec. No: G31-6
Temp: 260°F (127°C)
Stress 8.07 ksi 70% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	11144	
0.017	16063	
0.10	19274	
0.25	22144	
0.50	24287	
1	26229	
2		gage failed
92	specimen	failure

Recovery

S1C/5506

[illegible]

Test: Creep		
Orient: +45°		
Spec. No: G2B-4		
Temp: 260°F(127°C)		
Stress: 5.76 ksi 50 & ult.		
Elap. Time (hrs.)	Accum. Strain (Min/in)	Remarks
0	4266	
0.017	4771	
0.10	7824	
0.25	8960	
0.50	9755	
1	10400	
2	11023	
4	12322	
5	12907	
6	13382	
7	13706	
24	16054	
25	16157	
26	16288	
28	16512	
29	16662	
48	18046	
125	21956	
221	25127	
390	28699	
509	31161	
Recovery		
0	28078	Load off
1.5	26301	
2	26093	

[illegible]

S1C/5506

[illegible][illegible][illegible]

SLC/5506

[illegible][illegible][illegible]

SIC/5506

[illegible][illegible][illegible]

SiC/5506

Test: Creep		
Orient: 0°/+45°/90°		
Spec. No: G32-5		
Temp: 72°F (22°C)		
Stress: 83.48 ksi 70 % ult.		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	4580	
0.017	4589	
0.10	4599	
0.25	4607	
0.50	4611	
1	4617	
2	4621	
4	4633	
5	4635	
6	4637	
7	4643	
24	4651	
25	4655	
26	4651	
28	4652	
29	4646	
48	4650	
125	4676	
222	4702	
341	4705	
390	4731	
509	4730	
Recovery		
0	168	Load off
1	136	
2	130	

[illegible][illegible]

SIC/5506

[illegible][illegible][illegible]

SIC/5506

[illegible][illegible][illegible]

SIC/5506

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HvE 2034D

[illegible][illegible][illegible]

HYE 2034D

[illegible][illegible][illegible]

HvE 2034D

[illegible][illegible]

Test: <u>Creep</u>		
Orient: <u>+45°</u>		
Spec. No: <u>H19-6</u>		
Temp: <u>72°F (22°C)</u>		
Stress <u>5.43 ksi</u> <u>50 %</u> ult.		
Elap. Time (hrs.)	Accum. Strain (μin/in)	Remarks
0	1983	
0.017	2037	
0.10	2068	
0.25	2098	
0.50	2114	
1	2137	
3	2175	
4	2186	
5	2192	
6	2201	
28	2279	
77	2349	
148	2498	
216	2421	
316	2459	
473	2520	
504	2522	
Recovery		
0	550	Load off
1	385	
3	359	

MyZ 2034D

Test: Creep
 Orient: $\pm 45^\circ$
 Spec. No: H10-6
 Temp: 260°F (127°C)
 Stress: 4.70 ksi 50% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	1945	
0.017	1993	
0.10	2046	
0.25	2084	
0.50	2120	
1	2162	
2	2213	
3	2238	
4	2263	
5	2287	
6	2301	
7	2320	
24	2441	
79	2725	
198	3040	
312	3228	
414	3337	
504	3431	

Recovery

0	1605	Load off
1	1426	
2	1407	
4.5	1367	

Test: Creep
 Orient: $\pm 45^\circ$
 Spec. No: H11-10
 Temp: 260°F (127°C)
 Stress: 4.70 ksi 50% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	1761	
0.017	1779	
0.10	1815	
0.25	1845	
0.50	1876	
1	1909	
2	1950	
3	1973	
4	1991	
5	2004	
6	2018	
7	2029	
24	2126	
79	2384	
198	2596	
312	2730	
414	2805	
504	2884	

Recovery

0	1099	Load off
1	965	
2	950	
4.5	915	

Test: Creep
 Orient: $\pm 45^\circ$
 Spec. No: H16-6
 Temp: 260°F (127°C)
 Stress: 4.70 ksi 50% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	1750	
0.017	1829	
0.10	1880	
0.25	1918	
0.50	1957	
1	1998	
2	2049	
3	2076	
4	2104	
5	2122	
6	2132	
7	2149	
24	2271	
79	2549	
198	2886	
312	3102	
414	3279	
504	3397	

Recovery

0	1656	Load off
1	1510	
2	1501	
4.5	1457	

HYE 2034D

[illegible][illegible][illegible]

HyE 20340

Test: Creep
 Orient: +45°
 Spec. No: H12-8
 Temp: 260°F (127°C)
 Stress: 5.63 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	2133	
0.017	2257	
0.10	2345	
0.25	2411	
0.50	2469	
1	2532	
2	2616	
4	2709	
5	2739	
6	2775	
7	2796	
24	3021	
143	3552	
246	3885	
365	4208	
414	4355	
527	4666	

Recovery

0	2403	Load off
0.5	2236	
1	2188	
2	2134	
3	2096	

Test: Creep
 Orient: +45°
 Spec. No: H19-5
 Temp: 260°F (127°C)
 Stress: 5.63 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	2466	
0.017	2506	
0.10	2553	
0.25	2595	
0.50	2634	
1	2684	
2	2752	
4	2818	
5	2841	
6	2860	
7	2877	
24	3045	
143	3336	
246	3493	
365	3662	
414	3727	
527	3872	

Recovery

0	1493	Load off
0.5	1299	
1	1251	
2	1207	
3	1189	

Test: Creep
 Orient: +45°
 Spec. No: H16-5
 Temp: 260°F (127°C)
 Stress: 5.63 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	2437	
0.017	2448	
0.10	2567	
0.25	2631	
0.50	2696	
1	2765	
2	2859	
4	2861	
5	2993	
6	3027	
7	3054	
24	3310	
143	3858	
246	4186	
365	4545	
414	4655	
527	4959	

Recovery

0	2517	Load off
0.5	2309	
1	2259	
2	2204	
3	2171	

HYE 2034D

[illegible]

Test: <u>Creep</u>		
Orient: <u>+45°</u>		
Spec. No: <u>H12-10</u>		
Temp: <u>350°F (177°C)</u>		
Stress: <u>5.25 ksi 60 % ult.</u>		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	3203	
0.017	3361	
0.10	3716	
0.25	4155	
0.50	4548	
1	5123	
3	6313	
4	6936	
5	7549	
6	8195	
24	22391	
114	---	failure
Recovery		

[illegible]

HVE 2034D

[illegible][illegible][illegible]

HYE 2034D

[illegible][illegible][illegible]

HYE 2034D

[illegible][illegible][illegible]

HYE 2034D

[illegible][illegible][illegible]

HVE 2034D

[illegible][illegible][illegible]

HyE 2034D

[illegible]

Test: <u>Creep</u>		
Orient: <u>0/+45/90°</u>		
Spec. No: <u>H24-6</u>		
Temp: <u>260°F(127°C)</u>		
Stress: <u>60.0 ksi</u> <u>72 %</u> ult.		
Elap. Time (hrs.)	Accum. Strain (μin/in)	Remarks
0	1970	tab slipped
0.017	1962	
0.10	1962	
0.25	2036	
0.50	2051	
1	2051	
2	2045	
4	2042	
5	2042	
6	2037	
7	2033	
21	failure	
Recovery		

[illegible]

HYE 2034D

[illegible][illegible][illegible]

HVE 20340

[illegible][illegible][illegible]

HYE 2034D

[illegible][illegible][illegible]

HVE 2034D

[illegible][illegible][illegible]

HYE 2034D

[illegible][illegible][illegible]

V378A

Test: Creep
 Orient: +45°
 Spec. No: I3-4
 Temp: 72°F (22°C)
 Stress: 16.93 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	8762	
0.017	9276	
0.10	9913	
0.25	10265	
0.50	10514	
1	10807	
2	11130	
3	11333	
5	11628	
7	11949	
8	11942	
24	12554	
73	13428	
144	14323	
223	14850	
413	15549	
503	15644	

Recovery

0 gage failed on unloading

Test: Creep
 Orient: +45°
 Spec. No: I4-10
 Temp: 72°F (22°C)
 Stress: 16.93 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	8152	
0.017	8560	
0.10	9137	
0.25	9423	
0.50	9691	
1	10065	
2	10372	
3	10564	
5	10741	
6.5	10872	
7.5	10995	
8	11031	
24	11807	
84	failure	

Recovery

Test: Creep
 Orient: +45°
 Spec. No: I7-8
 Temp: 72°F (22°C)
 Stress: 16.93 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	9010	
0.017	9428	
0.10	10024	
0.25	10350	
0.50	10590	
1	10876	
2	11189	
3	11385	
5	11676	
7	11827	
8	11910	
24	12515	
73	13368	
144	14257	
223	14752	
413	15413	
503	15510	

Recovery

0 7103 load off
 0.5 6081
 1 5387
 2 5067
 3 4864

V378A

[illegible][illegible][illegible]

Test: Creep
Orient: +45°
Spec. No: I3-7
Temp: 72°F (22°C)
Stress: 12.77 ksi 60% ult.

[illegible]

Test: Creep
Orient: +45°
Spec. No: I6-3
Temp: 72°F (22°C)
Stress: 12.77 ksi 60% ult.

[illegible]

Test: Creep
Orient: +45°
Spec. No: 18-1
Temp: 72°F (22°C)
Stress 12.77 ksi 60% ult.

[illegible]

V378A

[illegible][illegible][illegible]

V378A

[illegible]

Test: <u>Creep</u>		
Orient: <u>+45°</u>		
Spec. No: <u>I4-8</u>		
Temp: <u>350°F (177°C)</u>		
Stress: <u>9.67 ksi</u> <u>60 %</u> ult.		
Elap. Time (hrs.)	Accum. Strain (Min/in)	Remarks
0	5188	
0.017	5588	
0.10	5918	
0.25	6153	
0.50	6310	
1	6526	
4	7127	
6	7406	
7	7501	
8	7568	
30	8673	
120	10282	
242	11046	
320	11600	
456	12769	
476	12967	
510	13172	
Recovery		
0	8565	load off
0.5	7925	
1	7839	
1.5	7781	

[illegible]

V379A

[illegible][illegible][illegible]

[illegible][illegible][illegible]

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U378A

[illegible][illegible][illegible]

V378A

[illegible][illegible][illegible]

V378A

[illegible][illegible]

Test: <u>Creep</u>		
Orient: <u>0/+45/90°</u>		
Spec. No: <u>I40-5</u>		
Temp: <u>350°F (177°C)</u>		
Stress <u>84.86 ksi</u> <u>60%</u> ult.		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	7312	
0.017	7361	
0.10	7403	
0.25	7424	
0.50	7441	
1	7447	
2	7459	
4	7464	
5	7467	
6	7470	
7	7474	
26	7497	
145	7472	
222	7471	
295	7522	
361	7489	
455	7534	
530	7569	
Recovery		
0	364	load off
0.5	328	
1	322	
4	320	
5	316	

V378A

[illegible][illegible][illegible]

HvE 1076J

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Test: Creep
Orient: +45°
Spec. No: J7-2
Temp: 72°F (22°C)
Stress: 17.83 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6830	
0.017	7362	
0.10	7726	
0.25	7925	
0.50	8096	
1	8260	
3	8576	
4	8656	
5	8690	
6	8748	
46	9193	
142	9618	
240	9938	
310	10158	
407	10330	
504	10664	

Recovery

0	3212	load off
0.5	2502	
1	2082	
2	1874	
3	1804	

HyE 1076J
Test: Creep
Orient: +45°
Spec. No: J7-8
Temp: 72°F (22°C)
Stress: 17.83 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6470	
0.017	6718	
0.10	6984	
0.25	7134	
0.50	7251	
1	7388	
3	7624	
4	7692	
5	7712	
6	7760	
46	8108	
142	8480	
240	8718	
310	8873	
407	8996	
504	9242	

Recovery

0	2386	load off
0.5	1678	
1	1539	
2	1382	
3	1328	

Test: Creep
Orient: +45°
Spec. No: J10-3
Temp: 72°F (22°C)
Stress: 17.83 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6126	
0.017	6318	
0.10	6545	
0.25	6684	
0.50	6801	
1	6922	
3	7146	
4	7208	
5	7225	
6	7268	
46	7600	
142	7926	
240	8118	
310	8258	
407	8370	
504	8586	

Recovery

0	2107	load off
0.5	1494	
1	1374	
2	1230	
3	1172	

NyE 1076J

Test: Creep
Orient: +45°
Spec. No: J12-3
Temp: 72°F (22°C)
Stress: 15.60 ksi 70% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6229	
0.017	6370	
0.10	6586	
0.25	6716	
0.50	6806	
1	6900	
2	6996	
4	7094	
6	7142	
8	7172	
24	7395	
176	7732	
272	7881	
390	7996	
508	8115	

Recovery

0	1907	Load off
0.5	1084	
1	1014	
2	944	
3	879	

Test: Creep
Orient: +45°
Spec. No: J8-8
Temp: 72°F (22°C)
Stress: 15.60 ksi 70% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6334	
0.017	6728	
0.10	6914	
0.25	7065	
0.50	7166	
1	7268	
2	7387	
4	7490	
6	7546	
8	7580	
24	7828	
176	8220	
272	8391	
390	8528	
508	8664	

Recovery

0	2138	Load off
0.5	1352	
1	1268	
2	1193	
3	1114	

Test: Creep
Orient: +45°
Spec. No: J9-3
Temp: 72°F (22°C)
Stress: 15.60 ksi 70% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6018	
0.017	6240	
0.10	6426	
0.25	6555	
0.50	6644	
1	6737	
2	6831	
4	6928	
6	6978	
8	7006	
24	7222	
176	7554	
272	7703	
390	7807	
508	7923	

Recovery

0	1840	Load off
0.5	1122	
1	1053	
2	985	
3	918	

HYE 1076J

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HyE 1076J

[illegible][illegible]

Test:		Creep
Orient:	<u>+45°</u>	
Spec. No:	<u>J9-10</u>	
Temp:	<u>260°F (127°C)</u>	
Stress <u>11.55 ksi</u> <u>70%</u> ult.		
Elap. Time (hrs.)	Accum. Strain ($\mu\text{in/in}$)	Remarks
0	5038	
0.017	5315	
0.10	5560	
0.25	5713	
0.50	5853	
1	6000	
2	6162	
3	6316	
4	6386	
5	6409	
25	6918	
100	7567	
174	7991	
246	8327	
270	8403	
395	8836	
446	9016	
508	9202	
Recovery		
0	4463	Load off
0.5	3754	
1	3641	
2	3511	
3	3437	

HYE 1076J

Test: <u>Creep</u>		
Orient: <u>+45°</u>		
Spec. No: <u>J6-3</u>		
Temp: <u>260°F (127°C)</u>		
Stress: <u>9.30 ksi</u> <u>60 %</u> ult.		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	4754	
0.017	3107	
0.10	5592	
0.25	5691	
0.50	5728	
1	5768	
2	5832	
3	5870	
25	6114	
122	6448	
219	6657	
337	6846	
456	7044	
504	7101	
Recovery		
0	3021	Load off
0.5	2722	
1	2660	
2	2590	
3	2546	

[illegible][illegible]

HyE 1075J

[illegible][illegible][illegible]

Test: Creep
Orient: +45°
Spec. No: J3-8
Temp: 350°F (177°C)
Stress: 11.62 ksi 70% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	10676	
0.017	11179	
0.10	12510	
0.25	13308	
0.50	13813	
1	14531	
2	11002	
24	12677	
146	19627	
234	18960	
360	19330	
502	19410	

0	15759	Load off
0.5	15588	
1	15556	
2	15525	
3	15466	

Test: Creep
Orient: +45°
Spec. No: J4-7
Temp: 350°F (177°C)
Stress: 11.62 ksi 70 % ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	9641	
0.017	10195	
0.10	10942	
0.25	12141	
0.50	13052	
1	13815	
2	14531	
24	21027	
146	gage failed	
502	no failure	

Test: Creep
Orient: +45°
Spec. No: J10-9
Temp: 350°F (177°C)
Stress 11.62 ksi 70% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	11268	
0.017	11859	
0.10	13032	
0.25	14192	
0.50	14966	
1	16099	
2	16729	
24	gage failed	
502	no failure	

HYE 1076J

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HyE 1076J

[illegible][illegible][illegible]

HVE 1076J

Test: Creep
 Orient: 0/+45/90°
 Spec. No: J22-8
 Temp: 72°F(22°C)
 Stress: 70.09 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	5573	
0.017	5593	
0.10	5620	
0.25	5627	
0.50	5633	
1	5634	
2	5631	
3	5627	
68	5577	
170	5655	
236	5673	
331	5688	
427	5663	
570	5691	

Recovery

0	143	load off
0.5	111	
1	108	
2	97	

3 92

Test: Creep
 Orient: 0/+45/90°
 Spec. No: J13-10
 Temp: 72°F(22°C)
 Stress: 70.09 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6030	
0.017	6053	
0.10	6074	
0.25	6082	
0.50	6088	
1	6094	
2	6097	
3	6094	
79	6079	
170	6166	
236	6184	
331	6202	
427	6177	
571	6214	

Recovery

0	207	load off
0.5	164	
1	155	
2	146	

3 140

Test: Creep
 Orient: 0/+45/90°
 Spec. No: J20-10
 Temp: 72°F(22°C)
 Stress: 70.09 ksi 60% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6826	
0.017	6868	
0.10	6890	
0.25	6904	
0.50	6915	
1	6921	
2	6933	
3	6934	
24	6957	
123	6988	
259	7028	
363	7056	
435	7070	
500	7080	

Recovery

0	254	
0.5	217	
1	207	
5	192	

HyE 1076J

Test: Creep
Orient: 0/+45/90°
Spec. No: J15-7
Temp: 260°F(127°C)
Stress: 96.06 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	7702	
0.017	7710	
0.10	7694	
0.25	7700	
0.50	7692	
1	7693	
30	7654	
100	7627	
130.4	failed	

Recovery

Test: Creep
Orient: 0/+45/90°
Spec. No: J16-9
Temp: 260°F(127°C)
Stress: 96.06 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6433	
0.017	6435	
0.10	6435	
0.25	6425	
0.50	6423	
1	6415	
100	6401	
218	6411	
313	6423	
493	6432	
506	6436	

Recovery

0	-230	load off
0.5	-230	
1	-204	
2	-206	
3	-182	

Test: Creep
Orient: 0/+45/90°
Spec. No: J16-10
Temp: 260°F(127°C)
Stress: 96.06 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	8159	
0.017	8163	
0.10	8170	
0.25	8179	
0.50	8181	
1	8183	
30	8203	
100	8220	
130.4	failed	

Recovery

HyE 1076J

[illegible][illegible][illegible]

Test: Creep
Orient: 0/+45/90°
Spec. No: J14-9
Temp: 260°F (127°C)
Stress: 72.04 ksi 60 % ult.

[illegible]

Test: Crimp
Orient: 0/+45/90°
Spec. No: J14-10
Temp: 260°F (127°C)
Stress: 72.04 ksi 60% ult.

[illegible]

Test: Crimp
Orient: 0/+45/90°
Spec. No: J14-8
Temp: 260°F(127°C)
Stress 72.04 ksi @ 60 % ult.

[illegible]

Test: Creep
Orient: 0/+45/90°
Spec. No: J20-7
Temp: 350°F (177°C)
Stress: 94.49 ksi @ 80 % ult.

[illegible]

Test: Creep
Orient: 0/+45/90°
Spec. No: J17-8
Temp: 350°F (177°C)
Stress: 94.49 ksi 80% ult.

[illegible]

Test: Creep
Orient: 0/+45/90°
Spec. No: J21-7
Temp: 350°F(177°C)
Stress 94.49 ksi 80% ult.

[illegible]

NyE 1076J

[illegible][illegible][illegible]

6535-1

[illegible][illegible][illegible]

Test: Creep
Orient: +45°
Spec. No: K8-6
Temp: 72°F (22°C)
Stress: 11.57 ksi 70% ult.

[illegible]

Test: Creep
Orient: +45°
Spec. No: K10-9
Temp: 72°F (22°C)
Stress: 11.57 ksi 70% ult.

[illegible]

Test: Creep
Orient: +45°
Spec. No: K11-6
Temp: 72°F (22°C)
Stress 11.57 ksi 70 % ult.

[illegible]

6535-1

[illegible][illegible][illegible]

6535-1

[illegible][illegible][illegible]

6535-1

[illegible][illegible][illegible]

6535-1

[illegible][illegible][illegible]

6535-1

Test:	<u>Creep</u>	
Orient:	<u>+45°</u>	
Spec. No:	<u>K3-1</u>	
Temp:	<u>350°F (177°C)</u>	
Stress: <u>11,54 ksi 70% ult.</u>		
Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	5574	
0.017	6329	
0.10	7338	
0.25	8092	
0.50	8571	
1	9198	
2	9869	
3	10402	
5.5	11136	
7	11456	
8	11687	
31	14284	
79	16567	
144	18440	
247	20764	
315	22307	
415	23965	
504	25513	
Recovery		
0	20250	load off
0.5	17465	
1	16962	
3	16385	
5	15865	

[illegible][illegible]

6535-1

[illegible][illegible][illegible]

6535-1

[illegible][illegible][illegible]

6535-1

Test: Creep
 Orient: See below
 Spec. No: K24-4
 Temp: 72°F(22°C)
 Stress: 72.70 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6278	
0.017	6302	
0.10	6316	
0.25	6323	
0.50	6327	
1	6330	
3	6335	
5	6335	
6	6335	
71	6366	
175	6382	
240	6404	
342	6399	
406	6420	
502	6426	

Recovery

0	158	load off
0.5	122	
1	115	
2	102	

[0,+45,-45,0,0,-45,-45,0,90,0]_s

Test: Creep
 Orient: See below
 Spec. No: K26-2
 Temp: 72°F(22°C)
 Stress: 72.70 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	failure on loading	

Recovery

Test: Creep
 Orient: See below
 Spec. No: K24-8
 Temp: 72°F(22°C)
 Stress: 72.70 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6253	
0.017	6380	
0.10	6401	
0.25	6410	
0.50	6418	
1	6423	
2	6428	
25	6452	
91	6478	
194	6490	
260	6514	
362	6511	
427	6534	
501	6532	

Recovery

0	237	load off
0.5	193	
1	188	
3	183	
4	177	

6535-1

[illegible][illegible][illegible] $[0, +45, -45, 0, 0, -45, +45, 0, 90, 0]_s$

6535-1

[illegible][illegible][illegible]
$$\{0, +45, -45, 0, 0, -45, +45, 0\}.$$

6535-1

Test: Creep
 Orient: See below
 Spec. No: K34-7
 Temp: 72°F (22°C)
 Stress: 64.07 ksi 70.5 ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	5596	
0.017	5614	
0.10	5632	
0.25	5642	
0.50	5650	
1	5653	
2	5658	
4	5670	
5	5664	
7	5664	
25	5683	
103	5686	
271	5710	
367	5704	
438	5706	
510	5707	

Recovery

0	60	load off
0.5	31	
1	25	
2	21	

Test: Creep
 Orient: See below
 Spec. No: K35-10
 Temp: 72°F (22°C)
 Stress: 64.07 ksi 70.5 ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	5717	
0.017	5746	
0.10	5767	
0.25	5780	
0.50	5786	
1	5792	
2	5797	
4	5808	
5	5806	
7	5802	
30	5818	
103	5828	
271	5851	
367	5836	
438	5837	
510	5838	

Recovery

0	94	load off
0.5	53	
1	47	
2	40	

Test: Creep
 Orient: See below
 Spec. No: K36-6
 Temp: 72°F (22°C)
 Stress: 64.07 ksi 70.5 ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	5604	
0.017	5782	
0.10	5816	
0.25	5826	
0.50	5833	
1	5839	
2	5844	
4	5852	
5	5852	
7	5848	
30	5862	
103	5872	
271	5897	
367	5882	
438	5884	
510	5885	

Recovery

0	137	load off
0.5	90	
1	80	
2	75	

[0,+45,-45,0,0,-45,+45,0]₄

6535-1

Test: Creep
 Orient: See below
 Spec. No: K38-4
 Temp: 72°F(22°C)
 Stress: 77.83 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6404	
0.017	6422	
0.10	6437	
0.25	6443	
0.50	6448	
1	6453	
2	6460	
3	6456	
48	6482	
125	6492	
219	6501	
265	6475	
461	6482	
487	6502	
506	6462	

Recovery

0	73	load off
0.5	39	
1	39	
2	39	

Test: Creep
 Orient: See below
 Spec. No: K39-5
 Temp: 72°F(22°C)
 Stress: 77.83 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0		failure on loading

Recovery

0		
0.5		
1		
2		

Test: Creep
 Orient: See below
 Spec. No: K37-10
 Temp: 72°F(22°C)
 Stress: 77.83 ksi 80% ult.

Elap. Time (hrs.)	Accum. Strain (μ in/in)	Remarks
0	6488	
0.017	6506	
0.10	6522	
0.25	6530	
0.50	6537	
1	6542	
3	6552	
4	6556	
5	6556	
51	6579	
127	6592	
222	6606	
342	6583	
464	6588	
481	6606	
505	6574	

Recovery

0	117	
0.5	60	
1	56	
2	60	

[0.90, -45, -45, 0.0, -45, +45, 0.0]s

Test: Creep
Orient: See below
Spec. No: K38-7
Temp: 72°F (22°C)
~~Stress:~~ 68.10 ksi 70% ult.

[illegible]
$$[0, 90, +45, -45, 0, 0, -45, +45, 0, 0]_S$$

Test: CARD
Orient: See below
Spec. No: K39-3
Temp: 72°F (22°C)
Stress: 68.10 ksi 70% ult.

[illegible]

Test: Creep
Orient: See below
Spec. No: K37-5
Temp: 72°F (22°C)
Stress 68.10 ksi 70% ult.

[illegible]

APPENDIX K
THERMAL EXPANSION DATA

All of the thermal expansion data generated during this program are presented in this appendix. In addition, a typical thermal expansion curve is included at the end of the section. The procedure for computing coefficient of thermal expansion from such a curve is detailed in Paragraph 3.5.10. These data are summarized in Paragraphs 4.1 through 4.6.

Test: Coefficient of Thermal Expansion				
Materials: T300/AFR800				
Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10^{-6} in/in-°F)	Remarks
FB1-5	0°	-67	-0.083	
FB2-6	0°	-67	-0.036	
FB3-3	0°	-67	-0.135	
Avg.			-0.085	
FB1-7	0°	72	-0.358	
FB2-4	0°	72	-0.352	
FB3-4	0°	72	-0.403	
Avg.			-0.371	
FB1-1	0°	260	-0.130	
FB2-1	0°	260	-0.125	
FB3-1	0°	260	-0.155	
Avg.			-0.137	
FB1-4	0°	350	-0.109	
FB2-2	0°	350	-0.327	
FB3-2	0°	350	-0.170	
Avg.			-0.202	
FA1-6	90°	-67	12.18	
FA1-8	90°	-67	11.96	
FA2-4	90°	-67	14.47	
Avg.			12.87	
FA1-7	90°	72	13.60	
FA1-9	90°	72	13.32	
FA2-5	90°	72	13.72	
Avg.			13.55	

Test: Coefficient of Thermal Expansion

Materials: T300/APR800

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10^{-6} in/in-°F)	Remarks
FA1-1	90°	260	12.85	
FA1-3	90°	260	14.79	
FA2-3	90°	260	15.70	
Avg.			14.45	
FA1-2	90°	350	17.03	
FA1-5	90°	350	17.38	
FA2-2	90°	350	16.31	
Avg.			16.91	
FC1-3	±45°	-67	2.378	
FC2-3	±45°	-67	2.905	
FC3-3	±45°	-67	2.599	
Avg.			2.627	
FC1-4	±45°	72	2.440	
FC2-4	±45°	72	2.732	
FC3-4	±45°	72	2.171	
Avg.			2.448	
FC1-1	±45°	260	2.939	
FC2-1	±45°	260	2.988	
FC3-1	±45°	260	2.508	
Avg.			2.812	
FC1-2	±45°	350	3.416	
FC2-2	±45°	350	3.529	
FC3-2	±45°	350	2.768	
Avg.			3.238	

Test: Coefficient of Thermal Expansion				
Materials: SiC/5506				
Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10 ⁻⁶ in/in-°F)	Remarks
G10-A	0°	-67	1.38	
G10-B	0°	-67	1.34	
G10-C	0°	-67	1.29	
Avg.			1.34	
G10-A	0°	72	1.28	
G10-B	0°	72	1.52	
G10-C	0°	72	1.47	
Avg.			1.56	
G10-A	0°	260	2.34	
G10-B	0°	260	1.76	
G10-C	0°	260	1.92	
Avg.			2.01	
G10-A	0°	350	2.70	
G10-B	0°	350	2.12	
G10-C	0°	350	1.88	
Avg.			2.23	
G10-D	90°	-67	7.78	
G10-E	90°	-67	8.11	
G10-F	90°	-67	7.78	
Avg.			7.89	
G10-D	90°	72	9.61	
G10-E	90°	72	9.67	
G10-F	90°	72	9.39	
Avg.			9.56	

Test: Coefficient of Thermal Expansion

Materials: SiC/5506

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10 ⁻⁶ in/in-°F)	Remarks
G10-D	90°	260	19.4	
G10-E	90°	260	20.2	
G10-F	90°	260	16.9	
Avg.			18.8	
G10-D	90°	350	38.2	
G10-E	90°	350	41.4	
G10-F	90°	350	33.9	
Avg.			37.8	
G15-A	±45°	-67	2.86	
G15-B	±45°	-67	2.92	
G17-A	±45°	-67	2.73	
Avg.			2.83	
G15-A	±45°	72	3.31	
G15-B	±45°	72	3.47	
G17-A	±45°	72	3.22	
Avg.			3.33	
G15-A	±45°	260	3.56	
G15-B	±45°	260	4.10	
G17-C	±45°	260	2.89	
Avg.			3.52	
G15-A	±45°	350	4.12	
G15-B	±45°	350	5.14	
G17-A	±45°	350	2.94	
Avg.			4.07	

Test: Coefficient of Thermal Expansion

Materials: HyE 2034D

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10^{-6} in/in-°F)	Remarks
H32-2	0°	-67	-1.00	
H32-3	0°	-67	-1.29	
H32-1	0°	-67	-1.38	
Avg.			-1.22	
H32-2	0°	72	-1.55	
H32-3	0°	72	-1.36	
H32-1	0°	72	-1.70	
Avg.			-1.54	
H32-1	0°	260	-1.62	
H32-2	0°	260	-1.65	
H32-3	0°	260	-1.57	
Avg.			-1.61	
H32-1	0°	350	-1.43	
H32-2	0°	350	-1.92	
H32-3	0°	350	-2.48	
Avg.			-1.94	
H32-4	90°	-67	26.5	
H32-5	90°	-67	26.6	
H32-6	90°	-67	28.2	
Avg.			27.1	
H32-4	90°	72	32.0	
H32-5	90°	72	29.6	
H32-6	90°	72	30.3	
Avg.			30.6	

Test: Coefficient of Thermal Expansion

Materials: HVE 2034D

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10 ⁻⁶ in/in-°F)	Remarks
H32-4	90°	260	39.4	
H32-5	90°	260	37.1	
H32-6	90°	260	42.2	
Avg.			39.6	
H32-4	90°	350	58.7	
H32-5	90°	350	54.7	
H32-6	90°	350	59.9	
Avg.			57.8	
H34-1	45°	-67	-0.463	
H34-2	45°	-67	-0.320	
H34-3	45°	-67	-0.0127	
Avg.			-0.265	
H34-1	45°	72	-0.517	
H34-2	45°	72	-0.475	
H34-3	45°	72	-0.221	
Avg.			-0.404	
H34-1	45°	260	-0.557	
H34-2	45°	260	-0.694	
H34-3	45°	260	-0.662	
Avg.			-0.638	
H34-1	45°	350	-0.674	
H34-2	45°	350	-0.923	
H34-3	45°	350	-1.06	
Avg.			-0.886	

Test: Coefficient of Thermal Expansion

Materials: T300/V378A

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10^{-6} in/in-°F)	Remarks
I43-1	0°	-67	0.145	
I43-2	0°	-67	0.099	
I43-3	0°	-67	0.415	
Avg.			0.217	
I43-1	0°	72	-0.101	
I43-2	0°	72	-0.162	
I43-3	0°	72	-0.556	
Avg.			-0.273	
I43-1	0°	350	-0.108	
I43-2	0°	350	-0.219	
I43-3	0°	350	-0.281	
Avg.			-0.203	
I43-1	0°	450	-0.148	
I43-2	0°	450	-0.217	
I43-3	0°	450	-0.370	
Avg.			-0.245	
I44-1	45°	-67	4.27	
I44-2	45°	-67	3.80	
I44-3	45°	-67	3.86	
Avg.			3.98	
I44-1	45°	72	2.96	
I44-2	45°	72	2.84	
I44-3	45°	72	3.12	
Avg.			2.97	

Test: Coefficient of Thermal Expansion

Materials: T300/V378A

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10^{-6} in/in-°F)	Remarks
I44-1	45°	350	4.00	
I44-2	45°	350	2.89	
I44-3	45°	350	4.49	
Avg.			3.79	
I44-1	45°	450	3.86	
I44-2	45°	450	2.63	
I44-3	45°	450	4.65	
Avg.			3.71	
I43-4	90°	-67	29.5	
I43-5	90°	-67	29.9	
I43-6	90°	-67	25.9	
Avg.			28.4	
I43-4	90°	72	32.0	
I43-5	90°	72	33.0	
I43-6	90°	72	28.5	
Avg.			31.2	
I43-4	90°	350	42.6	
I43-5	90°	350	40.4	
I43-6	90°	350	40.6	
Avg.			41.1	
I43-4	90°	450	43.6	
I43-5	90°	450	42.1	
I43-6	90°	450	42.3	
Avg.			42.7	

Test: Coefficient of Thermal Expansion

Materials: HyE 1076J

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10 ⁻⁶ in/in-°F)	Remarks
1	0°	-67	0.152	
2	0°	-67	0.120	
3	0°	-67	0.180	
Avg.			0.151	
1	0°	72	-0.560	
2	0°	72	-0.578	
3	0°	72	-0.475	
Avg.			-0.538	
1	0°	260	-0.365	
2	0°	260	-0.486	
3	0°	260	-0.457	
Avg.			-0.436	
1	0°	350	-0.288	
2	0°	350	-0.492	
3	0°	350	-0.180	
Avg.			-0.320	
1	90°	-67	21.9	
2	90°	-67	22.4	
3	90°	-67	22.2	
Avg.			22.2	
4	90°	72	23.8	
5	90°	72	25.2	
6	90°	72	24.3	
Avg.			24.4	

Test: Coefficient of Thermal Expansion

Materials: HyE 1076J

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10 ⁻⁶ in/in-°F)	Remarks
4	90°	260	31.2	
5	90°	260	31.4	
6	90°	260	31.6	
Avg.			31.4	
4	90°	350	34.7	
5	90°	350	35.0	
6	90°	350	34.2	
Avg.			34.6	
1	±45°	-67	3.02	
2	±45°	-67	3.39	
3	±45°	-67	2.85	
Avg.			3.08	
1	±45°	72	2.98	
2	±45°	72	2.44	
3	±45°	72	2.32	
Avg.			2.58	
1	±45°	260	2.41	
2	±45°	260	2.58	
3	±45°	260	2.61	
Avg.			2.53	
1	±45°	350	2.42	
2	±45°	350	2.81	
3	±45°	350	2.78	
Avg.			2.67	

Test: Coefficient of Thermal Expansion

Materials: G-160/6535-1

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Thern. Expansion (10 ⁻⁶ in/in-°F)	Remarks
K20-A	0°	-67	0.17	
K20-B	0°	-67	-0.06	
K20-C	0°	-67	0.15	
Avg.			0.08	
K20-A	0°	72	-0.34	
K20-B	0°	72	-0.41	
K20-C	0°	72	-0.38	
Avg.			-0.37	
K20-A	0°	260	-0.27	
K20-B	0°	260	-0.39	
K20-C	0°	260	-0.48	
Avg.			-0.38	
K20-A	0°	350	-0.15	
K20-B	0°	350	-0.17	
K20-C	0°	350	-0.29	
Avg.			-0.20	
K20-D	90°	-67	23.0	
K20-E	90°	-67	22.0	
K20-F	90°	-67	22.5	
Avg.			22.5	
K20-D	90°	72	24.5	
K20-E	90°	72	24.0	
K20-F	90°	72	25.3	
Avg.			24.8	

Test: Coefficient of Thermal Expansion

Materials: G-160/6535-1

Specimen Number	Fiber Orientation	Temp. Range (°F)	Coeff. Therm. Expansion (10^{-6} in/in-°F)	Remarks
K20-D	90°	260	29.8	
K20-E	90°	260	30.2	
K20-F	90°	260	29.9	
Avg.			30.0	
K20-D	90°	350	33.2	
K20-E	90°	350	31.7	
K20-F	90°	350	32.3	
Avg.			32.4	
K40-A	±45	-67	3.05	
K40-B	±45	-67	2.60	
K40-C	±45	-67	3.13	
Avg.			2.93	
K40-A	±45	72	2.25	
K40-B	±45	72	2.51	
K40-C	±45	72	2.61	
Avg.			2.46	
K40-A	±45	260	2.24	
K40-B	±45	260	2.23	
K40-C	±45	260	2.24	
Avg.			2.24	
K40-A	±45	350	2.88	
K40-B	±45	350	2.55	
K40-C	±45	350	2.19	
Avg.			2.54	

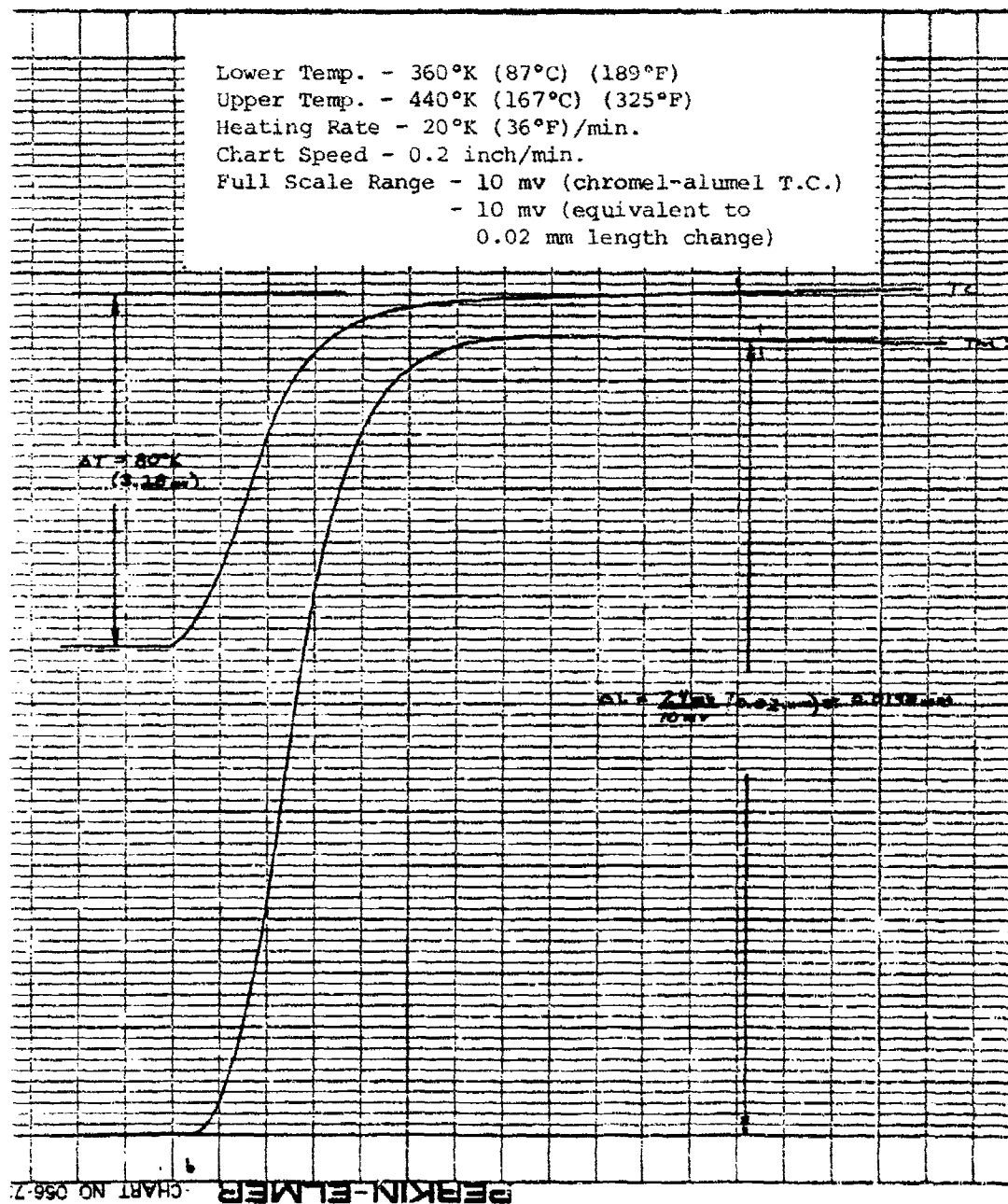


Figure K-1. Thermal Expansion Characteristics of SiC/5506 Composite Laminate; 90° Fiber Direction.

APPENDIX L
SPECIFIC HEAT DATA

All of the specific heat data generated during this program are presented in this section. A typical set of differential scanning calorimeter (DSC) traces, from which specific heat is determined, is included at the end of this section.

The values listed in the succeeding tables were computed according to the following equation:

$$C_p(\text{sample}) = \frac{\text{mass of sapphire std.}}{\text{mass of sample}} \times \frac{D_3 - D_1}{D_2 - D_1} \times C_p(\text{sapphire std.}),$$

where, D_1 , D_2 and D_3 represent the relative displacements of the DSC curves for the empty aluminum pan, sapphire reference, and sample, respectively. For the sample traces included,

$$\begin{aligned} C_p(\text{HyE 1076J, \#1}) &= \frac{8.54\text{gm}}{4.23\text{gm}} \times \frac{12.4 \text{ div} - 17.2 \text{ div}}{10.8 \text{ div} - 17.2 \text{ div}} \times 0.22545 \frac{\text{cal}}{\text{gm-}^\circ\text{K}} \\ &= 0.341 \text{ cal/gm-}^\circ\text{K, or } 0.341 \text{ BTU/lb-}^\circ\text{F} \\ &\quad \text{at } 400^\circ\text{K, or } 260^\circ\text{F.} \end{aligned}$$

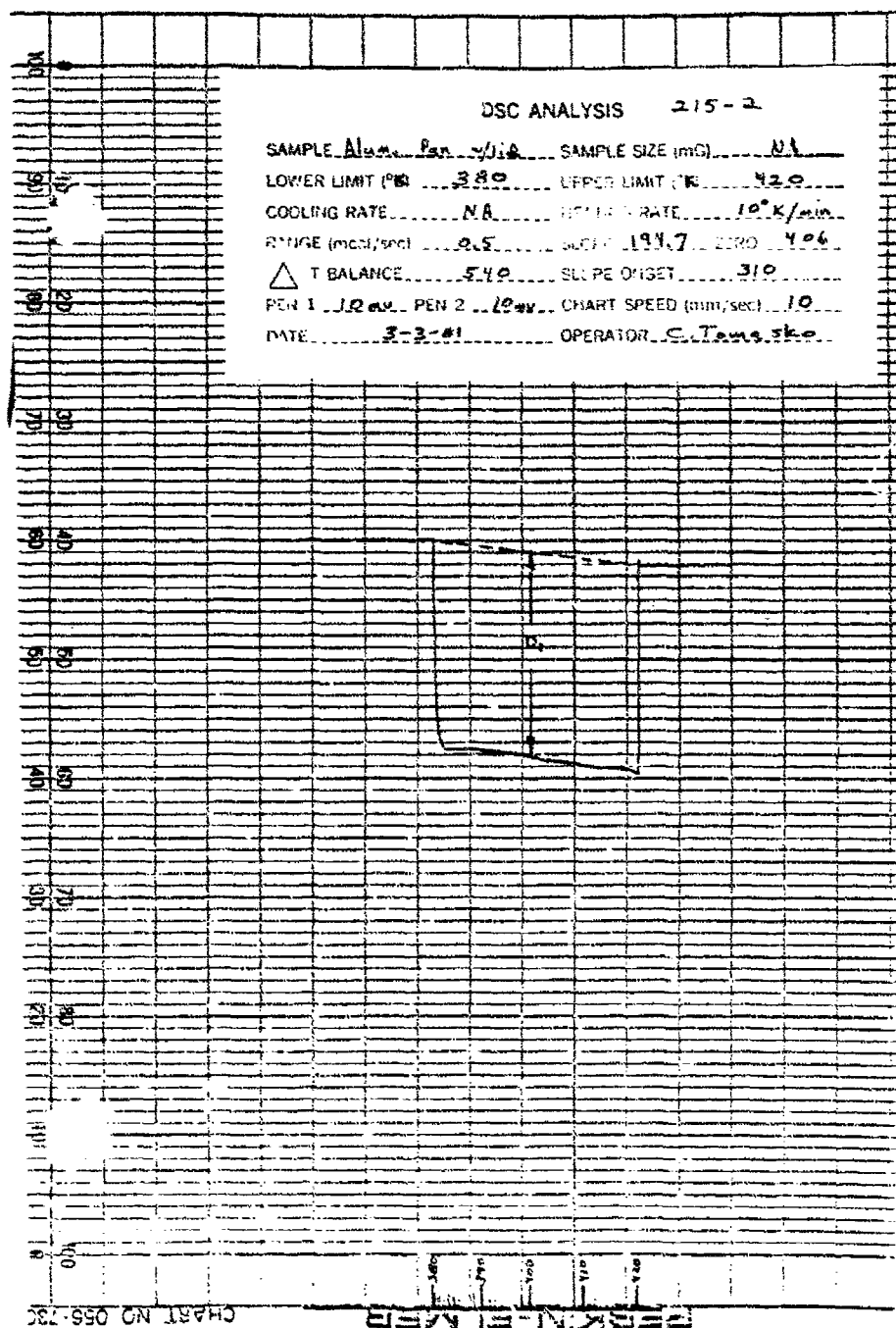


Figure L-1. DSC Analysis of Empty Sample Pan.

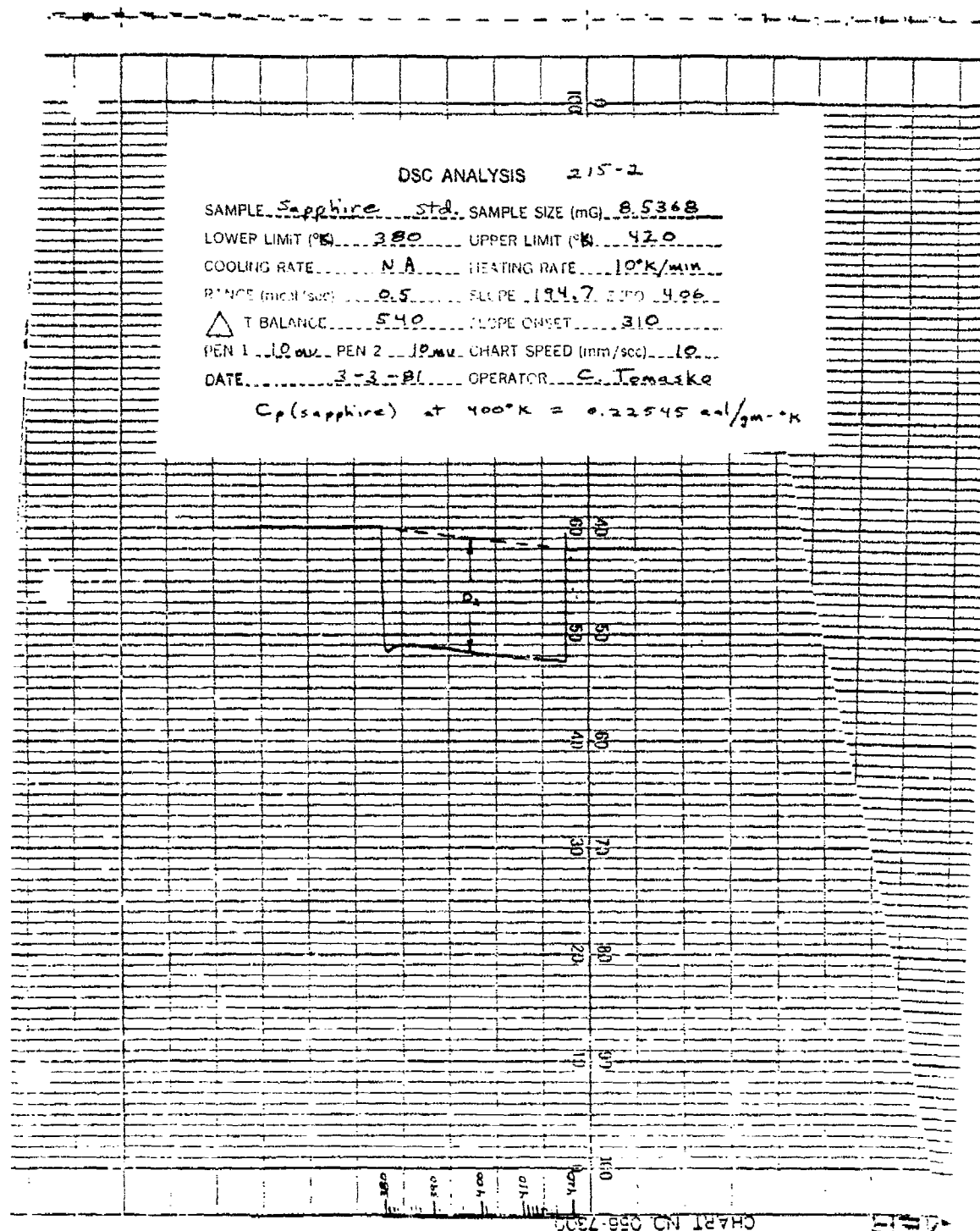


Figure L-2. DSC Analysis of Sapphire Reference Standard.

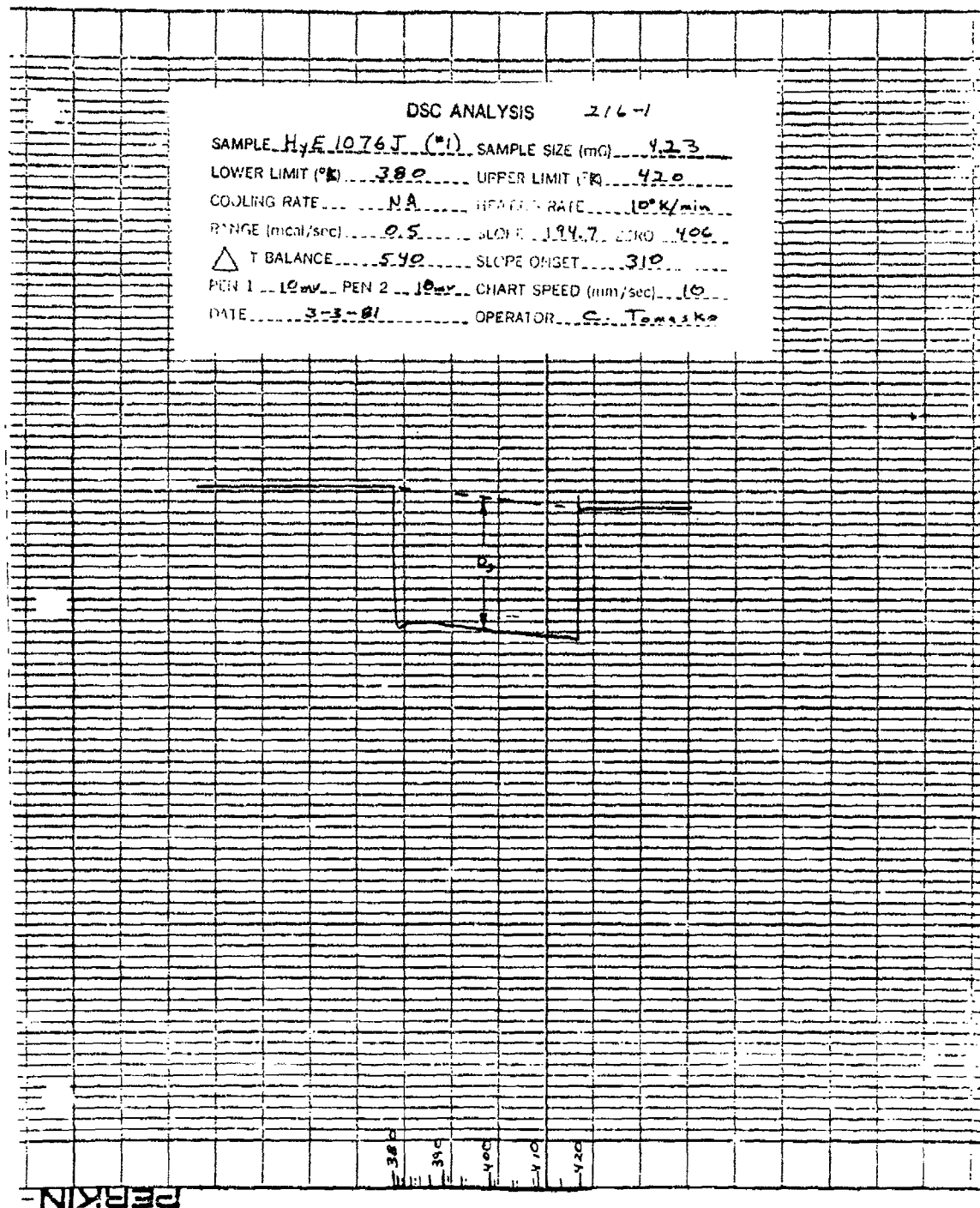


Figure L-3. DSC Analysis of HyE 1076J Graphite/Epoxy Composite Material.

APPENDIX M
THERMAL CONDUCTIVITY DATA

All of the thermal conductivity measurements made during this program are tabulated in this section. The average values presented in Sections 4.1 through 4.6 were taken from linear regression curves drawn through all of the respective data points tabulated here.

Test: Thermal Conductivity**Materials: T300/AFR800**

Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
F37-1	0°	-69	0.295	
F37-1	0°	-30	0.341	
F37-1	0°	56	0.364	
F37-1	0°	60	0.486	
F37-1	0°	65	0.854	
F37-1	0°	67	0.244	
F37-1	0°	70	0.611	
F37-1	0°	74	0.308	
F37-1	0°	77	0.399	
F37-1	0°	81	0.499	
F37-1	0°	82	0.301	
F37-1	0°	85	0.568	
F37-1	0°	91	0.552	
F37-1	0°	93	0.295	
F37-1	0°	96	0.434	
F37-1	0°	100	0.331	
F37-1	0°	101	0.491	
F37-1	0°	106	0.508	
F37-1	0°	112	0.487	
F37-1	0°	117	0.494	
F37-1	0°	118	0.529	
F37-1	0°	125	0.459	
F37-1	0°	130	0.524	
F37-1	0°	136	0.508	
F37-1	0°	136	0.385	
F37-1	0°	145	0.529	
F37-1	0°	150	0.481	
F37-1	0°	160	0.544	
F37-1	0°	164	0.557	
F37-1	0°	222	0.410	

Test: Thermal Conductivity				
Materials: T300/APR800				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
F37-1	0°	235	0.558	
F37-1	0°	291	0.463	
F37-1	0°	325	0.467	
F37-1	0°	350	0.510	
F37-2	0°	-83	0.379	
F37-2	0°	-59	0.375	
F37-2	0°	89	0.564	
F37-2	0°	117	0.486	
F37-2	0°	144	0.536	
F37-2	0°	170	0.502	
F37-2	0°	217	0.551	
F37-2	0°	279	0.515	
F37-2	0°	354	0.643	
F37-3	0°	-75	0.294	
F37-3	0°	-50	0.299	
F37-3	0°	-22	0.306	
F37-3	0°	91	0.494	
F37-3	0°	119	0.383	
F37-3	0°	146	0.424	
F37-3	0°	173	0.431	
F37-3	0°	222	0.443	
F37-3	0°	273	0.479	
F37-3	0°	334	0.503	
F37-3	0°	351	0.500	

Materials: SiC/5506

[illegible]

Materials: HyE 2034D

[illegible]

Test: Thermal Conductivity				
Materials: HVE 2034D				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
H37-1	±45°	99	0.516	
H37-1	±45°	113	0.625	
H37-1	±45°	111	0.507	
H37-1	±45°	146	0.551	
H37-1	±45°	140	0.523	
H37-1	±45°	170	0.607	
H37-1	±45°	170	0.629	
H37-1	±45°	199	0.563	
H37-1	±45°	235	0.594	
H37-1	±45°	231	0.585	
H37-1	±45°	286	0.596	
H37-1	±45°	331	0.584	
H37-1	±45°	339	0.603	
H37-2	±45°	96	0.460	
H37-2	±45°	110	0.601	
H37-2	±45°	138	0.572	
H37-2	±45°	164	0.533	
H37-2	±45°	192	0.576	
H37-2	±45°	228	0.555	
H37-2	±45°	274	0.603	
H37-2	±45°	305	0.638	
H37-2	±45°	366	0.555	
H37-3	±45°	80	0.703	
H37-3	±45°	88	1.417	
H37-3	±45°	91	0.985	
H37-3	±45°	101	1.464	
H37-3	±45°	111	1.44	
H37-3	±45°	125	1.238	
H37-3	±45°	196	0.764	
H37-3	±45°	244	0.613	

Materials: HyE 2034D

[illegible]

Test: Thermal Conductivity				
Materials: T300/V378A				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
I43-1	0°	62	0.331	
I43-1	0°	92	0.363	
I43-1	0°	121	0.372	
I43-1	0°	154	0.384	
I43-1	0°	188	0.397	
I43-1	0°	230	0.410	
I43-1	0°	272	0.440	
I43-1	0°	310	0.452	
I43-1	0°	337	0.457	
I43-2	0°	61	0.305	
I43-2	0°	92	0.335	
I43-2	0°	123	0.346	
I43-2	0°	157	0.331	
I43-2	0°	235	0.396	
I43-2	0°	235	0.398	
I43-2	0°	276	0.399	
I43-2	0°	316	0.408	
I43-2	0°	339	0.419	
I43-3	0°	-51	0.282	
I43-3	0°	-20	0.116	
I43-3	0°	-18	0.244	
I43-3	0°	61	0.370	
I43-3	0°	92	0.365	
I43-3	0°	120	0.395	
I43-3	0°	154	0.399	
I43-3	0°	191	0.356	
I43-3	0°	230	0.424	
I43-3	0°	273	0.467	
I43-3	0°	312	0.436	
I43-3	0°	339	0.462	

Test: Thermal Conductivity				
Materials: T300/V378A				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
I44-1	±45°	-64	0.249	
I44-1	±45°	-39	0.242	
I44-1	±45°	-19	0.249	
I44-1	±45°	72	0.225	
I44-1	±45°	97	0.327	
I44-1	±45°	124	0.328	
I44-1	±45°	121	0.318	
I44-1	±45°	123	0.320	
I44-1	±45°	149	0.329	
I44-1	±45°	195	0.335	
I44-1	±45°	207	0.352	
I44-1	±45°	255	0.354	
I44-1	±45°	280	0.363	
I44-1	±45°	369	0.394	
I44-1	±45°	367	0.287	
I44-1	±45°	412	0.405	
I44-1	±45°	436	0.414	
I44-2	±45°	-82	0.273	
I44-2	±45°	-44	0.351	
I44-2	±45°	18	0.388	
I44-2	±45°	119	0.329	
I44-2	±45°	175	0.347	
I44-2	±45°	255	0.376	
I44-2	±45°	368	0.432	
I44-2	±45°	368	0.426	
I44-2	±45°	435	0.462	

Materials: T300/V378A

[illegible]

Test: Thermal Conductivity				
Materials: HyE 1076J				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
J33-1	±45°	92	0.445	
J33-1	±45°	124	0.507	
J33-1	±45°	145	0.545	
J33-1	±45°	214	0.578	
J33-1	±45°	258	0.570	
J33-1	±45°	311	0.578	
J33-1	±45°	341	0.601	
J33-2	±45°	91	0.297	
J33-2	±45°	116	0.429	
J33-2	±45°	138	0.400	
J33-2	±45°	203	0.417	
J33-2	±45°	248	0.471	
J33-2	±45°	305	0.513	
J33-2	±45°	334	0.453	
J33-3	±45°	93	0.497	
J33-3	±45°	120	0.493	
J33-3	±45°	145	0.460	
J33-3	±45°	208	0.604	
J33-3	±45°	260	0.563	
J33-3	±45°	305	0.572	
J33-3	±45°	343	0.580	
J33-3	±45°	-72	0.226	
J33-3	±45°	-60	0.222	
J33-3	±45°	-51	0.272	
J33-3	±45°	-25	0.273	

Test: Thermal Conductivity				
Materials: HyE 1076J				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
J34-1	0°	-75	0.418	
J34-1	0°	-47	0.397	
J34-1	0°	-26	0.397	
J34-1	0°	91	0.380	
J34-1	0°	111	0.416	
J34-1	0°	141	0.402	
J34-1	0°	211	0.432	
J34-1	0°	278	0.494	
J34-1	0°	324	0.480	
J34-1	0°	335	0.519	
J34-2	0°	95	0.393	
J34-2	0°	109	0.443	
J34-2	0°	139	0.451	
J34-2	0°	187	0.453	
J34-2	0°	234	0.460	
J34-2	0°	263	0.460	
J34-2	0°	308	0.509	
J34-2	0°	333	0.531	
J34-2	0°	343	0.535	
J34-3	0°	91	0.425	
J34-3	0°	128	0.437	
J34-3	0°	138	0.447	
J34-3	0°	205	0.483	
J34-3	0°	269	0.488	
J34-3	0°	312	0.518	
J34-3	0°	327	0.521	

Test: Thermal Conductivity				
Materials: G-160/6535-1				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
K20-1	0°	81	0.397	
K20-1	0°	107	0.421	
K20-1	0°	132	0.458	
K20-1	0°	160	0.466	
K20-1	0°	217	0.509	
K20-1	0°	265	0.517	
K20-1	0°	311	0.509	
K20-1	0°	352	0.531	
K20-2	0°	80	0.437	
K20-2	0°	106	0.450	
K20-2	0°	133	0.456	
K20-2	0°	163	0.496	
K20-2	0°	212	0.511	
K20-2	0°	255	0.580	
K20-2	0°	303	0.743	
K20-2	0°	342	0.619	
K20-3	0°	-25	0.113	
K20-3	0°	-25	0.253	
K20-3	0°	-19	0.208	
K20-3	0°	-3	0.258	
K20-3	0°	85	0.357	
K20-3	0°	111	0.388	
K20-3	0°	133	0.453	
K20-3	0°	164	0.479	
K20-3	0°	217	0.641	
K20-3	0°	267	0.597	
K20-3	0°	312	0.658	
K20-3	0°	347	0.665	

Test: Thermal Conductivity				
Materials: G-160/6535-1				
Specimen Number	Fiber Orientation	Temp. (°F)	Thermal Conductivity (Btu-ft/ft ² -hr-°F)	Remarks
K40-1	±45°	-62	0.395	
K40-1	±45°	-47	0.390	
K40-1	±45°	-21	0.426	
K40-1	±45°	107	0.435	
K40-1	±45°	131	0.457	
K40-1	±45°	161	0.509	
K40-1	±45°	256	0.496	
K40-1	±45°	300	0.659	
K40-1	±45°	345	0.594	
K40-2	±45°	80	0.395	
K40-2	±45°	105	0.449	
K40-2	±45°	133	0.437	
K40-2	±45°	162	0.459	
K40-2	±45°	208	0.468	
K40-2	±45°	252	0.497	
K40-2	±45°	297	0.546	
K40-2	±45°	344	0.516	
K40-3	±45°	81	0.417	
K40-3	±45°	109	0.438	
K40-3	±45°	131	0.447	
K40-3	±45°	174	0.473	
K40-3	±45°	219	0.448	
K40-3	±45°	265	0.454	
K40-3	±45°	311	0.513	
K40-3	±45°	350	0.521	

APPENDIX N
GLASS-TRANSITION TEMPERATURE DATA

The glass-transition temperatures determined for the materials characterized during this program are presented here along with a typical loss-modulus vs. temperature trace, from which the T_g 's are determined by DMA.

GLASS TRANSITION TEMPERATURE

Material	Dry T _g (°F)	Wet ¹ T _g (°F)
T300/AFR800	468	381
SiC/5506	394	293
HyE 2034D	430	342
T300/V378A ²	702	702
HyE 1076J	518	493
G-160/6535-1	507	471

¹Specimen exposed to 160°F (71°C) and 100% R.H. until it reached equilibrium weight gain.

²This material gained weight very rapidly during humidity aging. If it dried just as rapidly also, the specimen may have been completely dry by the end of the test, hence, the wet value indicated may actually have been for a dry material.

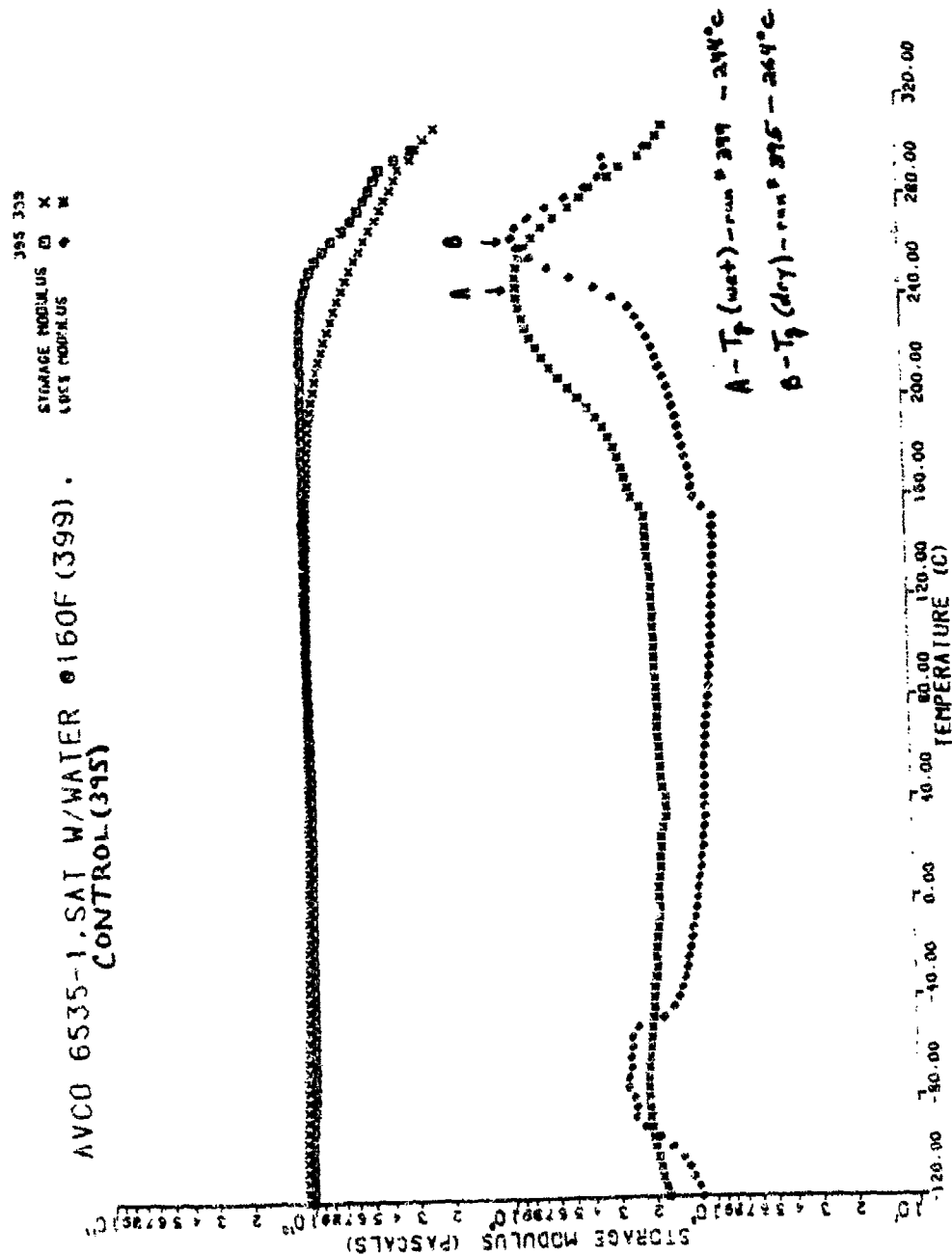


Figure N-1. Dynamic Mechanical Analysis of G-160/6535-1 Graphite/Epoxy Composite Material.

APPENDIX O
HUMIDITY AGED TENSION DATA

All of the tensile data generated during this program on specimens which had been humidity aged at 160°F (71°C) and 100% R.H. are presented in this section. Summaries of these data are tabulated and plotted in the form of stress-strain curves in Sections 4.1 through 4.6.

Test: Tension After Environmental Aging @ 160°F & 100% R.H. Material: T300/AFR800										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mgd. (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ult. Strain (µin/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
F15-2	90°	72	6.37	1.45	1.55	---	4580	196	0.63	50% saturation
F15-8	90°	72	4.22	1.46	1.49	---	3080	196	0.63	50% saturation
F15-10	90°	72	5.60	1.55	1.08	---	4000	196	0.63	50% saturation
F16-5	90°	72	5.60	1.54	0.95	---	3950	196	0.60	50% saturation
F16-10	90°	72	4.85	1.42	3.54	---	3500	196	0.62	50% saturation
Avg.			5.33	1.48	1.72	---	3820		0.62	
Std.Dev.			0.82	0.06	1.05	---	570		0.01	
F14-3	90°	260	2.95	1.62	0.53	---	2680	196	0.40	50% saturation
F15-1	90°	260	2.79	1.40	0.47	---	2600	196	0.62	50% saturation
F15-9	90°	260	3.52	1.50	0.47	---	3380	196	0.63	50% saturation
F16-9	90°	260	3.88	1.54	0.44	---	3750	196	0.61	50% saturation
F17-8	90°	260	3.53	1.70	0.48	---	3180	196	0.65	50% saturation
Avg.			3.31	1.55	0.48	---	3120		0.58	
Std.Dev.			0.48	0.11	0.03	---	480		0.10	
F15-4	90°	72	3.62	1.41	3.62	---	3030	1,416	1.36	100% saturation
F16-7	90°	72	4.03	1.42	4.03	---	2840	1,416	1.26	100% saturation
F17-9	90°	72	3.60	1.41	3.60	---	2560	1,416	1.27	100% saturation
F18-3	90°	72	2.85	1.55	2.84	---	1840	1,416	1.24	100% saturation
Avg.			3.52	1.45	3.52	---	2570		1.28	
Std.Dev.			0.49	0.07	0.49	---	520		0.04	
F14-10	90°	260	1.78	0.91	1.42	---	2190	1,848	1.30	100% saturation
F16-3	90°	260	1.28	1.10	0.95	---	1290	1,848	1.26	100% saturation
F17-3	90°	260	1.47	1.07	1.47	---	1450	1,848	1.27	100% saturation
F18-8	90°	260	1.42	1.01	1.19	---	1440	1,848	1.30	100% saturation
Avg.			1.49	1.02	1.26	---	1590		1.27	
Std.Dev.			0.21	0.08	0.24	---	400		0.04	

Test: Tension After Environmental Aging @ 160°F & 100% R.H. Material: SiC/5506										
Spec. No.	Fiber Orlen.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ult. Strain (in/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
G9-2	90°	72	9.04	2.97	2.69	---	3600	175	0.60	50% saturation
G9-11	90°	72	8.20	3.06	2.25	---	3300	175	0.62	50% saturation
G22-8	90°	72	9.50	2.83	2.42	---	3870	175	0.59	50% saturation
G25-8	90°	72	8.66	3.44	1.65	---	3190	175	0.59	50% saturation
G26-8	90°	72	8.43	3.08	2.29	---	3200	175	0.56	50% saturation
Avg.			8.77	3.08	2.26	---	3420		0.59	
Std.Dev.			0.51	0.23	0.38	---	310		0.02	
G9-10	90°	260	4.27	0.92	1.14	---	8300	175	0.61	50% saturation
G22-4	90°	260	3.98	1.09	0.82	---	8500	175	0.62	50% saturation
G24-6	90°	260	3.78	1.15	0.66	---	7700	175	0.62	50% saturation
G25-2	90°	260	3.77	1.34	0.88	---	6700	175	0.58	50% saturation
G26-6	90°	260	3.29	1.03	0.56	---	7000	175	0.58	50% saturation
Avg.			3.82	1.11	0.81	---	7640		0.60	
Std.Dev.			0.36	0.16	0.22	---	790		0.02	
G9-8	90°	72	5.02	2.37	3.10	---	2380	1,546	1.28	100% saturation
G24-5	90°	72	6.52	2.49	3.10	---	3000	1,546	1.29	100% saturation
G25-7	90°	72	6.81	2.64	2.29	---	2900	1,546	1.23	100% saturation
G26-3	90°	72	6.39	2.52	3.12	---	2910	1,546	1.24	100% saturation
G26-9	90°	72	6.14	2.87	1.30	---	2630	1,546	1.27	100% saturation
Avg.			6.17	2.58	2.58	---	2760		1.26	
Std.Dev.			0.69	0.19	0.90	---	260		0.03	
G9-1	90°	260	2.02	1.08	0.81	---	3680	1,546	1.27	100% saturation
G22-6	90°	260	1.75	0.51	0.64	---	4880	1,546	1.21	100% saturation
G22-7	90°	260	1.89	0.70	0.66	---	4310	1,546	1.23	100% saturation
G24-8	90°	260	1.82	0.47	0.55	---	6100	1,546	1.29	100% saturation
G25-1	90°	260	2.19	1.01	0.72	---	6070	1,546	1.32	100% saturation
Avg.			1.93	0.75	0.68	---	5010		1.26	
Std.Dev.			0.17	0.28	0.10	---	1070		0.04	

Test: Tension After Environmental Aging @ 160°F & 100% R.H. Material: HYE 2034D										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ult. Strain (in/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
H36-8	90°	72	2.67	0.96	0.76	---	2830	216.75	0.79	50% saturation
H36-7	90°	72	2.13	0.90	0.75	---	2400	216.75	0.79	50% saturation
H36-1	90°	72	2.21	0.96	1.15	---	2400	216.75	0.80	50% saturation
H36-4	90°	72	2.85	0.97	1.08	---	3000	216.75	0.79	50% saturation
H36-2	90°	72	2.79	0.96	1.14	---	2960	216.75	0.78	50% saturation
Avg.			2.53	0.95	0.98	---	2720		0.79	
Std.Dev.			0.34	0.03	0.20	---	300		0.01	
H35-2	90°	260	1.89	0.74	0.82	---	2830	216.75	0.77	50% saturation
H35-4	90°	260	1.81	0.67	1.04	---	2920	216.75	0.79	50% saturation
H35-5	90°	260	1.44	0.76	0.62	---	2180	216.75	0.78	50% saturation
H35-6	90°	260	1.69	0.69	0.80	---	2670	216.75	0.80	50% saturation
H36-10	90°	260	1.76	0.71	0.72	---	2690	216.75	0.80	50% saturation
Avg.			1.72	0.71	0.80	---	2660		0.79	
Std.Dev.			0.17	0.04	0.16	---	280		0.01	
H3-8	90°	72	1.65	1.00	1.22	---	1700	982	1.17	100% saturation
H4-1	90°	72	2.25	1.07	1.14	---	2200	982	1.14	100% saturation
H4-6	90°	72	2.38	1.03	1.71	---	2300	982	1.22	100% saturation
H4-7	90°	72	1.87	0.99	1.60	---	2000	982	1.17	100% saturation
H6-5	90°	72	2.09	0.93	1.77	---	2300	982	1.19	100% saturation
Avg.			2.05	1.00	1.49	---	2100	982	1.18	
Std.Dev.			0.29	0.05	0.29	---	260		0.03	
H3-4	90°	260	0.88	0.43	0.88	---	2100	982	1.17	100% saturation
H3-5	90°	260	0.94	0.47	0.94	---	2100	982	1.16	100% saturation
H6-4	90°	260	1.21	0.48	1.01	---	2700	982	1.17	100% saturation
H6-8	90°	260	1.04	0.63	0.82	---	2000	982	1.17	100% saturation
H7-4	90°	260	1.13	0.59	0.80	---	2100	982	1.28	100% saturation
Avg.			1.04	0.52	0.89	---	2200		1.19	
Std.Dev.			0.13	0.09	0.09	---	280		0.05	

Test: Tension After Environmental Aging @ 160°F & 100% R.H. Material: T300/V378A										
Spec. No.	Fiber Orlen.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mpd. (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ult. Strain (µin/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
I15-2	90°	72	5.48	1.31	4.08	---	4100	18	0.75	50% saturation
I18-1	90°	72	6.11	1.39	2.22	---	4600	18	0.74	50% saturation
I19-3	90°	72	6.60	1.32	4.25	---	6200	18	0.79	50% saturation
I20-6	90°	72	4.97	1.28	4.97	---	3800	18	0.81	50% saturation
I21-5	90°	72	4.66	1.27	4.66	---	3600	18	0.80	50% saturation
Avg.			5.56	1.31	4.03	---	4460		0.78	
Std.Dev.			0.80	0.05	1.07	---	1040		0.03	
I15-1	90°	350	3.92	1.16	0.85	---	3800	18	0.72	50% saturation
I18-3	90°	350	4.48	1.17	0.63	---	4700	18	0.79	50% saturation
I19-2	90°	350	4.81	0.96	1.67	---	3900	18	0.83	50% saturation
I20-3	90°	350	3.54	1.08	0.79	---	3700	18	0.78	50% saturation
I21-6	90°	350	2.62	1.07	0.75	---	2700	18	0.81	50% saturation
Avg.			3.87	1.09	0.94	---	3760		0.79	
Std.Dev.			0.86	0.08	0.42	---	710		0.04	
I15-4	90°	72	3.96	1.34	3.54	---	3000	2588	1.76	100% saturation
I15-6	90°	72	3.58	1.30	3.55	---	2700	2588	1.75	100% saturation
I15-7	90°	72	3.81	1.28	3.43	---	2930	2588	1.77	100% saturation
I18-4	90°	72	4.22	1.32	3.45	---	3250	2588	1.76	100% saturation
I18-9	90°	72	3.96	1.30	3.94	---	2970	2588	1.77	100% saturation
Avg.			3.90	1.31	3.58	---	2970		1.76	
Std.Dev.			0.24	0.02	0.21	---	200		0.01	
I18-6	90°	350	0.84	0.94	0.66	---	900	2588	1.77	100% saturation
I19-7	90°	350	0.59	0.78	0.29	---	700	2588	1.75	100% saturation
I20-10	90°	350	0.86	1.10	0.59	---	800	2588	1.64	100% saturation
I21-2	90°	350	0.86	1.15	0.36	---	1000	2588	1.73	100% saturation
I21-3	90°	350	0.78	0.71	0.70	---	800	2588	1.74	100% saturation
Avg.			0.73	0.94	0.52	---	840		1.73	
Std.Dev.			0.11	0.19	0.19	---	110		0.05	

Test: Tension After Environmental Aging @ 160°F & 100% R.H. Material: HyE 1076J										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ult. Strain (in/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
J27-6	90°	72	5.98	1.45	2.43	---	4300	162	0.80	50% saturation
J28-10	90°	72	4.94	1.37	4.94	---	3600	162	0.78	50% saturation
J29-6	90°	72	4.30	1.42	4.30	---	3000	162	0.77	50% saturation
J30-4	90°	72	4.64	1.29	4.64	---	3600	162	0.71	50% saturation
J30-9	90°	72	4.14	1.52	1.15	---	3000	162	0.81	50% saturation
Avg.			4.80	1.41	3.49	---	3500		0.77	
Std. Dev.			0.73	0.09	1.63	---	540		0.04	
J26-9	90°	260	3.63	1.24	2.06	---	3200	162	0.75	50% saturation
J27-4	90°	260	2.47	1.22	0.72	---	2400	162	0.76	50% saturation
J27-7	90°	260	3.13	1.17	0.89	---	3000	162	0.80	50% saturation
J28-6	90°	260	2.58	1.07	1.95	---	2500	162	0.75	50% saturation
J29-9	90°	260	2.74	1.31	0.93	---	2400	162	0.73	50% saturation
Avg.			2.91	1.20	1.31	---	2700		0.76	
Std. Dev.			0.47	0.09	0.64	---	370		0.03	
J26-4	90°	72	4.26	1.49	4.26	---	2800	1,774	1.18	100% saturation
J26-10	90°	72	4.15	1.52	4.15	---	2700	1,774	1.14	100% saturation
J27-5	90°	72	3.80	1.42	2.80	---	2700	1,774	1.17	100% saturation
J28-2	90°	72	3.98	1.30	3.98	---	2900	1,774	1.17	100% saturation
J28-8	90°	72	3.94	1.33	3.94	---	2900	1,774	1.17	100% saturation
Avg.			4.03	1.41	3.83	---	2800		1.17	
Std. Dev.			0.18	0.10	0.59	---	100		0.02	
J26-7	90°	260	1.87	1.20	1.06	---	1600	1,774	1.16	100% saturation
J29-7	90°	260	1.92	1.11	1.37	---	1900	1,774	1.17	100% saturation
J30-1	90°	260	1.21	1.13	0.69	---	1100	1,774	1.15	100% saturation
J30-5	90°	260	1.26	0.88	1.07	---	1500	1,774	1.17	100% saturation
J30-8	90°	260	1.09	0.83	1.09	---	1300	1,774	1.18	100% saturation
Avg.			1.49	1.03	1.05	---	1480		1.17	
Std. Dev.			0.42	0.16	0.24	---	300		0.01	

Test: Tension After Environmental Aging @ 160°F & 100% R.H. Material: G-160/6535-1										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ult. Strain (uin/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
K14-6	90°	72	3.32	1.64	3.32	---	2050	216	0.69	50% saturation
K14-10	90°	72	3.85	1.77	3.85	---	2200	216	0.65	50% saturation
K15-8	90°	72	4.11	1.79	4.11	---	2270	216	0.67	50% saturation
K16-9	90°	72	4.14	1.72	4.14	---	2410	216	0.68	50% saturation
K18-10	90°	72	3.78	1.52	3.78	---	2480	216	0.66	50% saturation
Avg.			3.84	1.69	3.84	---	2280		0.67	
Std.Dev			0.33	0.11	0.33	---	170		0.02	
K16-8	90°	260	1.93	1.78	1.33	---	1150	216	0.67	50% saturation
K17-9	90°	260	2.55	1.61	1.59	---	1700	216	0.70	50% saturation
K15-9	90°	260	2.58	1.52	1.78	---	1750	216	0.68	50% saturation
K45-9	90°	260	2.62	1.26	1.87	---	2150	216	0.66	50% saturation
K18-8	90°	260	2.39	1.09	1.98	---	2230	216	0.69	50% saturation
Avg.			2.41	1.45	1.71	---	1800		0.68	
Std.Dev			0.29	0.28	0.26	---	430		0.02	
K14-4	90°	72	2.56	1.66	2.56	---	1450	3388	1.29	100% saturation
K15-5	90°	72	1.95	1.78	1.95	---	1100	3388	1.29	100% saturation
K16-6	90°	72	2.42	1.80	2.42	---	1400	3388	1.27	100% saturation
K17-6	90°	72	2.25	1.61	2.25	---	1420	3388	1.30	100% saturation
K18-9	90°	72	1.72	1.41	1.72	---	1230	3388	1.29	100% saturation
Avg.			2.18	1.65	2.18	---	1320		1.29	
Std.Dev			0.34	0.16	0.34	---	150		0.01	
K14-3	90°	260	1.67	1.27	0.59	---	1730	3388	1.29	100% saturation
K15-7	90°	260	1.61	1.34	0.58	---	1380	3388	1.28	100% saturation
K17-5	90°	260	1.53	1.38	0.46	---	1450	3388	1.31	100% saturation
K18-5	90°	260	1.52	1.06	0.53	---	1630	3388	1.28	100% saturation
K45-5	90°	260	1.61	1.17	0.75	---	1670	3388	1.27	100% saturation
Avg.			1.59	1.24	0.58	---	1570		1.29	
Std.Dev			0.06	0.13	0.11	---	150		0.01	

APPENDIX P
HUMIDITY AGED COMPRESSION DATA

All of the compression data generated during this program on specimens which had been humidity aged at 160°F (71°C) and 100% R.H. are presented in this section.

Summaries of these data are tabulated and plotted in the form of stress-strain curves in Sections 4.1 through 4.6.

Test: Compression After Environmental Aging @ 160°F & 100% R.H. Material: T300/AFR800										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ult. Strain (in/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
F35-7	90°	72	31.56	1.80	9.49	---	22,000	116	0.65	(1)
F35-19	90°	72	31.66	1.83	17.59	---	51,800	116	0.70	(1)
F35-29	90°	72	34.40	1.46	30.40	---	30,500	116	0.64	(1)
F36-1	90°	72	36.62	1.89	9.69	---	53,000	116	0.64	(1)
F36-16	90°	72	31.82	1.52	4.27	---	48,000	116	0.66	(1)
Avg.			32.92	1.70	14.29	---	41,100		0.66	
Std.Dev			2.47	0.20	10.19	---	14,000		0.02	
F35-4	90°	260	24.81	1.34	8.49	---	41,800	164	0.86	(1)
F35-13	90°	260	24.39	1.53	10.51	---	54,000	164	0.86	(1)
F35-16	90°	260	26.13	1.50	10.58	---	34,500	164	0.79	(1)
F36-11	90°	260	26.46	3.38	5.64	---	18,000	164	0.78	(1)
F36-17	90°	260	28.09	1.46	13.2	---	32,800	164	0.80	(1)
Avg.			25.98	1.84	9.69	---	36,200	164	0.81	
Std.Dev			1.47	0.86	2.82	---	13,200		0.03	
F35-10	90°	72	---	---	---	---	---	1904	1.27	(2)
F35-22	90°	72	33.82	2.31	8.92	---	37,000	1904	1.26	(2)
F36-12	90°	72	33.06	1.75	33.06	---	21,000	1904	1.34	(2)
F36-24	90°	72	29.69	1.35	9.41	---	54,300	1904	1.12	(2)
Avg.			32.19	1.80	17.13	---	37,400		1.25	
Std.Dev			2.19	0.48	13.80	---	16,700		0.10	
F35-12	90°	260	23.12	1.38	14.81	---	34,300	1904	1.34	(2)
F36-4	90°	260	25.93	2.23	10.87	---	13,000	1904	1.33	(2)
F36-10	90°	260	22.71	1.45	9.79	---	44,500	1904	1.35	(2)
F36-20	90°	260	24.69	1.46	10.61	---	43,600	1904	1.32	(2)
Avg.			24.11	1.63	11.52	---	33,900		1.34	
Std.Dev			1.48	0.40	2.24	---	14,600		0.02	

(1) 50% saturation (2) 100% saturation

Test: Compression After Environmental Aging @ 160°F & 100% R.H. Material: SIC/5506										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ult. Strain (in/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
G42-2	90°	72	30.41	4.59	4.34	---	32,100	162.5	0.83	(1)
G42-12	90°	72	31.44	3.14	7.85	---	33,000	162.5	0.64	(1)
G42-22	90°	72	29.88	5.25	18.29	---	7,100	162.5	0.79	(1), (3)
G42-38	90°	72	28.99	4.17	4.07	---	31,400	162.5	0.78	(1)
G42-54	90°	72	26.90	3.82	3.61	---	5,700	162.5	0.76	(1), (3)
Avg.			29.52	4.19	7.63	---	32,200		0.76	excludes G42-22 & G42-54
Std.Dev			1.71	0.79	6.19	---	800		0.07	
G42-3	90°	260	19.77	3.14	5.50	---	5,300	162.5	0.78	(1), (3)
G42-5	90°	260	17.52	3.37	7.44	---	5,000	162.5	0.80	(1), (3)
G42-8	90°	260	18.45	2.04	6.53	---	8,000	162.5	0.75	(1), (3)
G42-13	90°	260	19.29	2.63	5.19	---	7,400	162.5	0.79	(1), (3)
G42-28	90°	260	19.12	3.87	3.75	---	27,400	162.5	0.82	(1), (3)
Avg.			18.83	3.01	5.68	---	10,620		0.79	
Std.Dev			0.87	0.70	1.40	---	9,470		0.03	
G42-4	90°	72	25.71	2.33	11.22	---	17,900	1,752	---	(2)
G42-16	90°	72	24.69	2.72	8.15	---	18,200	1,752	1.41	(2)
G42-20	90°	72	24.05	2.51	11.42	---	19,000	1,752	1.22	(2)
G42-49	90°	72	23.77	3.90	5.33	---	32,100	1,752	1.30	(2)
G42-50	90°	72	24.09	2.79	15.39	---	15,200	1,752	1.31	(2)
Avg.			24.46	2.85	10.30	---	20,480		1.31	
Std.Dev			0.77	0.61	3.79	---	6,650		0.08	
G42-9	90°	260	18.96	3.18	9.73	---	14,700	1,752	1.31	(2)
G42-23	90°	260	16.46	2.90	11.59	---	5,970	1,752	1.32	(2)
G42-24	90°	260	17.59	2.81	8.78	---	21,600	1,752	1.31	(2)
G42-30	90°	260	19.98	4.70	15.45	---	3,470	1,752	1.29	(2), (3)
G42-43	90°	260	15.58	3.03	9.41	---	10,000	1,752	1.32	(2)
Avg.			17.71	3.32	10.99	---	11,150		1.31	
Std.Dev			1.79	0.78	2.70	---	7,230		0.01	

(1) 50% saturation (2) 100% saturation (3) Evidence of buckling

Test: Compression After Environmental Aging @ 160°F & 100% R.H. Material: HVE 2034D

Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ult. Strain (µin/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
H29-12	90°	72	12.00	3.02	3.35	---	13200	144.5	0.75	(1)
H29-33	90°	72	14.50	1.91	1.89	---	19500	144.5	0.78	(1)
H30-4	90°	72	17.59	1.26	3.51	---	30700	144.5	0.73	(1)
H30-18	90°	72	12.39	1.47	2.58	---	18500	144.5	0.70	(1)
Avg.			14.12	1.92	2.83	---	20480		0.74	
Std. Dev.			2.56	0.79	0.75	---	7360		0.03	
H29-14	90°	260	11.26	1.07	2.47	---	17500	144.5	0.76	(1)
H29-26	90°	260	12.80	2.00	2.38	---	22000	144.5	0.79	(1)
H29-18	90°	260	15.62	1.39	2.23	---	17700	144.5	0.79	(1)
H30-10	90°	260	13.56	1.08	2.87	---	23500	144.5	0.75	(1)
H30-15	90°	260	13.70	1.38	---	---	11750	144.5	0.73	(1)
Avg.			13.39	1.32	2.49	---	18490		0.76	
Std. Dev.			1.58	0.38	0.27	---	4600		0.03	
H29-3	90°	72	14.73	1.18	6.25	---	14600	1706.25	1.29	(2)
H29-8	90°	72	14.57	0.89	6.79	---	19200	1706.25	1.32	(2)
H29-27	90°	72	13.75	1.17	6.42	---	12300	2182.75	1.32	(2)
H29-30	90°	72	13.55	0.96	3.53	---	13800	2182.75	1.37	(2)
H30-8	90°	72	19.34	1.07	4.92	---	16000	2182.75	1.35	(2)
Avg.			15.19	1.05	5.58	---	15180		1.33	
Std. Dev.			2.38	0.13	1.35	---	2620		0.03	
H29-1	90°	260	13.33	1.22	2.10	---	19500	2182.75	1.25	(2)
H29-4	90°	260	---	1.04	2.09	---	---	2182.75	1.57	(2), (3)
H30-5	90°	260	14.15	0.96	3.33	---	25900	2182.75	1.36	(2)
H30-11	90°	260	17.05	1.27	3.76	---	13400	2182.75	1.32	(2)
H30-13	90°	260	19.63	0.86	---	---	18300	2182.75	1.39	(2)
Avg.			16.04	1.07	2.82	---	19280		1.38	
Std. Dev.			2.88	0.17	0.86	---	5140		0.12	

(1) 50% saturation (2) 100% saturation (3) Damaged before test

Test: Compression After Environmental Aging @ 160°F & 100% R.H. Material: T300/V378A										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ult. Strain (in/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
I42-21	90°	72°	26.99	1.96	1.53	---	25,500	17.5	0.73	(1)
I42-29	90°	72	25.73	1.79	1.82	---	36,300	17.5	0.64	(1)
I42-43	90°	72	25.35	2.56	1.98	---	43,800	17.5	0.64	(1)
I42-50	90°	72	21.77	1.94	1.77	---	30,600	17.5	0.70	(1)
I42-54	90°	72	21.17	1.54	1.61	---	22,800	17.5	0.72	(1)
Avg.			24.20	1.96	1.74	---	31,800		0.69	
Std.Dev			2.57	0.36	0.18	---	8,460		0.04	
I42-5	90°	350	20.12	1.95	1.29	---	11,700	17.5	0.70	(1), (3)
I42-34	90°	350	20.41	2.13	2.43	---	29,500	17.5	0.76	(1)
I42-45	90°	350	17.36	1.42	1.10	---	29,700	17.5	0.72	(1)
I42-51	90°	350	16.99	1.21	5.22	---	11,800	17.5	0.71	(1), (3)
I42-58	90°	350	16.77	1.29	1.76	---	13,800	17.5	0.67	(1), (3)
Avg.			18.33	1.60	2.36	---	29,600*		0.71	*excludes I42-5, I42-51, I42-58
Std.Dev			1.78	0.41	1.68	---	---		0.03	
I42-7	90°	72	24.88	2.76	2.72	---	11,900	2,471	1.33	(2), (3)
I42-11	90°	72	24.52	2.47	5.05	---	30,900	2,471	1.33	(2)
I42-23	90°	72	25.97	1.71	5.09	---	32,500	2,471	1.36	(2)
I42-27	90°	72	24.92	2.86	4.52	---	11,500	2,471	1.33	(2), (3)
I42-31	90°	72	26.34	2.45	4.28	---	12,900	2,471	1.33	(2), (3)
Avg.			25.33	2.45	4.33	---	31,700*		1.34	*excludes I42-7, I42-27, I42-31
Std.Dev			0.79	0.45	0.97	---	---		0.01	
I42-35	90°	350	16.93	3.55	2.60	---	26,200	2,471	1.38	(2)
I42-39	90°	350	17.07	1.13	4.22	---	15,500	2,471	1.34	(2)
I42-46	90°	350	21.97	3.68	2.21	---	33,400	2,471	1.37	(2)
I42-53	90°	350	20.36	2.60	3.43	---	11,500	2,471	1.36	(2), (3)
I42-55	90°	350	20.53	1.89	3.54	---	11,800	2,471	1.35	(2), (3)
Avg.			19.37	2.57	3.20	---	25,030*		1.36	*excludes I42-53, I42-55
Std.Dev			2.25	1.09	0.80	---	9,010*		0.02	

(1) 50% saturation (2) 100% saturation (3) Evidence of buckling

Test: Compression After Environmental Aging @ 160°F & 100% R.H. Material: HYE 1076J										
Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strngth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop.Lim. (ksi)	Pois. Ratio	Ult. Strain $\mu\text{in/in}$	Exposure Time (hrs)	Weight Gain (%)	Remarks
J31-13	90°	72	28.30	2.06	5.36	---	28200	161	0.74	(1)
J31-37	90°	72	24.25	2.42	4.81	---	24300	161	0.80	(1)
J31-41	90°	72	23.98	2.11	1.81	---	21700	161	0.75	(1)
J31-54	90°	72	25.45	2.27	3.02	---	11600	161	0.68	(1)
Avg.			25.50	2.22	3.75	---	21450		0.74	
Std.Dev			1.98	.16	1.63	---	7090		0.05	
J31-3	90°	260	21.28	2.00	3.69	---	15900	161	0.69	(1)
J31-11	90°	260	19.19	2.04	2.81	---	11300	161	0.78	(1)
J31-30	90°	260	24.33	1.43	6.16	---	34700	161	0.68	(1)
J31-47	90°	260	20.17	2.44	2.91	---	12800	161	0.76	(1)
J31-51	90°	260	19.24	1.62	4.39	---	9500	161	0.78	(1), (3)
Avg.			20.84	1.91	3.99	---	18680*		0.74	*excludes J31-51
Std.Dev			2.13	0.39	1.37	---	10850*		0.05	
J31-1	90°	72	21.8	1.86	13.7	---	9400	1,242	1.04	(2), (3)
J31-14	90°	72	24.2	1.77	12.5	---	25400	1,242	1.08	(2)
J31-16	90°	72	26.4	1.40	6.9	---	26600	1,242	1.09	(2)
J31-24	90°	72	25.9	1.71	9.9	---	14300	1,242	1.07	(2), (3)
J31-40	90°	72	29.3	1.43	8.9	---	43100	1,242	0.97	(2)
Avg.			25.5	1.63	10.4	---	31700*		1.05	*excludes J31-1, J31-24
Std.Dev			2.8	0.21	2.7	---	9890*		0.05	
J31-8	90°	260	17.9	2.38	10.0	---	11600	1,242	1.09	(2)
J31-32	90°	260	18.9	1.76	5.9	---	32000	1,242	1.08	(2)
J31-44	90°	260	16.8	1.69	5.8	---	20800	1,242	1.07	(2)
J31-52	90°	260	20.3	1.15	4.6	---	17900	1,242	1.12	(2)
J31-56	90°	260	23.4	1.22	7.1	---	28800	1,242	1.08	(2)
Avg.			19.5	1.64	6.7	---	22220		1.09	
Std.Dev			2.6	0.50	2.1	---	8250		0.02	
(1) 50% saturation (2) 100% saturation (3) Evidence of buckling										

(1) 50% saturation (2) 100% saturation (3) Evidence of buckling

Test: Compression After Environmental Aging @ 160°F & 100% R.H. Material: G-160/6535-1

Spec. No.	Fiber Orien.	Test Temp. (°F)	Ult. Strgth. (ksi)	Init. Mod. (10 ⁶ psi)	Stress at Prop. Lim. (ksi)	Pois. Ratio	Ult. Strain (in/in)	Exposure Time (hrs)	Weight Gain (%)	Remarks
K19-8	90°	72	30.65	1.75	7.82	---	16,900	166.5	0.63	Evidence of buckling
K19-32	90°	72	25.85	1.78	14.63	---	26,000	166.5	0.61	50% saturation
K44-6	90°	72	29.98	---	3.35	---	---	166.5	0.62	50% saturation
K44-10	90°	72	28.51	1.79	14.06	---	29,000	166.5	0.61	50% saturation
K44-29	90°	72	28.89	1.90	5.50	---	20,000	166.5	0.65	50% saturation
Avg.			28.73	1.81	9.07	---	22,980		0.62	
Std.Dev.			1.84	0.06	5.07	---	5,510		0.02	
K19-38	90°	260	18.37	1.59	7.17	---	7,900	166.5	0.61	Evidence of buckling
K44-5	90°	260	21.30	1.43	8.48	---	36,000	166.5	0.62	50% saturation
K44-7	90°	260	20.76	1.45	4.29	---	35,000	166.5	0.64	50% saturation
K44-16	90°	260	22.33	1.25	6.80	---	36,000	166.5	0.65	50% saturation
K44-26	90°	260	20.12	1.31	6.10	---	31,000	166.5	0.63	50% saturation
Avg.			20.58	1.41	6.59	---	29,180		0.63	
Std.Dev.			1.48	0.13	1.50	---	12,070		0.02	
K19-31	90°	72	28.80	1.70	15.60	---	19,450	1532	1.22	100% saturation
K19-39	90°	72	23.28	1.43	13.20	---	30,500	1532	1.21	100% saturation
K44-14	90°	72	29.04	1.71	11.92	---	29,500	1532	1.23	100% saturation
K44-15	90°	72	28.27	1.64	7.12	---	27,100	1532	1.22	100% saturation
K44-20	90°	72	---	---	---	---	---	---	---	failed in handling
Avg.			27.35	1.62	11.96	---	26,640		1.22	
Std.Dev.			2.73	0.13	3.57	---	5,000		0.01	
K19-7	90°	260	18.74	1.63	4.20	---	12,700	3621	1.27	Evidence of buckling
K19-29	90°	260	16.90	1.63	2.97	---	28,000	3621	1.24	100% saturation
K19-33	90°	260	16.17	1.46	3.68	---	26,000	3621	1.28	100% saturation
K19-44	90°	260	16.49	1.66	2.48	---	31,000	3621	1.28	100% saturation
K44-9	90°	260	18.43	1.64	3.26	---	36,000	3621	1.28	100% saturation
Avg.			17.34	1.61	3.32	---	26,740		1.27	
Std.Dev.			1.16	0.08	0.66	---	8,710		0.02	

APPENDIX Q
HUMIDITY AGED INTERLAMINAR SHEAR DATA

All of the interlaminar shear data generated during this program on specimens which had been humidity aged at 160°F (71°C) and 100% R.H. are presented in this section. These data are summarized in Sections 4.1 through 4.6.

L/D Ratio: 4/1

[illegible]

Materials: T300/AFR300 L/D Ratio: 4/1

[illegible]

L/D Ratio: 4/1

[illegible]

L/D Ratio: 4/1

[illegible]

L/D Ratio: 4/1

[illegible]

L/D Ratio: 4/1

[illegible]

Test: Interlaminar (Short-Beam) Shear After Environmental Aging at 160°F and 100% R.H.

Materials: T300/W378A

L/D Ratio: 4/1

Specimen Number	Test Temp. (°F)	Ultimate Strength (ksi)	Exposure Time (Hrs)	Weight Gain (%)	Remarks
I 15-5	72°	14.40	<48 ¹	0.79	50% saturation
I 15-11	72°	13.45	<48 ¹	0.86	50% saturation
I 15-15	72°	13.67	<48 ¹	0.85	50% saturation
I 15-19	72°	14.16	<48 ¹	0.81	50% saturation
I 15-23	72°	13.86	<48 ¹	0.70	50% saturation
I 15-30	72°	14.03	<48 ¹	0.74	50% saturation
I 15-44	72°	14.33	<48 ¹	0.46	50% saturation
I 15-46	72°	13.96	<48 ¹	0.76	50% saturation
I 15-50	72°	14.19	<48 ¹	0.65	50% saturation
I 15-52	72°	13.88	<48 ¹	0.81	50% saturation
Avg.		13.99		0.74	
Std. Dev.		0.29		0.12	
I 15-54	350°	8.71	<48 ¹	0.65	50% saturation
I 15-57	350°	8.69	<48 ¹	0.72	50% saturation
I 15-60	350°	7.84	<48 ¹	0.74	50% saturation
I 15-72	350°	9.70	<48 ¹	0.77	50% saturation
I 15-73	350°	9.59	<48 ¹	0.74	50% saturation
Avg.		8.91		0.72	
Std. Dev.		0.76		0.05	
¹ Specimens gained weight so rapidly that they were already saturated at first weighing (48 hrs.). They were dried in a dessicator at 72° f and 0% R.H. for 116 hr. to reach weight gain indicated.					

L/D Ratio: 4/1

[illegible]

Test: Interlaminar (Short-Beam) Shear After Environmental Aging at 160°F and 100% R.H.

Materials: HyE 1076J L/D Ratio: 4/1

[illegible]

L/D Ratio: 4/1

[illegible]

Test: Interlaminar (Short-Beam) Shear After Environmental Aging at 160°F and 100% R.H.

Materials: G-160/6535-1 L/D Ratio: 4/1

[illegible]

Materials: G-160/6535-1 L/D Ratio: 4/1

[illegible]